



August 1, 2018  
Ms. Kafi Howard  
Town of Blacksburg, Town Engineer  
400 South Main Street  
Blacksburg, Virginia 24060

RE: 1222 Patrick Henry PRD Application  
B&A Job #24180058.00

Dear Kafi,

Included in this packet are the Stormwater Management calculations for the proposed 1222 Patrick Henry PRD application. If you have any questions or comments please feel free to call.

Thank you for all of your and the staff's assistance with this project.

Sincerely,  
**BALZER AND ASSOCIATES, INC.**

A handwritten signature in dark ink, appearing to read "S. Semones", is written over a horizontal line.

Steven M. Semones, LA  
Vice President

**STORMWATER MANAGEMENT CALCULATIONS**

**FOR**

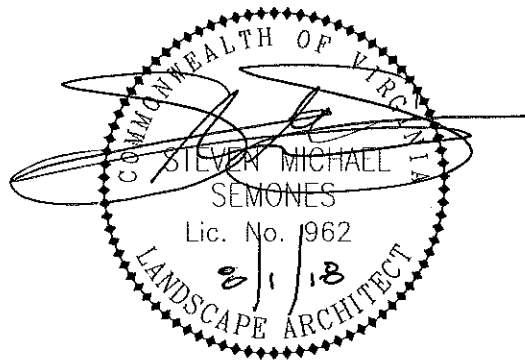
**1222 PATRICK HENRY  
PRD APPLICATION**

**1222 PATRICK HENRY DRIVE**

**PRICES FORK MAGISTERIAL DISTRICT  
TOWN OF BLACKSBURG, VA**

**B&A Job #24180058.00**

**AUGUST 1, 2018**



**PREPARED BY:**

**BALZER AND ASSOCIATES, INC.  
448 PEPPERS FERRY ROAD  
CHRISTIANSBURG, VIRGINIA 24073  
P-540-381-4290  
F-540-381-4291**

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## **SECTION I: PROJECT NARRATIVE**

### **Project Description**

The purpose of this project is the redevelopment of 4.215 acres of land to a PRD for Green Valley Builders. The site is located at 1222 Patrick Henry Drive in the Town of Blacksburg.

### **Existing Site Conditions**

The site<sup>1</sup> proposed for rezoning is approximately 4.215 acres. There is currently an existing house on the site. The ground cover is mostly grass with some trees. The site is bound by Patrick Henry Drive to the south, the Blacksburg Rescue Squad to the west, Town of Blacksburg open space to the north, and Hunters Ridge Apartments to the east. Existing soil conditions on-site are listed below. There are no wetlands or jurisdictional waters present on site. There are currently no stormwater management BMPs serving the site. Surrounding areas consist of developed urban land including commercial uses, multi-family residential, and single family residential.

#### **Existing soil conditions on-site include the following types:**

(See attached soils map and plans for specific locations.)

11C - Duffield-Ernest Complex, 7 to 15 percent slopes

K Factor: 0.28

Texture: Silt Loam

Hydrologic Soil Group: B

12C - Frederick and Vertrees Silt Loams, 7 to 15 percent slopes

K-Factor: 0.37

Texture: Silt Loam

Hydrologic Soil Group: B

18C - Groseclose-Urban Land Complex, 7 to 15 percent slopes

K Factor: 0.32

Texture: Loam

Hydrologic Soil Group: C

### **Development Plans**

The proposed development will remove the existing structures and build a new four-story apartment building. Surface parking will be provided around the building. An outdoor amenity area will be provided in a courtyard area and a clubhouse area will be provided indoors. A total of 276 bedrooms is proposed. The proposed site will also include sidewalk around the building, a connection to the existing public trail behind the site and a stormwater management facility. There is currently a Blacksburg Transit stop across Patrick Henry Drive, and a new stop on the project side of the street is proposed to be installed with this development.

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<sup>1</sup> For the purposes of the Project Narrative, “site” shall be defined as the area within the subject property boundary, 4.215 acres, Tax Map #196-A 5.

### **During Construction**

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The existing site consists of stabilized grasses areas that may become disturbed during construction activities. Any runoff from the site will be controlled with temporary measures such as a construction entrance, silt fence, inlet protection, sediment traps or basins, diversion dikes, seeding, and other measures per Virginia Erosion and Sediment Control Handbook standards.

### **Permanent Structures to Remain After Construction**

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After construction is complete, permanent ESC measures will be used for stabilization as needed. This will include measures such as permanent seeding, blankets and matting, and outlet protection, as well as anything else that is found to be necessary as design is finalized. There are two HUC's receiving waters from this site. Approximately half of the site drains to NE59 (New River-Stroubles Creek) while the other half drains to NE 60 (Toms Creek-Poverty Creek).

## **SECTION II: STORMWATER MANAGEMENT**

### **SUMMARY**

#### **PRE-DEVELOPMENT SUMMARY**

Please see sheet SW3 for drainage area map.

In the pre-development condition, the site is split into two distinct drainage areas. Runoff from Drainage Area #1 (approximately 8.00 acres total, with 1.98 acres coming from the project site) drains in a northwesterly direction towards the rear of the property, where it flows through an existing bioswale and under Progress Street by way of a 36" culvert. This culvert outfalls to a natural channel. From this point, runoff continues through a series of channels to Tom's Creek. Point of Analysis #1 has been set at the outfall of the 36" culvert.

Runoff from Drainage Area #2 (approximately 9.34 acres, with 2.23 acres coming from the project site) flows towards Patrick Henry Drive, where it is captured by curb inlets in the right of way and then carried across the street and into an existing detention pond. From this pond, flows continue through a combination of manmade and natural channels to the Duck Pond. Point of Analysis #2 has been set in the storm sewer on the southern side of Patrick Henry Drive.

There are no existing BMPs on the site or upstream of the development. All flows in this model have been analyzed using the SCS/TR-55, weighted Q method. See HydroCAD report for time of concentration calculations. Where a subwatershed is predominantly impervious, a minimum time of concentration of 6 minutes has been assumed.

**Point of Analysis #1**

Total Contributing Drainage Area = 8.00 acres

**PRE-DEVELOPMENT LAND COVER**

DESCRIPTION	AREA (AC)	SOIL TYPE	CN
OPEN SPACE	0.451	B	61
OPEN SPACE	1.433	C	74
WOODS	0.923	B	55
WOODS	0.285	C	70
RESIDENTIAL – 1/2 ACRE LOTS	0.164	B	70
RESIDENTIAL – 1/2 ACRE LOTS	0.371	C	80
RESIDENTIAL – 1/4 ACRE LOTS	0.282	B	75
RESIDENTIAL – 1/4 ACRE LOTS	0.496	C	83
MULTI-FAMILY RESIDENTIAL	0.044	B	85
URBAN COMMERCIAL	0.685	B	92
URBAN COMMERCIAL	2.402	C	94
ROW W/ CURB & GUTTER	0.047	B	98
ROW W/ CURB & GUTTER	0.209	C	98
IMPERVIOUS	0.104	B	98
IMPERVIOUS	0.101	C	98

*The CN value has been determined based upon soil type information obtained from the NRCS Web Soil Survey. All land covers are assumed to be in good condition and have been estimated from USGS mapping, aerial photography, and Town of Blacksburg GIS maps. All SCS land cover values were taken from Table 4-6a and Table 4-6b of the Virginia Stormwater Management Handbook. Rational “C” coefficients are derived from VSMH Table 4-3 “Rational Equation Runoff Coefficients”.*

The peak pre-development runoff flows at Point of Analysis #1 are as follows:  
(See HydroCAD report)

**1-year            3.67 cfs**  
**2-year            4.96 cfs**  
**10-year          8.69 cfs**  
**100-year        14.90 cfs**

**Point of Analysis #2**

Total Contributing Drainage Area = 9.34 acres

**PRE-DEVELOPMENT LAND COVER**

DESCRIPTION	AREA (AC)	SOIL TYPE	CN
OPEN SPACE	0.106	B	61
OPEN SPACE	1.061	C	74
WOODS	0.081	B	55
WOODS	1.159	C	70
MULTI-FAMILY RESIDENTIAL	0.326	B	85
MULTI-FAMILY RESIDENTIAL	4.881	C	90
ROW W/ CURB & GUTTER	0.028	B	98
ROW W/ CURB & GUTTER	0.285	C	98
IMPERVIOUS	1.415	C	98

*The CN value has been determined based upon soil type information obtained from the NRCS Web Soil Survey. All land covers are assumed to be in good condition and have been estimated from USGS mapping, aerial photography, and Town of Blacksburg GIS maps. All SCS land cover values were taken from Table 4-6a and Table 4-6b of the Virginia Stormwater Management Handbook. Rational "C" coefficients are derived from VSMH Table 4-3 "Rational Equation Runoff Coefficients".*

The peak pre-development runoff flows at Point of Analysis #2 are as follows:  
(See HydroCAD report)

<b>1-year</b>	<b>14.06 cfs</b>
<b>2-year</b>	<b>18.37 cfs</b>
<b>10-year</b>	<b>28.51 cfs</b>
<b>100-year</b>	<b>42.49 cfs</b>



## **POST-DEVELOPMENT SUMMARY**

Please see sheet SW4 for drainage area map and sheet SW5 for the stormwater management plan.

In the post development condition, the site will remain separated into two drainage areas. Two underground stormwater detention systems (one for each area) have been incorporated to manage and control runoff. Both systems have been designed to manage peak flows and meet all applicable water quantity requirements.

Please see the following pages and the enclosed HydroCAD report for a post development analysis of each drainage area.

**Point of Analysis #1**

The proposed underground system for Drainage Area #1 is located on the far western side of the site in the parking area. A small amount of drainage from the right of way will be rerouted to flow through the onsite system. Approximately 2.27 acres will drain to the system, with runoff being captured by curb and gutter and drainage inlets. The system will outfall at the rear of the site and runoff will flow through the existing bioswale. See below and enclosed HydroCAD calculations.

Total Drainage Area= 8.27 acres

**POST-DEVELOPMENT LAND COVER**

DESCRIPTION	AREA (AC)	SOIL TYPE	CN
OPEN SPACE	0.609	B	61
OPEN SPACE	0.808	C	74
WOODS	0.270	B	55
WOODS	0.076	C	70
RESIDENTIAL – 1/2 ACRE LOTS	0.164	B	70
RESIDENTIAL – 1/2 ACRE LOTS	0.371	C	80
RESIDENTIAL – 1/4 ACRE LOTS	0.282	B	75
RESIDENTIAL – 1/4 ACRE LOTS	0.496	C	83
RESIDENTIAL – MULTI-UNIT	0.044	B	85
URBAN COMMERCIAL	0.685	B	92
URBAN COMMERCIAL	2.402	C	94
ROW W/ CURB & GUTTER	0.047	B	98
ROW W/ CURB & GUTTER	0.209	C	98
IMPERVIOUS	0.407	B	98
IMPERVIOUS	1.406	C	98

*The CN value has been determined based upon soil type information obtained from the NRCS Web Soil Survey. All land covers are assumed to be in good condition and have been estimated from USGS mapping, aerial photography, and Town of Blacksburg GIS maps. All SCS land cover values were taken from Table 4-6a and Table 4-6b of the Virginia Stormwater Management Handbook. Rational “C” coefficients are derived from VSMH Table 4-3 “Rational Equation Runoff Coefficients”.*

The peak post-development runoff flows at the point of analysis are as follows:  
(See HydroCAD report)

**1-year            3.39 cfs**  
**2-year            4.89 cfs**  
**10-year          8.46 cfs**  
**100-year        15.35 cfs**

As shown above, the post-development flow at the Point of Analysis is less than the pre-development flow for the 1-year, 2-year, and 10-year storms, meeting the Town of Blacksburg stormwater management requirements.

**Point of Analysis #2**

The proposed underground stormwater system for Drainage Area #2 is located on the eastern side of the site, in the greenspace in front of the building. A small amount of offsite drainage will also be rerouted through this system. Approximately 2.27 acres will drain to the system as well, with runoff being captured by curb and gutter and drainage inlets. The system will outfall to a new manhole (labeled as “MH-A” on the plan), which will replace an existing curb inlet (“EX-1”). The curb inlet will need to be replaced due to the addition of the bus pull off lane. See below and enclosed HydroCAD calculations.

Total Drainage Area= 9.03 acres

**POST-DEVELOPMENT LAND COVER**

DESCRIPTION	AREA (AC)	SOIL TYPE	CN
OPEN SPACE	0.177	B	61
OPEN SPACE	0.665	C	74
WOODS	0.064	B	55
WOODS	0.074	C	70
RESIDENTIAL – MULTI-UNIT	0.326	B	85
RESIDENTIAL – MULTI-UNIT	4.878	C	90
PAVED ROADS/RIGHT OF WAY	0.028	B	98
PAVED ROADS/RIGHT OF WAY	1.519	C	98
IMPERVIOUS	0.131	B	98
IMPERVIOUS	1.172	C	98

*The CN value has been determined based upon soil type information obtained from the NRCS Web Soil Survey. All land covers are assumed to be in good condition and have been estimated from USGS mapping, aerial photography, and Town of Blacksburg GIS maps. All SCS land cover values were taken from Table 4-6a and Table 4-6b of the Virginia Stormwater Management Handbook. Rational “C” coefficients are derived from VSMH Table 4-3 “Rational Equation Runoff Coefficients”.*

The peak post-development runoff flows at the point of analysis are as follows:  
(See HydroCAD report)

**1-year            13.79 cfs**  
**2-year            17.83 cfs**  
**10-year          26.91 cfs**  
**100-year        50.06 cfs**

As shown above, the post-development flow at the Point of Analysis is less than the pre-development flow for the 1-year, 2-year, and 10-year storms, meeting the Town of Blacksburg stormwater management requirements.

### **Channel Protection**

In accordance with 9VAC25-870-66 (B), concentrated stormwater flows have been discharged directly to a stormwater conveyance system. The portion of the site<sup>2</sup> that discharges to Point of Analysis #1 outfalls to an existing bioswale and then travels through a series of natural conveyance systems to its 1% analysis point (approximately 228 acres). The portion of the site that discharges to Point of Analysis #2 outfalls to a manhole and travels first through a series storm pipes to an existing pond, then through a series of natural channels to its 1% analysis point (approximately 218 acres). Both drainage areas have met the requirements of channel protection per 9VAC25-870-66(B)(3) as shown below:

#### **R<sub>v</sub> Calculation – DA #1**

Pre-developed = 0.068 acre\*ft – See HydroCAD “RV Calculation” Report

Developed = 0.298 acre\*ft – See HydroCAD “RV Calculation” Report

$$Q_{Developed} \leq I.F. \times (Q_{Pre-developed} \times RV_{Pre-Developed}) / RV_{Developed}$$

$$Q_{Developed} \leq 0.8 \times (Q_{Pre-developed} \times 0.068) / 0.298$$

$$Q_{Developed} \leq 0.18 \times Q_{Pre-developed}$$

The resulting maximum allowable peak flow rate for the one-year 24-hour storm at Point of Analysis #1 is 3.41 cfs and the actual post-development peak flow achieved is 3.39 cfs.

#### **R<sub>v</sub> Calculation – DA #2**

Pre-developed = 0.117 acre\*ft – See HydroCAD “RV Calculation” Report

Developed = 0.276 acre\*ft – See HydroCAD “RV Calculation” Report

$$Q_{Developed} \leq I.F. \times (Q_{Pre-developed} \times RV_{Pre-Developed}) / RV_{Developed}$$

$$Q_{Developed} \leq 0.8 \times (Q_{Pre-developed} \times 0.117) / 0.276$$

$$Q_{Developed} \leq 0.34 \times Q_{Pre-developed}$$

The resulting maximum allowable peak flow rate for the one-year 24-hour storm at Point of Analysis #2 is 13.94 cfs and the actual post-development peak flow rate achieved is 13.79 cfs.

### **Flood Protection**

In accordance with 9VAC25-870-66 (C), concentrated stormwater flows have been discharged directly to a stormwater conveyance system.

For Drainage Area #1, the flow is discharged to an existing bioswale and is then carried through a natural stormwater conveyance system. This system carries flows to a point where the contributing drainage area is less than or equal to 1.0% of the total watershed area as defined in subdivision 3(a) of the regulations (at least 228 acres).

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<sup>2</sup> In the context of channel and flood protection, “site” shall be defined as the land or water area where the land-disturbing activity is physically conducted (the area of land disturbance, approx. 4.46 acres), including the limits of any off-site land disturbance. See Sheets SW3-SW4.

For Drainage Area #2, the flow is discharged to an existing manhole, then carried through a series of storm pipes to an existing pond. Once the flow exits the pond, it is carried through a natural conveyance system to a point where the contributing drainage area is less than or equal to 1.0% of the total watershed area as defined in subdivision 3(a) of the regulations (at least 218 acres).

As shown on the attached HydroCAD calculations, the point of discharge for each drainage area releases a post-development peak flow rate for the 10-year 24-hour storm event that is less than the pre-development peak flow rate from the 10-year 24-hour storm event, satisfying subdivision 2(b). Per subdivision (3), no further analysis of the downstream stormwater conveyance system is required.

## **SECTION III: STORMWATER QUALITY SUMMARY**

Water quality compliance has been achieved through use of the Virginia Runoff Reduction Method in accordance with the design criteria set forth in 9VAC25-870-65 and through the purchase of nutrient credits in accordance with the criteria set forth in the Code of Virginia. Per §62.1-44.15:35 (C)(2), the VSMP shall allow the use of nutrient credits when less than five acres of land will be disturbed or the phosphorus water quality reduction requirement is less than 10 pounds per year. The proposed development is within the thresholds for permitted use of credits, with a disturbance area of approximately 4.46 acres and a required phosphorus load reduction of 5.16 lb/yr.

The existing site<sup>3</sup> is a single-family lot with a house and shed located on it. The pre-development site has an impervious land cover of 0.35 acres (7.85%). The post development site has an impervious land cover of 3.10 acres (69.5%), resulting in a composite runoff coefficient ( $R_v$ ) of 0.72. The prescribed phosphorus pollutant reduction requirement is 5.16 lb/yr, which will be handled by purchasing credits. Please see attached calculation sheets.

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<sup>3</sup> In the context of water quality compliance, “site” shall be defined as the land or water area where the land-disturbing activity is physically conducted (the area of land disturbance, 4.46 acres), including the limits of any off-site land disturbance. See Sheets SW3-SW4.

## **SECTION IV: DOWNSTREAM ANALYSIS**

Runoff from Drainage Area #1 is discharged to an existing bioswale and is then carried through a natural conveyance system towards its 1% analysis point. Runoff from Drainage Area #2 is discharged directly to a manmade stormwater conveyance system and is then carried through a series of storm pipes to an existing pond. Once runoff leaves the pond, it enters a natural conveyance system and is carried through a combination of manmade and natural conveyance systems towards its 1% analysis point. The post development peak runoff rate for each drainage area has been mitigated through the use of BMP's to prevent adverse impacts to downstream properties in the form of channel erosion, flooding, or increased pollutant loads.

Per 9VAC25-870-66 subsection A, compliance with Minimum Standard 19 of the Virginia Erosion and Sediment Control Regulations has been satisfied by meeting the requirements of the for channel protection and flood protection as shown in the Post Development Summary. No adverse impacts to downstream properties are expected as a result of this development.

## **SECTION V: STORMWATER MANAGEMENT MAINTENANCE/INSPECTION PLAN**

### **Generally:**

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1. The owner is responsible for providing or coordinating all facility inspections and any required maintenance that may result from such inspections.
2. Requirements listed here are to be taken as a minimum and do not represent the limit of responsibility.
3. Any standing water pumped during the maintenance operation must be disposed of per the VESCH, 1992 edition and any local requirements.

### **Required Action:**

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#### **Underground Detention Facilities:**

1. Every (6) months and after each major runoff producing storm event, a maintenance visit shall be performed and documented, and any repairs necessary to areas of failure/concern discovered during inspection shall be carried out. Typical maintenance tasks include:
  - a. Cleanout of any debris or sediment accumulated in the structure that reduces the storage volume or otherwise hinders the performance of the facility.
  - b. Visual inspection for structural deterioration, spalling, or cracking of the structural components.
2. The flow control manholes shall be inspected after each runoff producing storm event to check for debris and/or sediment accumulation that may compromise the performance of the structure. Such debris and sediments shall be removed immediately.

Per the Town of Blacksburg stormwater ordinance, a formal maintenance agreement shall be provided to the Town for review and ultimately recorded at the Montgomery County Courthouse legally binding the identified party to the maintenance/inspection responsibilities listed above.



## **SECTION VI: ALTERNATIVE STORMWATER MANAGEMENT PLAN**

We have shown with the above calculations and enclosed HydroCAD report that stormwater runoff can be managed through the use of underground detention facilities on site and that all town and state requirements are able to be met. However, we plan to explore an alternative option prior to submitting for site plan approval. Instead of installing two systems on site, we will look at the possibility of taking all stormwater runoff offsite to an existing town-owned stormwater detention pond located at the southern end of the Collegiate Suites community. A field survey of the existing pond will be completed and all existing storm pipes currently draining to the pond will be analyzed. If it is determined that this is a practical and affordable option, we will submit a full analysis and design plan showing any improvements needed for the pond and existing storm sewer system.

**APPENDIX A:**  
**SOIL MAPS & SOIL DESCRIPTIONS**



United States  
Department of  
Agriculture

NRCS

Natural  
Resources  
Conservation  
Service

A product of the National  
Cooperative Soil Survey,  
a joint effort of the United  
States Department of  
Agriculture and other  
Federal agencies, State  
agencies including the  
Agricultural Experiment  
Stations, and local  
participants

# Custom Soil Resource Report for Montgomery County, Virginia



# Preface

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Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist ([http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2\\_053951](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951)).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# How Soil Surveys Are Made

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Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and



## Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

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The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

# Custom Soil Resource Report Soil Map



Map Scale: 1:1,210 if printed on A landscape (11" x 8.5") sheet.

Meters				
0	15	30	60	90

Feet				
0	50	100	200	300

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 17N WGS84

# Custom Soil Resource Report


## MAP LEGEND

### Area of Interest (AOI)

 Area of Interest (AOI)

### Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

### Special Point Features

 Blowout

 Borrow Pit

 Clay Spot

 Closed Depression

 Gravel Pit

 Gravelly Spot

 Landfill

 Lava Flow

 Marsh or swamp

 Mine or Quarry

 Miscellaneous Water

 Perennial Water

 Rock Outcrop


 Saline Spot

 Sandy Spot

 Severely Eroded Spot

 Sinkhole

 Slide or Slip

 Sodic Spot

 Spoil Area

 Stony Spot

 Very Stony Spot

 Wet Spot

 Other

 Special Line Features

### Water Features

 Streams and Canals

### Transportation

 Rails


 Interstate Highways

 US Routes

 Major Roads

 Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL:  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Montgomery County, Virginia  
Survey Area Data: Version 10, Oct 3, 2017

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Oct 22, 2012—Feb 5, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
11C	Duffield-Ernest complex, 7 to 15 percent slopes	0.2	4.5%
12C	Frederick and Vertrees silt loams, 7 to 15 percent slopes	0.6	14.2%
18C	Groseclose-Urban land complex, 7 to 15 percent slopes	3.4	81.3%
<b>Totals for Area of Interest</b>		<b>4.2</b>	<b>100.0%</b>

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or

landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## Montgomery County, Virginia

### 11C—Duffield-Ernest complex, 7 to 15 percent slopes

#### Map Unit Setting

*National map unit symbol:* kc1r

*Elevation:* 1,300 to 3,000 feet

*Mean annual precipitation:* 30 to 45 inches

*Mean annual air temperature:* 50 to 57 degrees F

*Frost-free period:* 117 to 185 days

*Farmland classification:* Farmland of statewide importance

#### Map Unit Composition

*Duffield and similar soils:* 45 percent

*Ernest and similar soils:* 35 percent

*Minor components:* 3 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

#### Description of Duffield

##### Setting

*Landform:* Drainageways

*Landform position (two-dimensional):* Footslope

*Landform position (three-dimensional):* Base slope

*Down-slope shape:* Concave

*Across-slope shape:* Convex

*Parent material:* Loamy colluvial, alluvial, eolian sediments underlain by loamy and clayey residuum of limestone and shale

##### Typical profile

*H1 - 0 to 7 inches:* silt loam

*H2 - 7 to 37 inches:* silty clay loam

*H3 - 37 to 79 inches:* clay

##### Properties and qualities

*Slope:* 7 to 15 percent

*Depth to restrictive feature:* 48 to 99 inches to lithic bedrock

*Natural drainage class:* Well drained

*Runoff class:* Medium

*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to high (0.57 to 1.98 in/hr)

*Depth to water table:* More than 80 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Available water storage in profile:* High (about 10.3 inches)

##### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 3e

*Hydrologic Soil Group:* B

*Hydric soil rating:* No

#### Description of Ernest

##### Setting

*Landform:* Drainageways

## Custom Soil Resource Report

*Landform position (two-dimensional):* Footslope  
*Landform position (three-dimensional):* Base slope  
*Down-slope shape:* Concave  
*Across-slope shape:* Convex  
*Parent material:* Interbedded limestone and shale residuum

### Typical profile

*H1 - 0 to 6 inches:* silt loam  
*H2 - 6 to 26 inches:* silty clay loam  
*H3 - 26 to 50 inches:* silty clay loam  
*H4 - 50 to 79 inches:* silty clay loam

### Properties and qualities

*Slope:* 7 to 15 percent  
*Depth to restrictive feature:* 20 to 35 inches to fragipan  
*Natural drainage class:* Moderately well drained  
*Runoff class:* Medium  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately low to moderately high (0.06 to 0.57 in/hr)  
*Depth to water table:* About 18 to 36 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Available water storage in profile:* Low (about 3.8 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 3e  
*Hydrologic Soil Group:* C  
*Hydric soil rating:* No

### Minor Components

#### Purdy

*Percent of map unit:* 3 percent  
*Landform:* Depressions, stream terraces  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Hydric soil rating:* Yes

## 12C—Frederick and Vertrees silt loams, 7 to 15 percent slopes

### Map Unit Setting

*National map unit symbol:* kc1t  
*Elevation:* 1,700 to 3,000 feet  
*Mean annual precipitation:* 30 to 45 inches  
*Mean annual air temperature:* 50 to 57 degrees F  
*Frost-free period:* 117 to 185 days  
*Farmland classification:* Farmland of statewide importance



### Map Unit Composition

*Frederick and similar soils:* 40 percent

*Vertrees and similar soils:* 35 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Frederick

#### Setting

*Landform:* Hills

*Landform position (two-dimensional):* Backslope, summit

*Landform position (three-dimensional):* Interfluve, side slope

*Down-slope shape:* Convex

*Across-slope shape:* Convex

*Parent material:* Limestone interbedded with siltstone and shale residuum

#### Typical profile

*H1 - 0 to 10 inches:* silt loam

*H2 - 10 to 22 inches:* clay

*H3 - 22 to 79 inches:* clay

#### Properties and qualities

*Slope:* 7 to 15 percent

*Depth to restrictive feature:* More than 80 inches

*Natural drainage class:* Well drained

*Runoff class:* Medium

*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to high (0.57 to 1.98 in/hr)

*Depth to water table:* More than 80 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Available water storage in profile:* High (about 9.1 inches)

#### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 3e

*Hydrologic Soil Group:* B

*Forage suitability group:* Moist, Fertile Soils (G128XB001VA)

*Hydric soil rating:* No

### Description of Vertrees

#### Setting

*Landform:* Hills

*Landform position (two-dimensional):* Backslope, summit

*Landform position (three-dimensional):* Interfluve, side slope

*Down-slope shape:* Convex

*Across-slope shape:* Convex

*Parent material:* Limestone, siltstone, and shale residuum

#### Typical profile

*H1 - 0 to 10 inches:* silt loam

*H2 - 10 to 25 inches:* silty clay

*H3 - 25 to 50 inches:* clay

*H4 - 50 to 79 inches:* clay

#### Properties and qualities

*Slope:* 7 to 15 percent

## Custom Soil Resource Report

*Depth to restrictive feature:* More than 80 inches

*Natural drainage class:* Well drained

*Runoff class:* Medium

*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high (0.20 to 0.57 in/hr)

*Depth to water table:* More than 80 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Available water storage in profile:* Moderate (about 8.9 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 3e

*Hydrologic Soil Group:* C

*Forage suitability group:* Moist, Fertile Soils (G128XB001VA)

*Hydric soil rating:* No

## 18C—Groseclose-Urban land complex, 7 to 15 percent slopes

### Map Unit Setting

*National map unit symbol:* kc28

*Elevation:* 1,300 to 3,000 feet

*Mean annual precipitation:* 30 to 45 inches

*Mean annual air temperature:* 50 to 57 degrees F

*Frost-free period:* 117 to 185 days

*Farmland classification:* Not prime farmland

### Map Unit Composition

*Groseclose and similar soils:* 40 percent

*Urban land:* 30 percent

*Minor components:* 3 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Groseclose

#### Setting

*Landform:* Hills

*Landform position (two-dimensional):* Backslope, summit

*Landform position (three-dimensional):* Interfluve, side slope

*Down-slope shape:* Convex

*Across-slope shape:* Convex

*Parent material:* Limestone, shale, siltstone, and sandstone residuum

#### Typical profile

*H1 - 0 to 10 inches:* loam

*H2 - 10 to 28 inches:* clay

*H3 - 28 to 39 inches:* clay

*H4 - 39 to 51 inches:* clay

*H5 - 51 to 79 inches:* clay loam

## Custom Soil Resource Report

### Properties and qualities

*Slope:* 7 to 15 percent  
*Depth to restrictive feature:* More than 80 inches  
*Natural drainage class:* Well drained  
*Runoff class:* High  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately low to moderately high (0.06 to 0.20 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Available water storage in profile:* Moderate (about 8.7 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 3e  
*Hydrologic Soil Group:* C  
*Hydric soil rating:* No

### Description of Urban Land

#### Setting

*Landform:* Hills  
*Landform position (two-dimensional):* Backslope, summit  
*Landform position (three-dimensional):* Interfluve, side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Parent material:* Limestone, shale, siltstone, and sandstone residuum

### Minor Components

#### Purdy

*Percent of map unit:* 3 percent  
*Landform:* Depressions, stream terraces  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Hydric soil rating:* Yes

# **Soil Information for All Uses**

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## **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

## **Soil Erosion Factors**

Soil Erosion Factors are soil properties and interpretations used in evaluating the soil for potential erosion. Example soil erosion factors can include K factor for the whole soil or on a rock free basis, T factor, wind erodibility group and wind erodibility index.

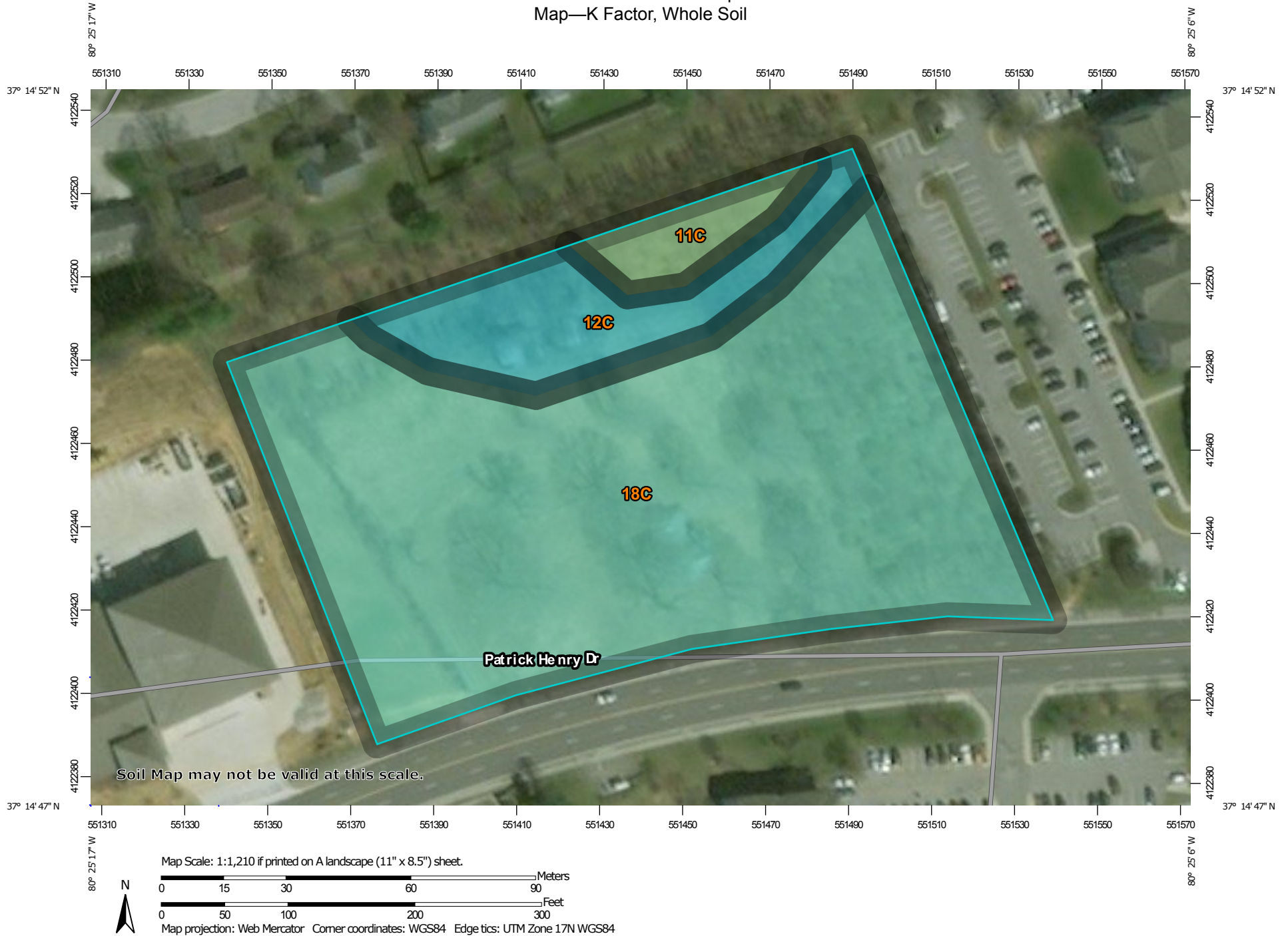
### **K Factor, Whole Soil**

Erosion factor K indicates the susceptibility of a soil to sheet and rill erosion by water. Factor K is one of six factors used in the Universal Soil Loss Equation (USLE) and the Revised Universal Soil Loss Equation (RUSLE) to predict the average annual rate of soil loss by sheet and rill erosion in tons per acre per year. The estimates are based primarily on percentage of silt, sand, and organic matter and on soil structure and saturated hydraulic conductivity (Ksat). Values of K range from 0.02 to 0.69. Other factors being equal, the higher the value, the more susceptible the soil is to sheet and rill erosion by water.

"Erosion factor Kw (whole soil)" indicates the erodibility of the whole soil. The estimates are modified by the presence of rock fragments.

# Custom Soil Resource Report


## Map—K Factor, Whole Soil



# Custom Soil Resource Report
















## MAP LEGEND

### Area of Interest (AOI)







 Area of Interest (AOI)










### Soils

#### Soil Rating Polygons
















	.02
	.05
	.10
	.15
	.17
	.20
	.24
	.28
	.32
	.37
	.43
	.49
	.55
	.64
	Not rated or not available

#### Soil Rating Lines








	.02
	.05
	.10
	.15
	.17
	.20

	.24
	.28
	.32
	.37
	.43
	.49
	.55
	.64
	Not rated or not available

#### Soil Rating Points

	.02
	.05
	.10
	.15
	.17
	.20
	.24
	.28
	.32
	.37
	.43
	.49
	.55
	.64
	Not rated or not available

### Water Features

	Streams and Canals
	Rails
	Interstate Highways
	US Routes
	Major Roads
	Local Roads
	Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL:  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Montgomery County, Virginia  
Survey Area Data: Version 10, Oct 3, 2017

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Oct 22, 2012—Feb 5, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

**Table—K Factor, Whole Soil**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
11C	Duffield-Ernest complex, 7 to 15 percent slopes	.28	0.2	4.5%
12C	Frederick and Vertrees silt loams, 7 to 15 percent slopes	.37	0.6	14.2%
18C	Groseclose-Urban land complex, 7 to 15 percent slopes	.32	3.4	81.3%
<b>Totals for Area of Interest</b>			<b>4.2</b>	<b>100.0%</b>

**Rating Options—K Factor, Whole Soil**

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Higher

*Layer Options (Horizon Aggregation Method):* Surface Layer (Not applicable)

**Soil Physical Properties**

Soil Physical Properties are measured or inferred from direct observations in the field or laboratory. Examples of soil physical properties include percent clay, organic matter, saturated hydraulic conductivity, available water capacity, and bulk density.

**Surface Texture**

This displays the representative texture class and modifier of the surface horizon.

Texture is given in the standard terms used by the U.S. Department of Agriculture. These terms are defined according to percentages of sand, silt, and clay in the fraction of the soil that is less than 2 millimeters in diameter. "Loam," for example, is soil that is 7 to 27 percent clay, 28 to 50 percent silt, and less than 52 percent sand. If the content of particles coarser than sand is 15 percent or more, an appropriate modifier is added, for example, "gravelly."




# Custom Soil Resource Report Map—Surface Texture








## MAP LEGEND

### Area of Interest (AOI)




 Area of Interest (AOI)

### Soils




#### Soil Rating Polygons

 Loam  
 Silt loam  
 Not rated or not available


#### Soil Rating Lines

 Loam  
 Silt loam  
 Not rated or not available






#### Soil Rating Points

 Loam  
 Silt loam  
 Not rated or not available

### Water Features

 Streams and Canals

### Transportation

 Rails  
 Interstate Highways  
 US Routes  
 Major Roads  
 Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

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 Survey Area Data: Version 10, Oct 3, 2017

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Oct 22, 2012—Feb 5, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

**Table—Surface Texture**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
11C	Duffield-Ernest complex, 7 to 15 percent slopes	Silt loam	0.2	4.5%
12C	Frederick and Vertrees silt loams, 7 to 15 percent slopes	Silt loam	0.6	14.2%
18C	Groseclose-Urban land complex, 7 to 15 percent slopes	Loam	3.4	81.3%
<b>Totals for Area of Interest</b>			<b>4.2</b>	<b>100.0%</b>

**Rating Options—Surface Texture**

*Aggregation Method:* Dominant Condition

*Component Percent Cutoff:* None Specified

*Tie-break Rule:* Lower

*Layer Options (Horizon Aggregation Method):* Surface Layer (Not applicable)

**Soil Qualities and Features**

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

**Hydrologic Soil Group**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

## Custom Soil Resource Report

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.


If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

# Custom Soil Resource Report Map—Hydrologic Soil Group



## MAP LEGEND

### Area of Interest (AOI)









 Area of Interest (AOI)

### Soils

#### Soil Rating Polygons





 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Lines


 A  
 A/D  
 B  
 B/D  
 C  
 C/D  
 D  
 Not rated or not available

#### Soil Rating Points






 A  
 A/D  
 B  
 B/D

 C  
 C/D  
 D  
 Not rated or not available


### Water Features

 Streams and Canals

### Transportation

 Rails  
 Interstate Highways  
 US Routes  
 Major Roads  
 Local Roads

### Background

 Aerial Photography

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Montgomery County, Virginia  
 Survey Area Data: Version 10, Oct 3, 2017

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Oct 22, 2012—Feb 5, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

**Table—Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
11C	Duffield-Ernest complex, 7 to 15 percent slopes	B	0.2	4.5%
12C	Frederick and Vertrees silt loams, 7 to 15 percent slopes	B	0.6	14.2%
18C	Groseclose-Urban land complex, 7 to 15 percent slopes	C	3.4	81.3%
<b>Totals for Area of Interest</b>			<b>4.2</b>	<b>100.0%</b>

**Rating Options—Hydrologic Soil Group***Aggregation Method: Dominant Condition**Component Percent Cutoff: None Specified**Tie-break Rule: Higher*

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---

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## Custom Soil Resource Report

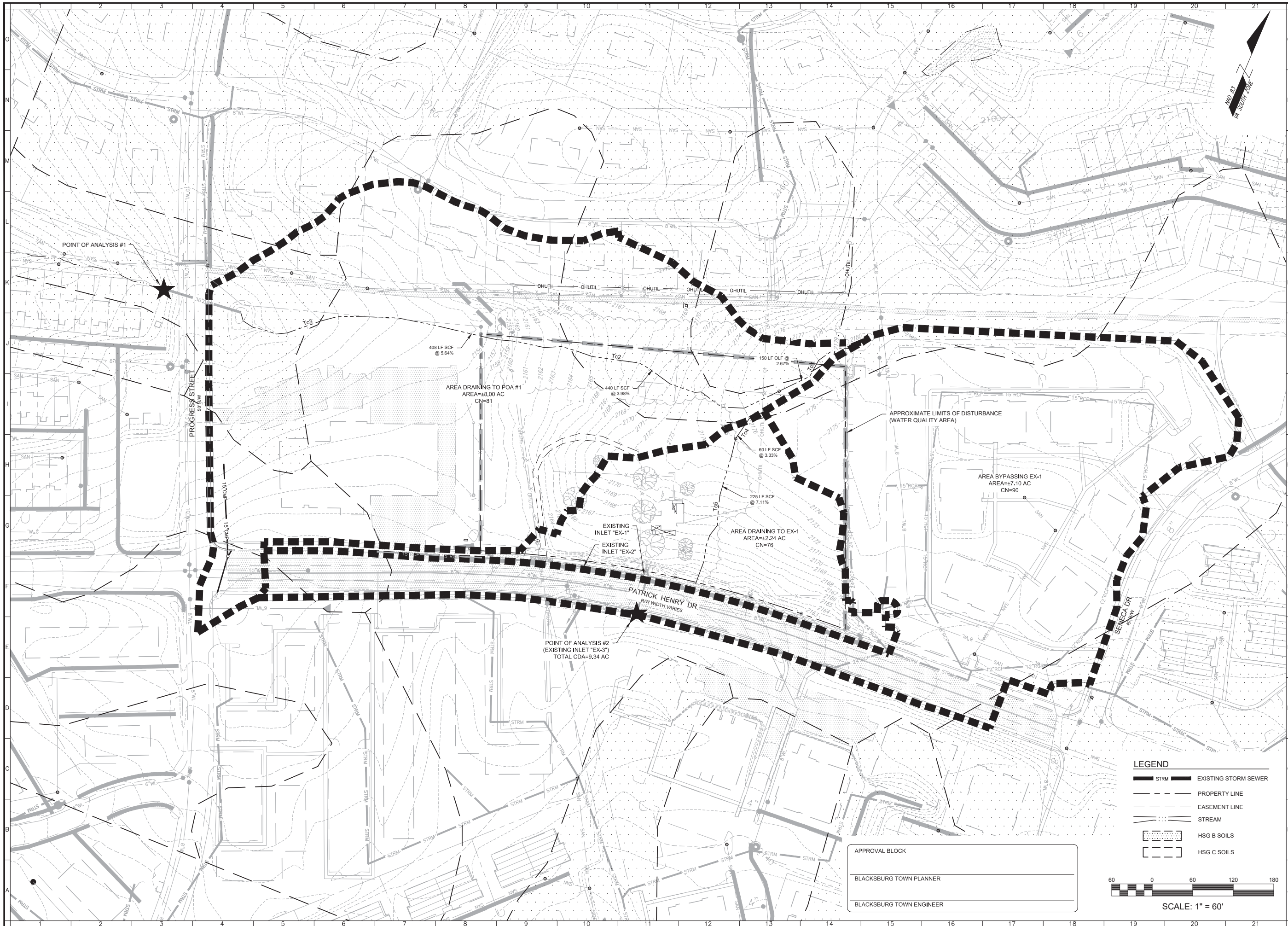
United States Department of Agriculture, Natural Resources Conservation Service. National soil survey handbook, title 430-VI. [http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/scientists/?cid=nrcs142p2\\_054242](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/scientists/?cid=nrcs142p2_054242)

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**APPENDIX B:**  
**DRAINAGE MAPS**



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Richmond  
Roanoke  
Staunton  
Harrisonburg

RESIDENTIAL LAND DEVELOPMENT ENGINEERING  
SITE DEVELOPMENT ENGINEERING  
LAND USE PLANNING & ZONING  
LANDSCAPE ARCHITECTURE  
LAND SURVEYING  
ARCHITECTURE  
STRUCTURAL ENGINEERING  
TRANSPORTATION ENGINEERING  
ENVIRONMENTAL & SOIL SCIENCE  
WETLAND DELINEATIONS & STREAM EVALUATIONS

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448 Peppers Ferry Road, NW  
Christiansburg, VA 24073  
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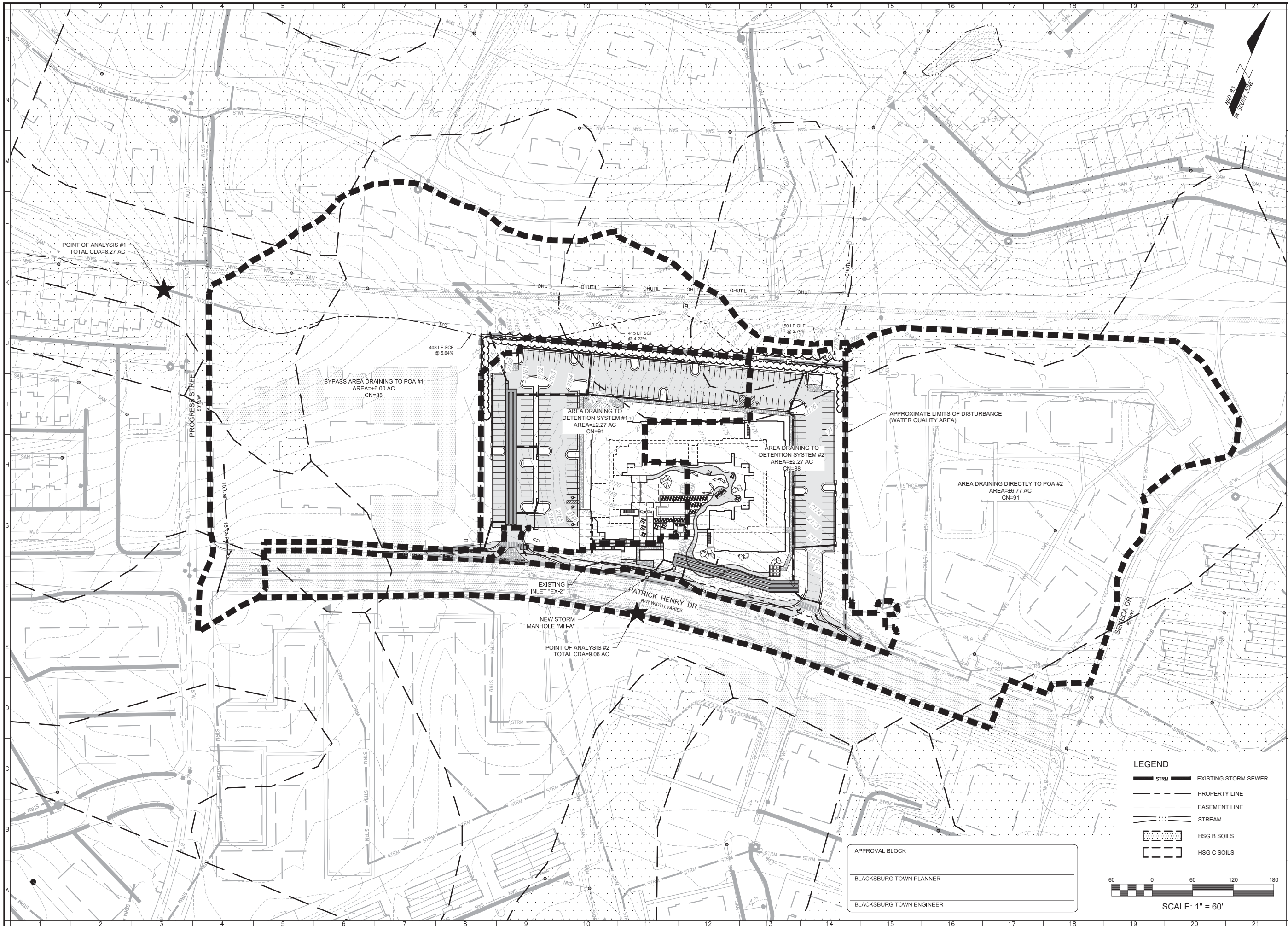
1222 PATRICK HENRY PRD  
1222 PATRICK HENRY DRIVE  
PRE-DEVELOPMENT DRAINAGE AREA MAP  
PRICES FORK MAGISTERIAL DISTRICT  
TOWN OF BLACKSBURG, VIRGINIA

DRAWN BY GLM  
DESIGNED BY GLM  
CHECKED BY SMS  
DATE 8/1/18  
SCALE 1"=60'

REVISIONS:

SHEET NO.  
**SW3**  
JOB NO. 24180058.00





www.balzer.cc  
New River Valley  
Richmond  
Roanoke  
Staunton  
Harrisonburg

RESIDENTIAL LAND DEVELOPMENT ENGINEERING  
SITE DEVELOPMENT ENGINEERING  
LAND USE PLANNING & ZONING  
LANDSCAPE ARCHITECTURE  
LAND SURVEYING  
ARCHITECTURE  
STRUCTURAL ENGINEERING  
TRANSPORTATION ENGINEERING  
ENVIRONMENTAL & SOIL SCIENCE  
WETLAND DELINEATIONS & STREAM EVALUATIONS

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Christiansburg, VA 24073  
540-381-4290  
FAX 540-381-4291



1222 PATRICK HENRY PRD  
1222 PATRICK HENRY DRIVE  
POST-DEVELOPMENT DRAINAGE AREA MAP  
PRICES FORK MAGISTERIAL DISTRICT  
TOWN OF BLACKSBURG, VIRGINIA

DRAWN BY GLM  
DESIGNED BY GLM  
CHECKED BY SMS  
DATE 8/1/18  
SCALE 1"=60'

REVISIONS:

SHEET NO.  
**SW4**  
JOB NO. 24180058.00

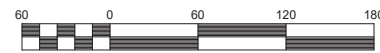
#### LEGEND

- STRM EXISTING STORM SEWER
- PROPERTY LINE
- EASEMENT LINE
- STREAM
- HSG B SOILS
- HSG C SOILS

APPROVAL BLOCK

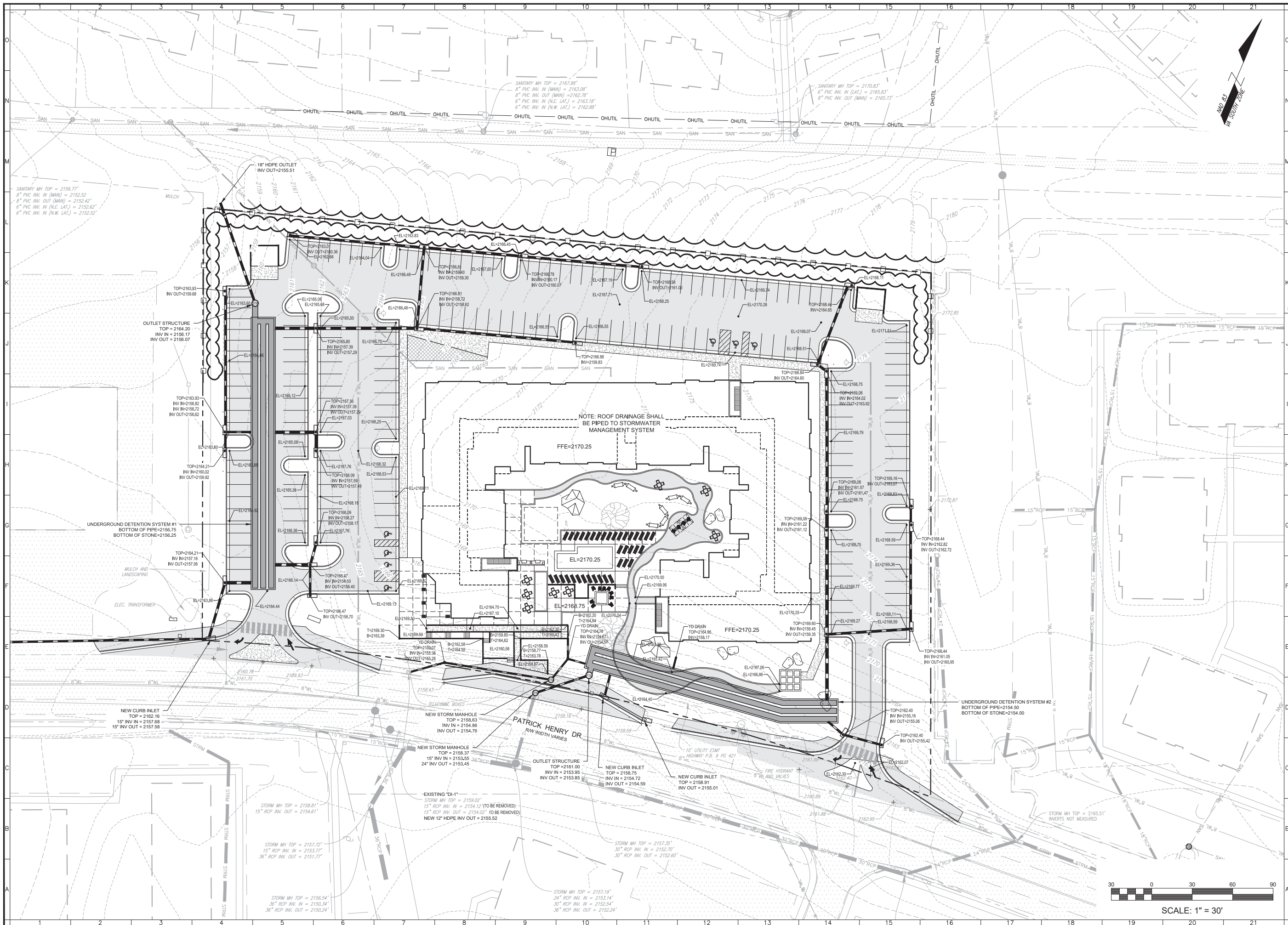
BLACKSBURG TOWN PLANNER

BLACKSBURG TOWN ENGINEER



SCALE: 1" = 60'





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New River Valley  
Richmond  
Roanoke  
Staunton  
Harrisonburg

RESIDENTIAL LAND DEVELOPMENT ENGINEERING  
SITE DEVELOPMENT ENGINEERING  
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LANDSCAPE ARCHITECTURE  
LAND SURVEYING  
ARCHITECTURE  
STRUCTURAL ENGINEERING  
TRANSPORTATION ENGINEERING  
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**1222 PATRICK HENRY PRD**  
1222 PATRICK HENRY DRIVE  
**STORMWATER MANAGEMENT PLAN**  
PRICES FORK MAGISTERIAL DISTRICT  
TOWN OF BLACKSBURG, VIRGINIA

DRAWN BY GLM  
DESIGNED BY GLM  
CHECKED BY SMS  
DATE 8/1/18  
SCALE 1"=30'  
REVISIONS:

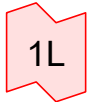
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**APPENDIX C:**  
**STORMWATER MANAGEMENT CALCULATIONS**

## **WATER QUANTITY**



DA #1



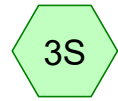
POA #1



AREA DRAINING TO  
EX-1



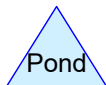
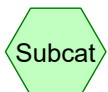
EX-1



AREA BYPASSING  
EX-1



POA #2



### Routing Diagram for PRE DEV

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**PRE DEV**

VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Prepared by Balzer &amp; Associates, Inc.

Printed 8/1/2018

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Page 2

Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q  
Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

**Subcatchment1S: DA #1**

Runoff Area=7.997 ac Runoff Depth=0.97"  
Flow Length=998' Tc=58.8 min CN=WQ Runoff=3.67 cfs 0.648 af

**Subcatchment2S: AREA DRAINING TO EX-1**

Runoff Area=2.238 ac Runoff Depth=0.67"  
Flow Length=285' Tc=22.7 min CN=WQ Runoff=1.01 cfs 0.125 af

**Subcatchment3S: AREA BYPASSING EX-1**

Runoff Area=7.104 ac Runoff Depth=1.38"  
Tc=6.0 min CN=WQ Runoff=13.72 cfs 0.814 af

**Link 1L: POA #1**

Inflow=3.67 cfs 0.648 af  
Primary=3.67 cfs 0.648 af

**Link 2L: EX-1**

Inflow=1.01 cfs 0.125 af  
Primary=1.01 cfs 0.125 af

**Link 3L: POA #2**

Inflow=14.06 cfs 0.939 af  
Primary=14.06 cfs 0.939 af

**Total Runoff Area = 17.339 ac Runoff Volume = 1.587 af Average Runoff Depth = 1.10"**



**PRE DEV**

VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

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Page 3

**Summary for Subcatchment 1S: DA #1**

Runoff = 3.67 cfs @ 12.75 hrs, Volume= 0.648 af, Depth= 0.97"

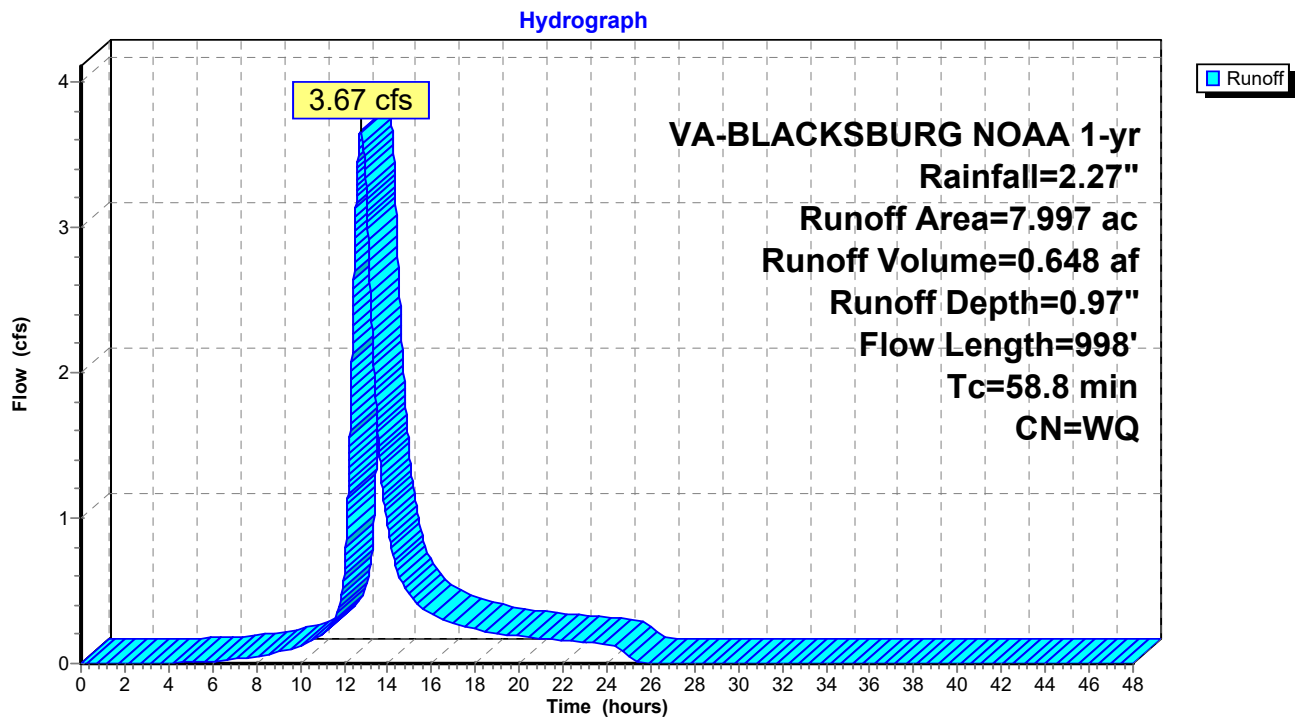
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Area (ac)	CN	Description
0.451	61	>75% Grass cover, Good, HSG B
1.433	74	>75% Grass cover, Good, HSG C
0.923	55	Woods, Good, HSG B
0.285	70	Woods, Good, HSG C
0.164	70	1/2 acre lots, 25% imp, HSG B
0.371	80	1/2 acre lots, 25% imp, HSG C
0.282	75	1/4 acre lots, 38% imp, HSG B
0.496	83	1/4 acre lots, 38% imp, HSG C
0.044	85	1/8 acre lots, 65% imp, HSG B
0.685	92	Urban commercial, 85% imp, HSG B
2.402	94	Urban commercial, 85% imp, HSG C
0.047	98	Paved roads w/curbs & sewers, HSG B
0.209	98	Paved roads w/curbs & sewers, HSG C
0.104	98	Paved parking, HSG B
0.101	98	Paved parking, HSG C
7.997		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
49.6	150	0.0267	0.05		<b>Sheet Flow, Tc1</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
7.4	440	0.0398	1.00		<b>Shallow Concentrated Flow, Tc2</b> Woodland Kv= 5.0 fps
1.8	408	0.0564	3.82		<b>Shallow Concentrated Flow, Tc3</b> Unpaved Kv= 16.1 fps
58.8	998	Total			

## Subcatchment 1S: DA #1



**Summary for Subcatchment 2S: AREA DRAINING TO EX-1**

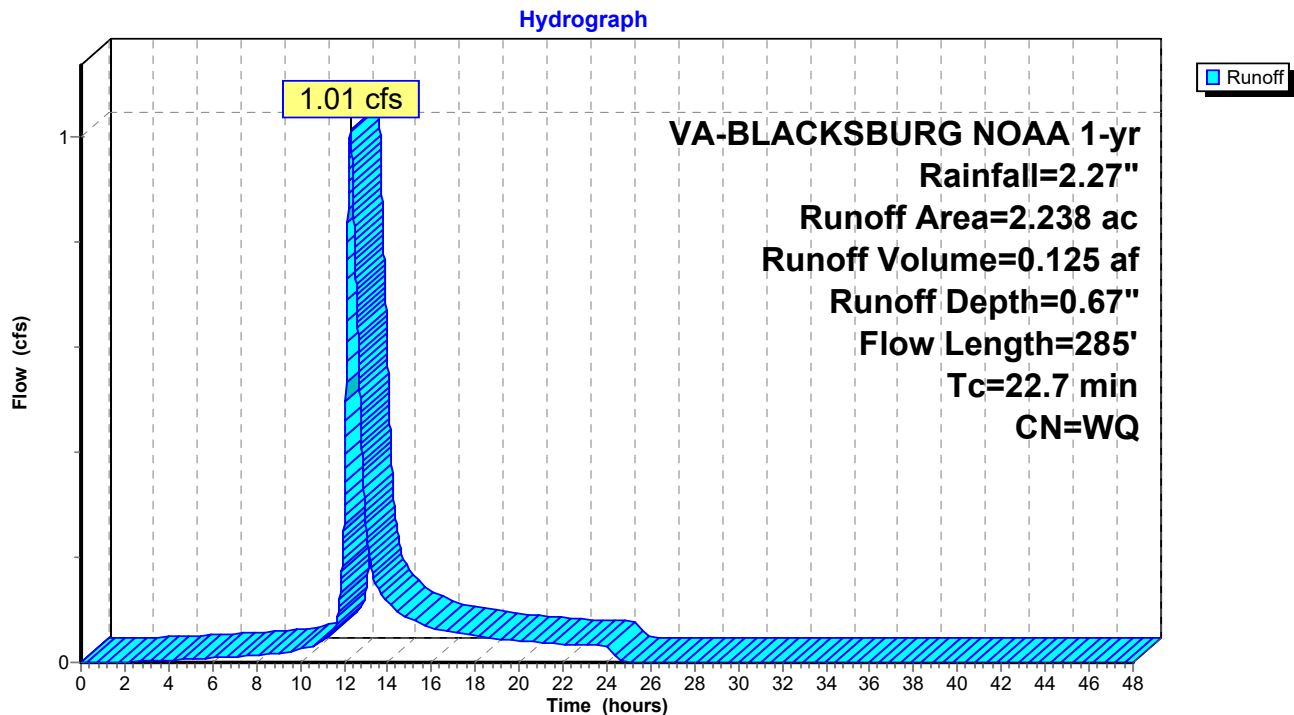
Runoff = 1.01 cfs @ 12.29 hrs, Volume= 0.125 af, Depth= 0.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Area (ac)	CN	Description
1.017	74	>75% Grass cover, Good, HSG C
0.005	55	Woods, Good, HSG B
0.872	70	Woods, Good, HSG C
0.285	98	Paved roads w/curbs & sewers, HSG C
0.059	98	Paved parking, HSG C
2.238		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.8	60	0.0333	0.05		<b>Sheet Flow, Tc4</b>
					Woods: Dense underbrush n= 0.800 P2= 2.76"
0.9	225	0.0711	4.29		<b>Shallow Concentrated Flow, Tc5</b>
					Unpaved Kv= 16.1 fps
22.7	285	Total			

**Subcatchment 2S: AREA DRAINING TO EX-1**

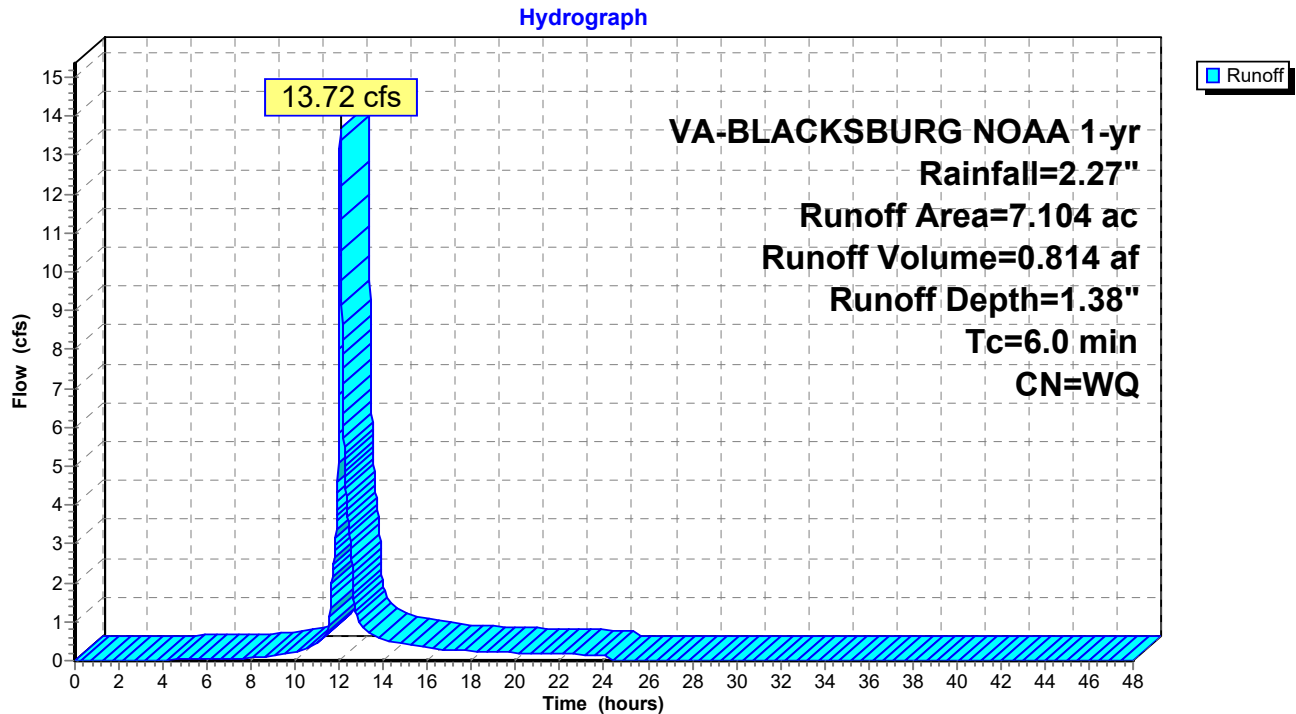
**Summary for Subcatchment 3S: AREA BYPASSING EX-1**

Runoff = 13.72 cfs @ 12.04 hrs, Volume= 0.814 af, Depth= 1.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Area (ac)	CN	Description
0.106	61	>75% Grass cover, Good, HSG B
0.044	74	>75% Grass cover, Good, HSG C
0.076	55	Woods, Good, HSG B
0.287	70	Woods, Good, HSG C
0.326	85	1/8 acre lots, 65% imp, HSG B
4.881	90	1/8 acre lots, 65% imp, HSG C
0.028	98	Paved roads w/curbs & sewers, HSG B
1.356	98	Paved parking, HSG C
7.104		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 3S: AREA BYPASSING EX-1**

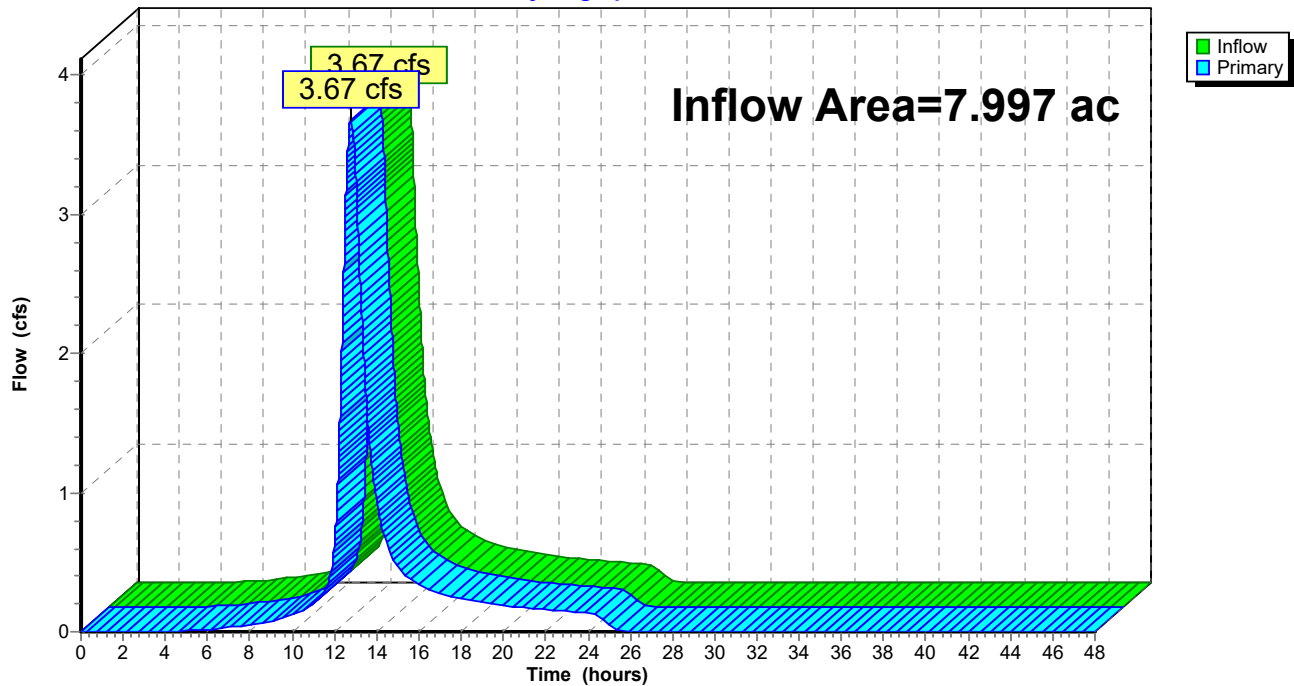
**Summary for Link 1L: POA #1**

Inflow Area = 7.997 ac, Inflow Depth = 0.97" for 1-yr event  
Inflow = 3.67 cfs @ 12.75 hrs, Volume= 0.648 af  
Primary = 3.67 cfs @ 12.75 hrs, Volume= 0.648 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 1L: POA #1**

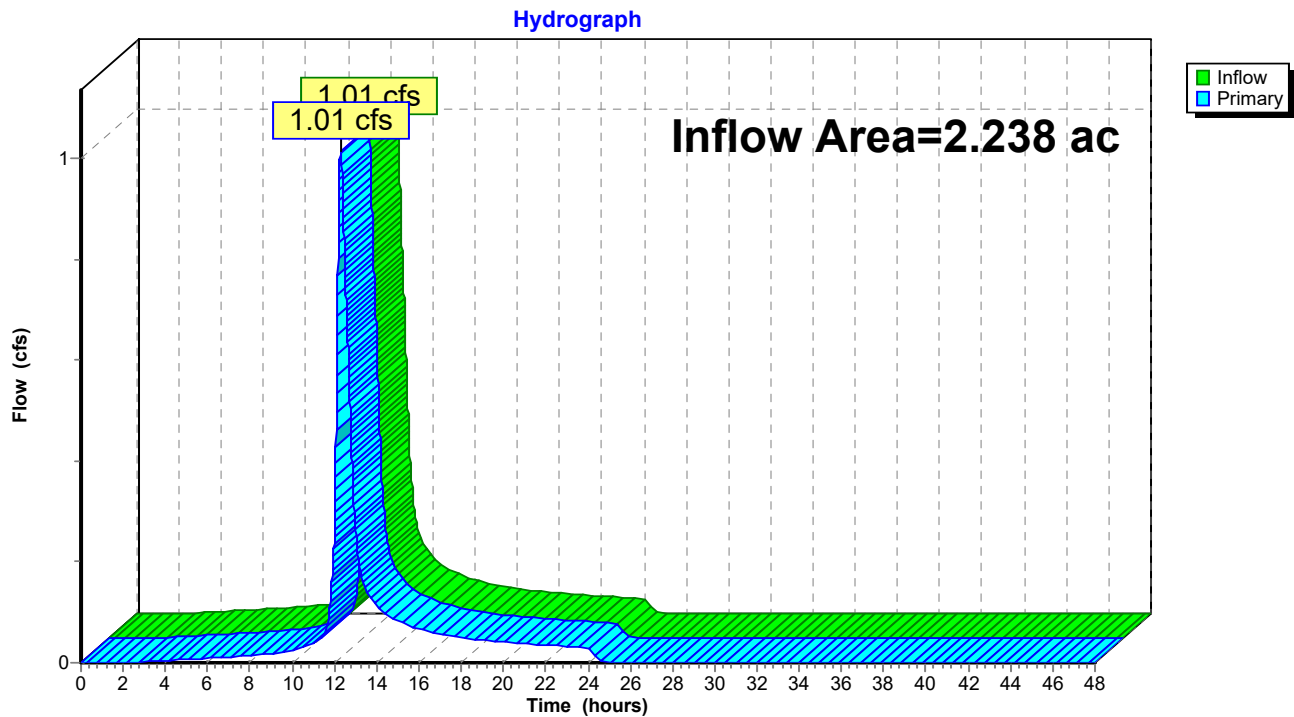
Hydrograph



**Summary for Link 2L: EX-1**

Inflow Area = 2.238 ac, Inflow Depth = 0.67" for 1-yr event  
Inflow = 1.01 cfs @ 12.29 hrs, Volume= 0.125 af  
Primary = 1.01 cfs @ 12.29 hrs, Volume= 0.125 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 2L: EX-1**

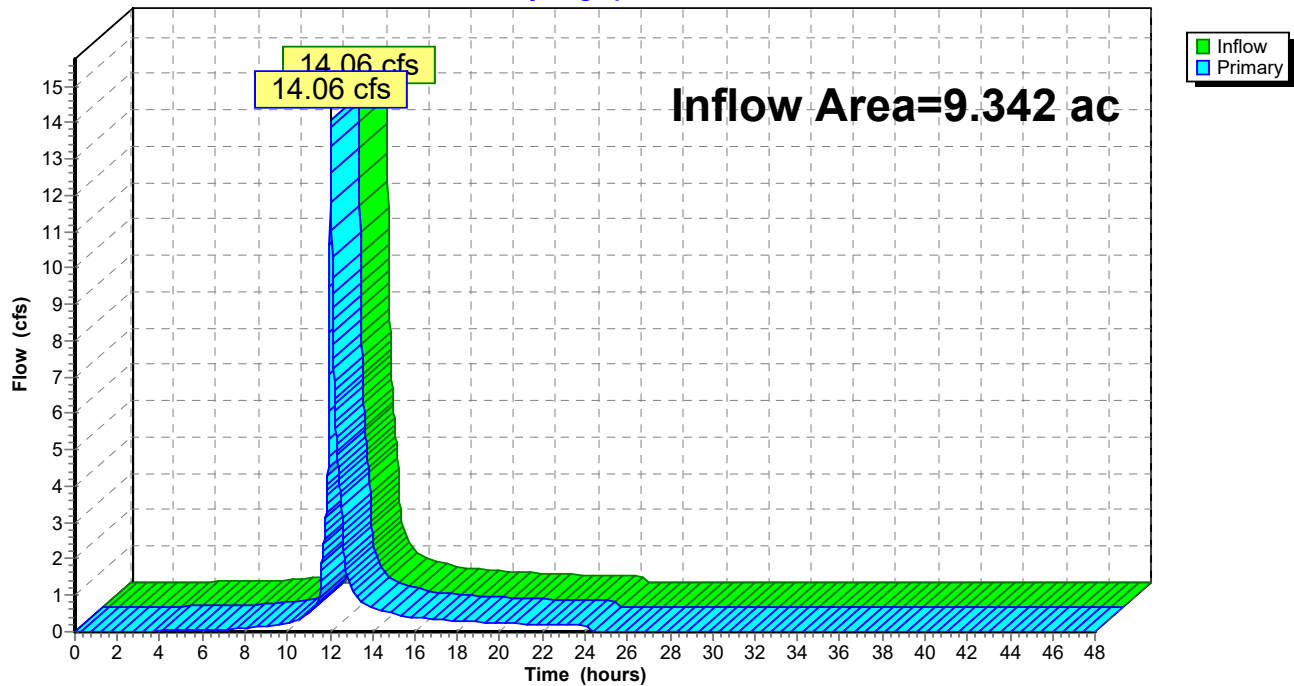
**Summary for Link 3L: POA #2**

Inflow Area = 9.342 ac, Inflow Depth = 1.21" for 1-yr event  
Inflow = 14.06 cfs @ 12.04 hrs, Volume= 0.939 af  
Primary = 14.06 cfs @ 12.04 hrs, Volume= 0.939 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 3L: POA #2**

Hydrograph



**PRE DEV**

VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q  
Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

**Subcatchment1S: DA #1**

Runoff Area=7.997 ac Runoff Depth=1.30"  
Flow Length=998' Tc=58.8 min CN=WQ Runoff=4.96 cfs 0.870 af

**Subcatchment2S: AREA DRAINING TO EX-1**

Runoff Area=2.238 ac Runoff Depth=0.96"  
Flow Length=285' Tc=22.7 min CN=WQ Runoff=1.55 cfs 0.178 af

**Subcatchment3S: AREA BYPASSING EX-1**

Runoff Area=7.104 ac Runoff Depth=1.79"  
Tc=6.0 min CN=WQ Runoff=17.83 cfs 1.062 af

**Link 1L: POA #1**

Inflow=4.96 cfs 0.870 af  
Primary=4.96 cfs 0.870 af

**Link 2L: EX-1**

Inflow=1.55 cfs 0.178 af  
Primary=1.55 cfs 0.178 af

**Link 3L: POA #2**

Inflow=18.37 cfs 1.241 af  
Primary=18.37 cfs 1.241 af

**Total Runoff Area = 17.339 ac Runoff Volume = 2.110 af Average Runoff Depth = 1.46"**



**PRE DEV**

VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

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**Summary for Subcatchment 1S: DA #1**

Runoff = 4.96 cfs @ 12.75 hrs, Volume= 0.870 af, Depth= 1.30"

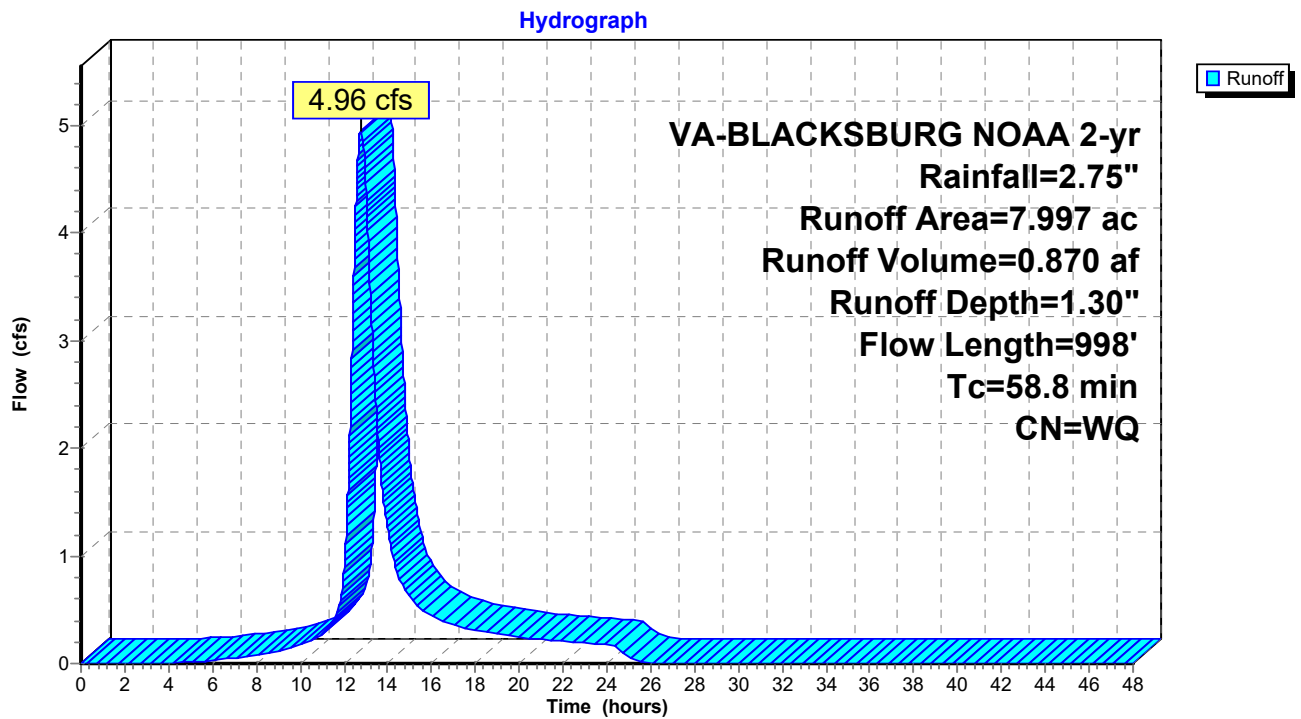
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

Area (ac)	CN	Description
0.451	61	>75% Grass cover, Good, HSG B
1.433	74	>75% Grass cover, Good, HSG C
0.923	55	Woods, Good, HSG B
0.285	70	Woods, Good, HSG C
0.164	70	1/2 acre lots, 25% imp, HSG B
0.371	80	1/2 acre lots, 25% imp, HSG C
0.282	75	1/4 acre lots, 38% imp, HSG B
0.496	83	1/4 acre lots, 38% imp, HSG C
0.044	85	1/8 acre lots, 65% imp, HSG B
0.685	92	Urban commercial, 85% imp, HSG B
2.402	94	Urban commercial, 85% imp, HSG C
0.047	98	Paved roads w/curbs & sewers, HSG B
0.209	98	Paved roads w/curbs & sewers, HSG C
0.104	98	Paved parking, HSG B
0.101	98	Paved parking, HSG C
7.997		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
49.6	150	0.0267	0.05		<b>Sheet Flow, Tc1</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
7.4	440	0.0398	1.00		<b>Shallow Concentrated Flow, Tc2</b> Woodland Kv= 5.0 fps
1.8	408	0.0564	3.82		<b>Shallow Concentrated Flow, Tc3</b> Unpaved Kv= 16.1 fps
58.8	998	Total			

## Subcatchment 1S: DA #1



**Summary for Subcatchment 2S: AREA DRAINING TO EX-1**

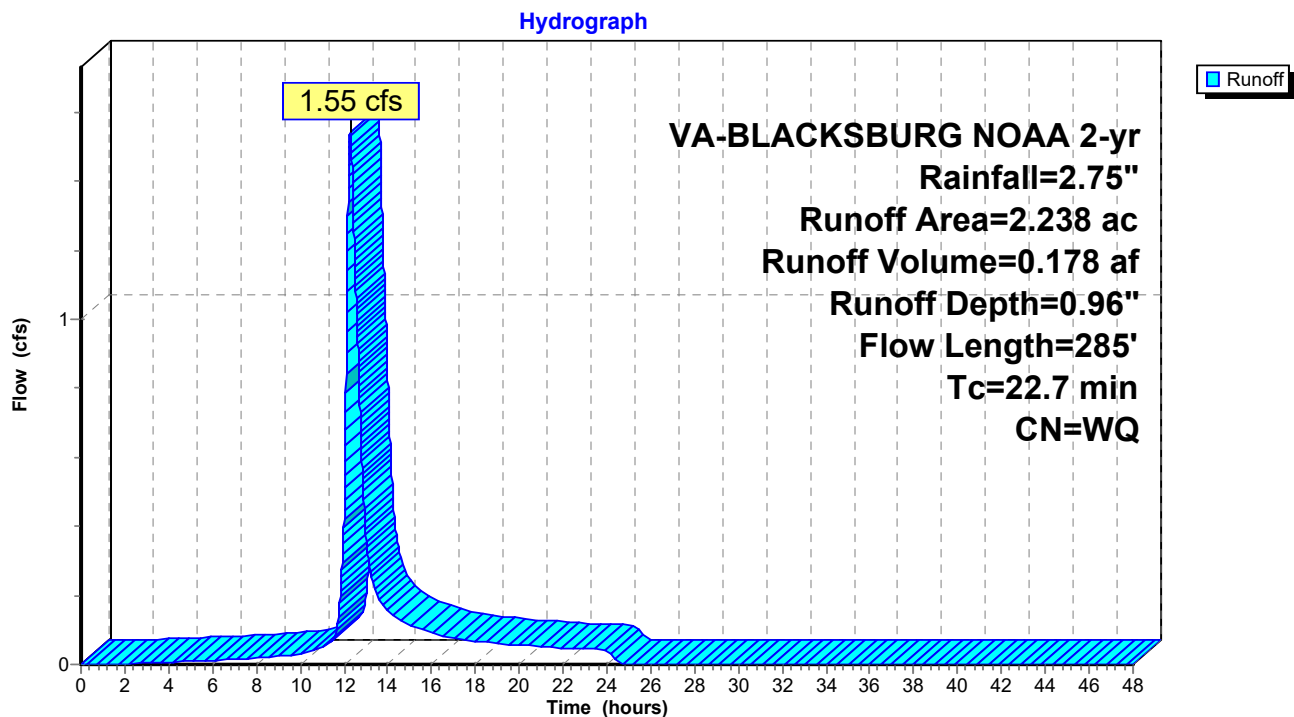
Runoff = 1.55 cfs @ 12.29 hrs, Volume= 0.178 af, Depth= 0.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

Area (ac)	CN	Description
1.017	74	>75% Grass cover, Good, HSG C
0.005	55	Woods, Good, HSG B
0.872	70	Woods, Good, HSG C
0.285	98	Paved roads w/curbs & sewers, HSG C
0.059	98	Paved parking, HSG C
2.238		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.8	60	0.0333	0.05		<b>Sheet Flow, Tc4</b>
					Woods: Dense underbrush n= 0.800 P2= 2.76"
0.9	225	0.0711	4.29		<b>Shallow Concentrated Flow, Tc5</b>
					Unpaved Kv= 16.1 fps
22.7	285	Total			

**Subcatchment 2S: AREA DRAINING TO EX-1**

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VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

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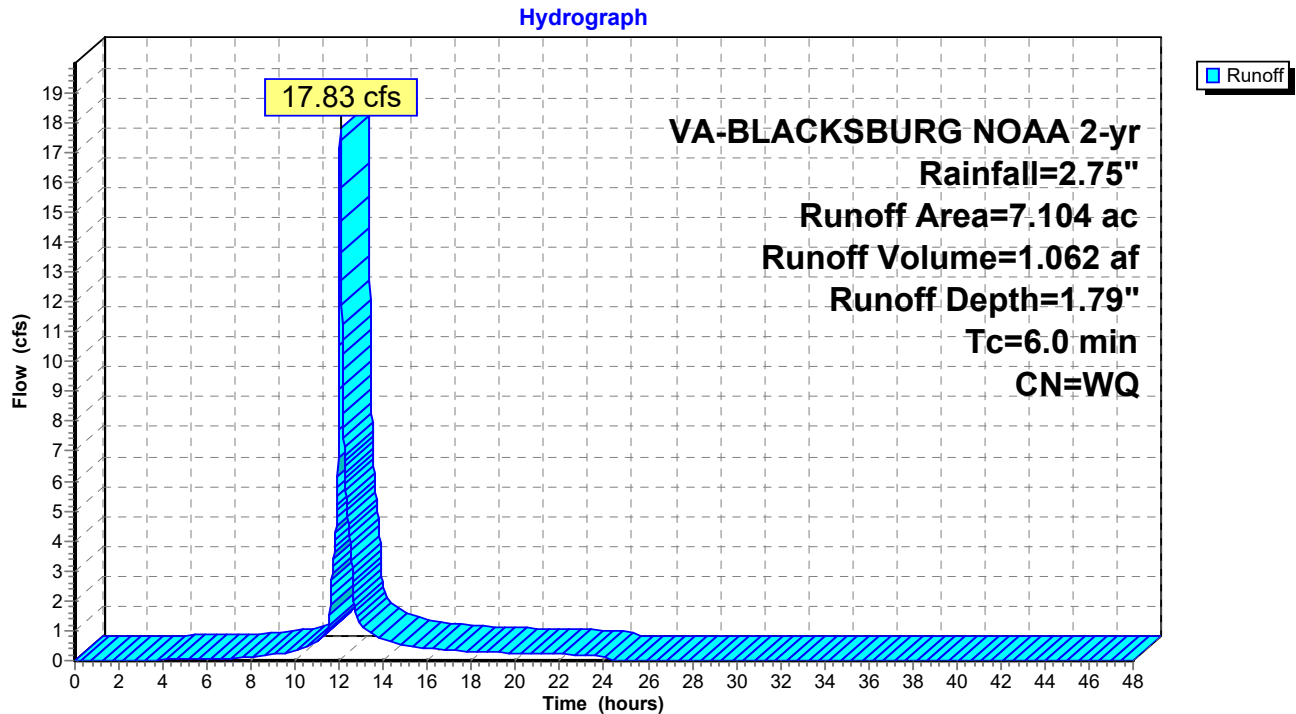
**Summary for Subcatchment 3S: AREA BYPASSING EX-1**

Runoff = 17.83 cfs @ 12.04 hrs, Volume= 1.062 af, Depth= 1.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

Area (ac)	CN	Description
0.106	61	>75% Grass cover, Good, HSG B
0.044	74	>75% Grass cover, Good, HSG C
0.076	55	Woods, Good, HSG B
0.287	70	Woods, Good, HSG C
0.326	85	1/8 acre lots, 65% imp, HSG B
4.881	90	1/8 acre lots, 65% imp, HSG C
0.028	98	Paved roads w/curbs & sewers, HSG B
1.356	98	Paved parking, HSG C
7.104		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 3S: AREA BYPASSING EX-1**

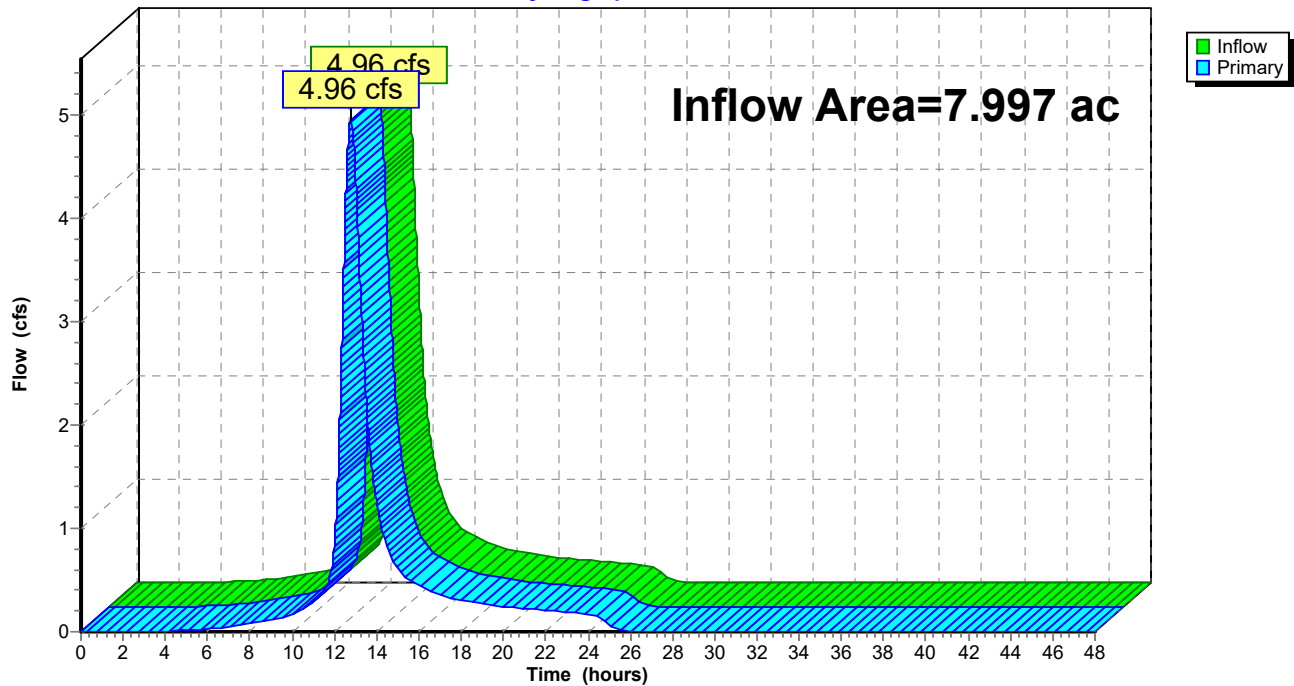
**Summary for Link 1L: POA #1**

Inflow Area = 7.997 ac, Inflow Depth = 1.30" for 2-yr event  
Inflow = 4.96 cfs @ 12.75 hrs, Volume= 0.870 af  
Primary = 4.96 cfs @ 12.75 hrs, Volume= 0.870 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 1L: POA #1**

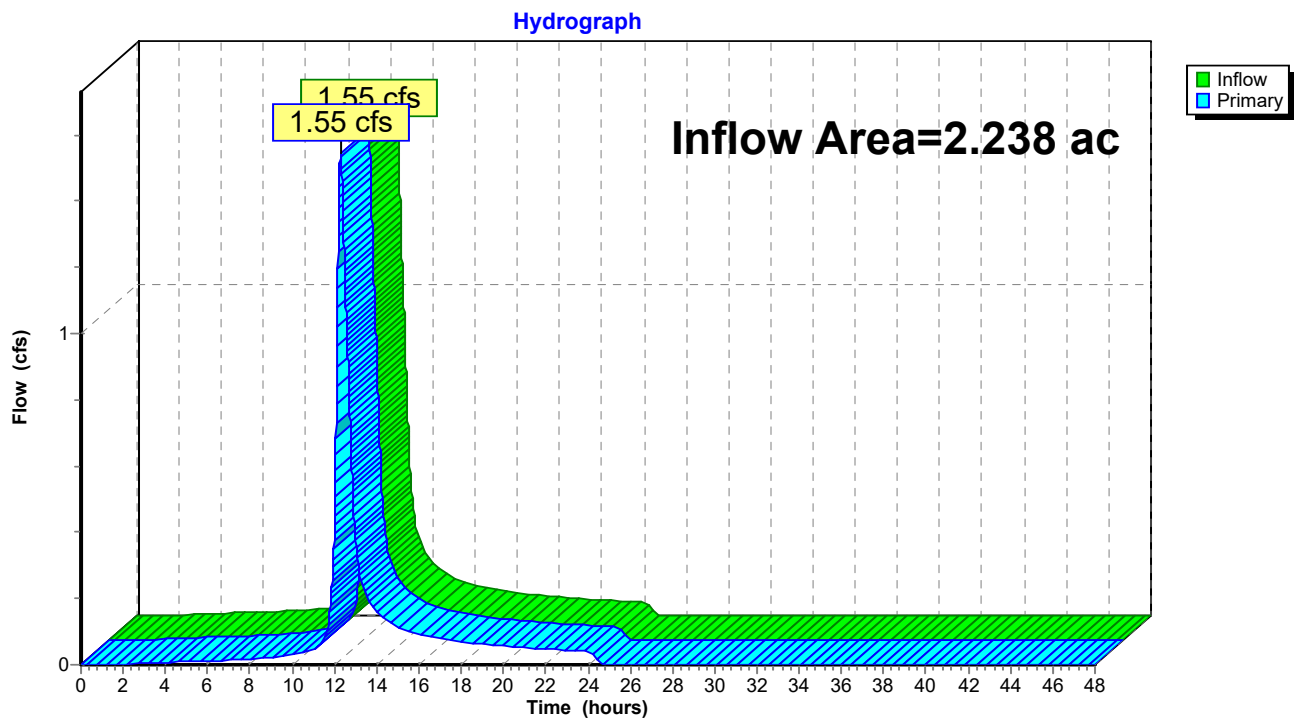
Hydrograph



**Summary for Link 2L: EX-1**

Inflow Area = 2.238 ac, Inflow Depth = 0.96" for 2-yr event  
Inflow = 1.55 cfs @ 12.29 hrs, Volume= 0.178 af  
Primary = 1.55 cfs @ 12.29 hrs, Volume= 0.178 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 2L: EX-1**

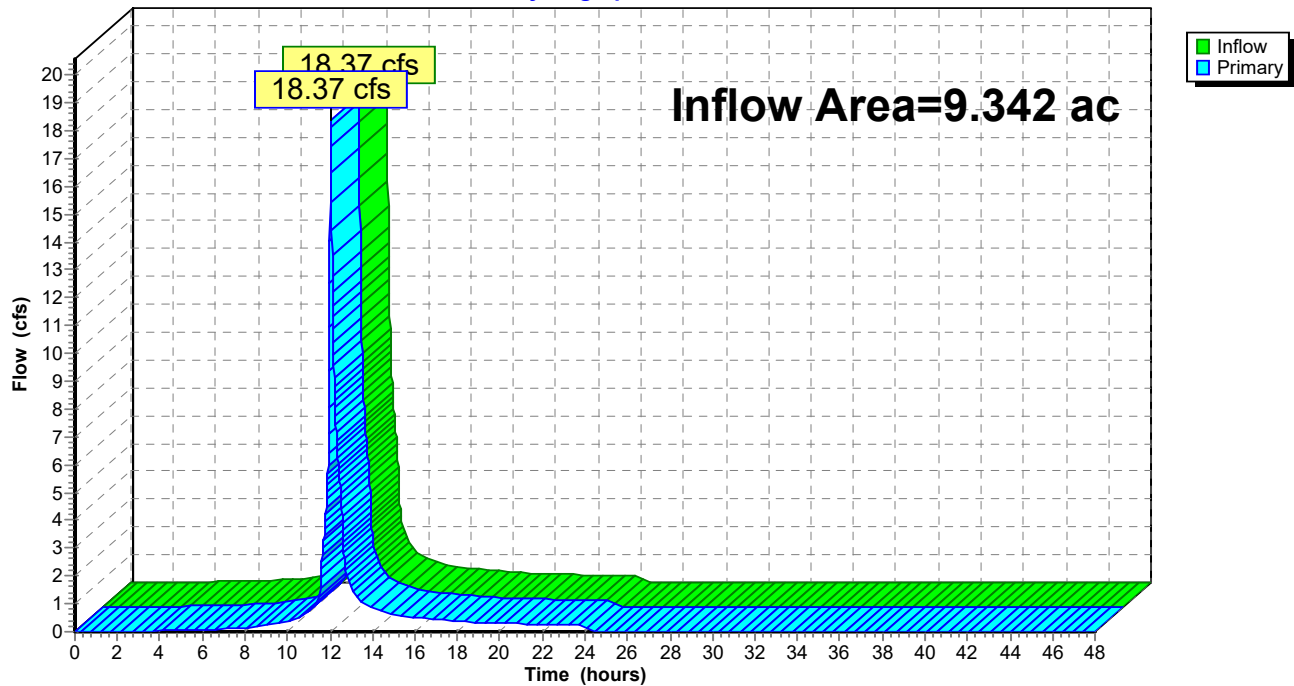
**Summary for Link 3L: POA #2**

Inflow Area = 9.342 ac, Inflow Depth = 1.59" for 2-yr event  
Inflow = 18.37 cfs @ 12.04 hrs, Volume= 1.241 af  
Primary = 18.37 cfs @ 12.04 hrs, Volume= 1.241 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 3L: POA #2**

Hydrograph



**PRE DEV**

VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q  
Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

**Subcatchment1S: DA #1**

Runoff Area=7.997 ac Runoff Depth=2.33"  
Flow Length=998' Tc=58.8 min CN=WQ Runoff=8.69 cfs 1.554 af

**Subcatchment2S: AREA DRAINING TO EX-1**

Runoff Area=2.238 ac Runoff Depth=1.89"  
Flow Length=285' Tc=22.7 min CN=WQ Runoff=3.13 cfs 0.353 af

**Subcatchment3S: AREA BYPASSING EX-1**

Runoff Area=7.104 ac Runoff Depth=3.02"  
Tc=6.0 min CN=WQ Runoff=27.19 cfs 1.786 af

**Link 1L: POA #1**

Inflow=8.69 cfs 1.554 af  
Primary=8.69 cfs 1.554 af

**Link 2L: EX-1**

Inflow=3.13 cfs 0.353 af  
Primary=3.13 cfs 0.353 af

**Link 3L: POA #2**

Inflow=28.51 cfs 2.139 af  
Primary=28.51 cfs 2.139 af

**Total Runoff Area = 17.339 ac Runoff Volume = 3.693 af Average Runoff Depth = 2.56"**



**PRE DEV**

VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

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**Summary for Subcatchment 1S: DA #1**

Runoff = 8.69 cfs @ 12.74 hrs, Volume= 1.554 af, Depth= 2.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

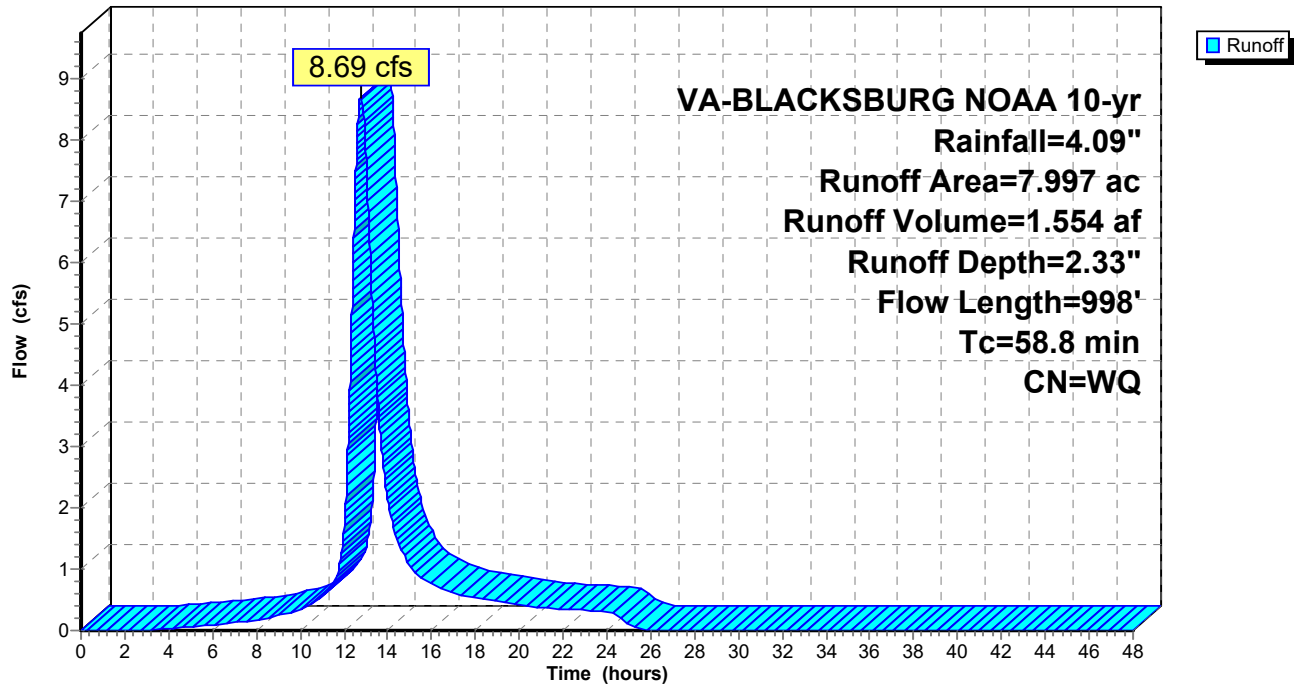
Area (ac)	CN	Description
0.451	61	>75% Grass cover, Good, HSG B
1.433	74	>75% Grass cover, Good, HSG C
0.923	55	Woods, Good, HSG B
0.285	70	Woods, Good, HSG C
0.164	70	1/2 acre lots, 25% imp, HSG B
0.371	80	1/2 acre lots, 25% imp, HSG C
0.282	75	1/4 acre lots, 38% imp, HSG B
0.496	83	1/4 acre lots, 38% imp, HSG C
0.044	85	1/8 acre lots, 65% imp, HSG B
0.685	92	Urban commercial, 85% imp, HSG B
2.402	94	Urban commercial, 85% imp, HSG C
0.047	98	Paved roads w/curbs & sewers, HSG B
0.209	98	Paved roads w/curbs & sewers, HSG C
0.104	98	Paved parking, HSG B
0.101	98	Paved parking, HSG C
7.997		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
49.6	150	0.0267	0.05		<b>Sheet Flow, Tc1</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
7.4	440	0.0398	1.00		<b>Shallow Concentrated Flow, Tc2</b> Woodland Kv= 5.0 fps
1.8	408	0.0564	3.82		<b>Shallow Concentrated Flow, Tc3</b> Unpaved Kv= 16.1 fps
58.8	998	Total			

## Subcatchment 1S: DA #1

Hydrograph



**PRE DEV**

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VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

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**Summary for Subcatchment 2S: AREA DRAINING TO EX-1**

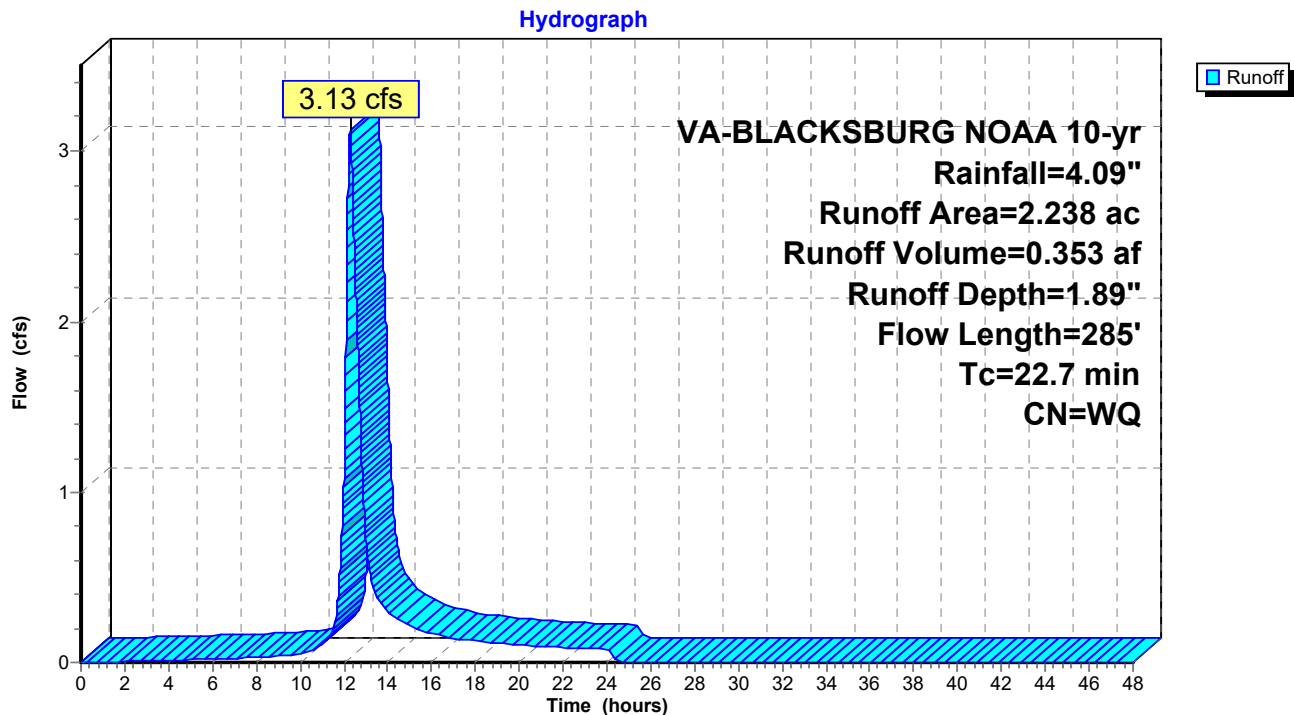
Runoff = 3.13 cfs @ 12.28 hrs, Volume= 0.353 af, Depth= 1.89"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

Area (ac)	CN	Description
1.017	74	>75% Grass cover, Good, HSG C
0.005	55	Woods, Good, HSG B
0.872	70	Woods, Good, HSG C
0.285	98	Paved roads w/curbs & sewers, HSG C
0.059	98	Paved parking, HSG C
2.238		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.8	60	0.0333	0.05		<b>Sheet Flow, Tc4</b>
					Woods: Dense underbrush n= 0.800 P2= 2.76"
0.9	225	0.0711	4.29		<b>Shallow Concentrated Flow, Tc5</b>
					Unpaved Kv= 16.1 fps
22.7	285	Total			

**Subcatchment 2S: AREA DRAINING TO EX-1**

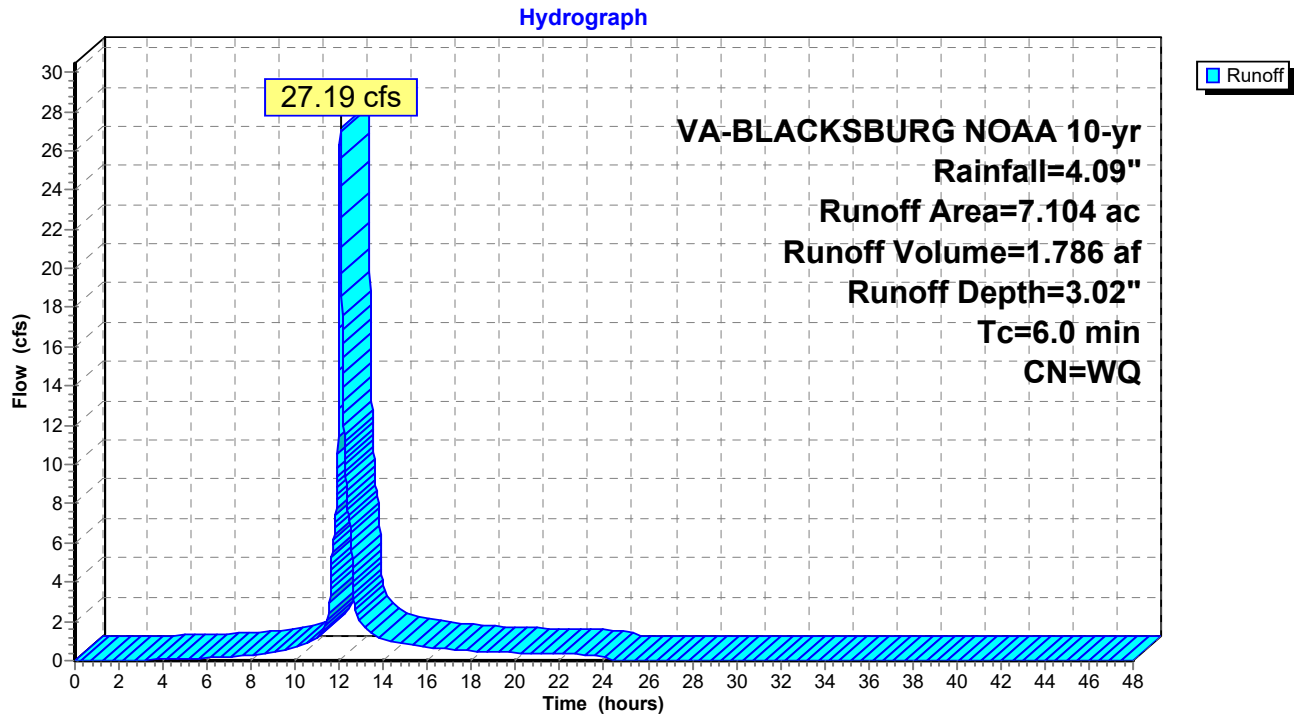
**Summary for Subcatchment 3S: AREA BYPASSING EX-1**

Runoff = 27.19 cfs @ 12.04 hrs, Volume= 1.786 af, Depth= 3.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

Area (ac)	CN	Description
0.106	61	>75% Grass cover, Good, HSG B
0.044	74	>75% Grass cover, Good, HSG C
0.076	55	Woods, Good, HSG B
0.287	70	Woods, Good, HSG C
0.326	85	1/8 acre lots, 65% imp, HSG B
4.881	90	1/8 acre lots, 65% imp, HSG C
0.028	98	Paved roads w/curbs & sewers, HSG B
1.356	98	Paved parking, HSG C
7.104		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 3S: AREA BYPASSING EX-1**

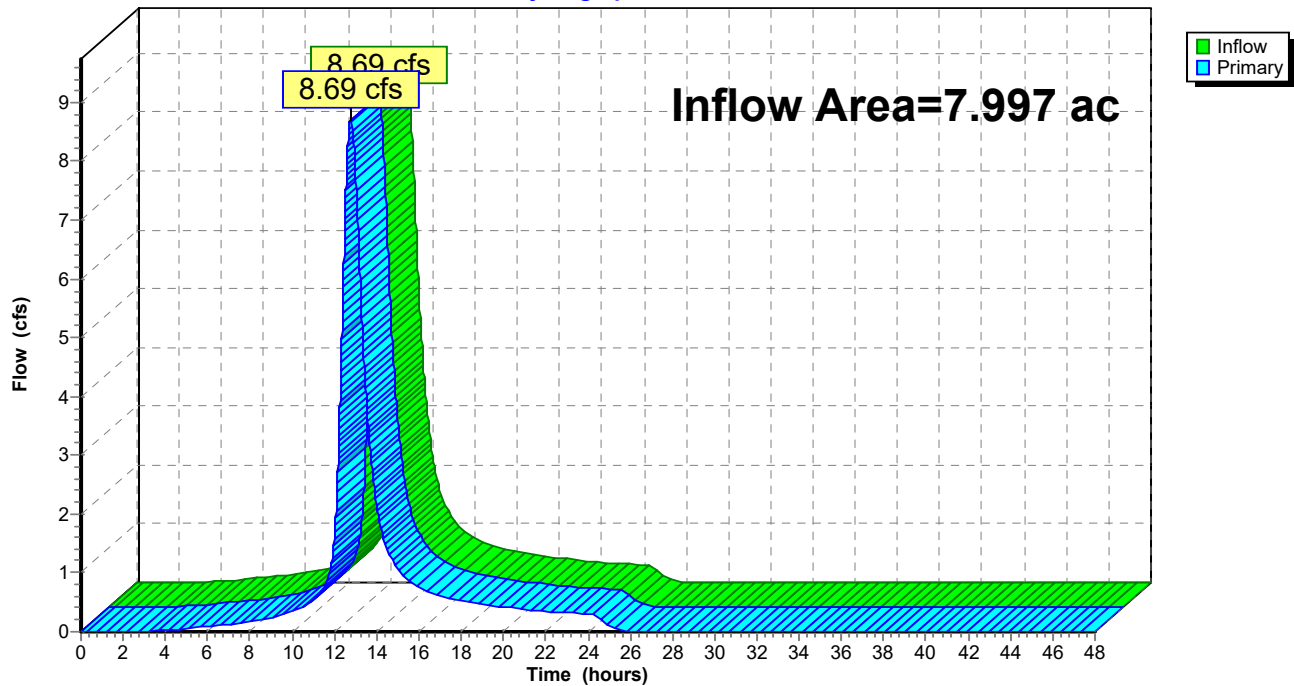
**Summary for Link 1L: POA #1**

Inflow Area = 7.997 ac, Inflow Depth = 2.33" for 10-yr event  
Inflow = 8.69 cfs @ 12.74 hrs, Volume= 1.554 af  
Primary = 8.69 cfs @ 12.74 hrs, Volume= 1.554 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 1L: POA #1**

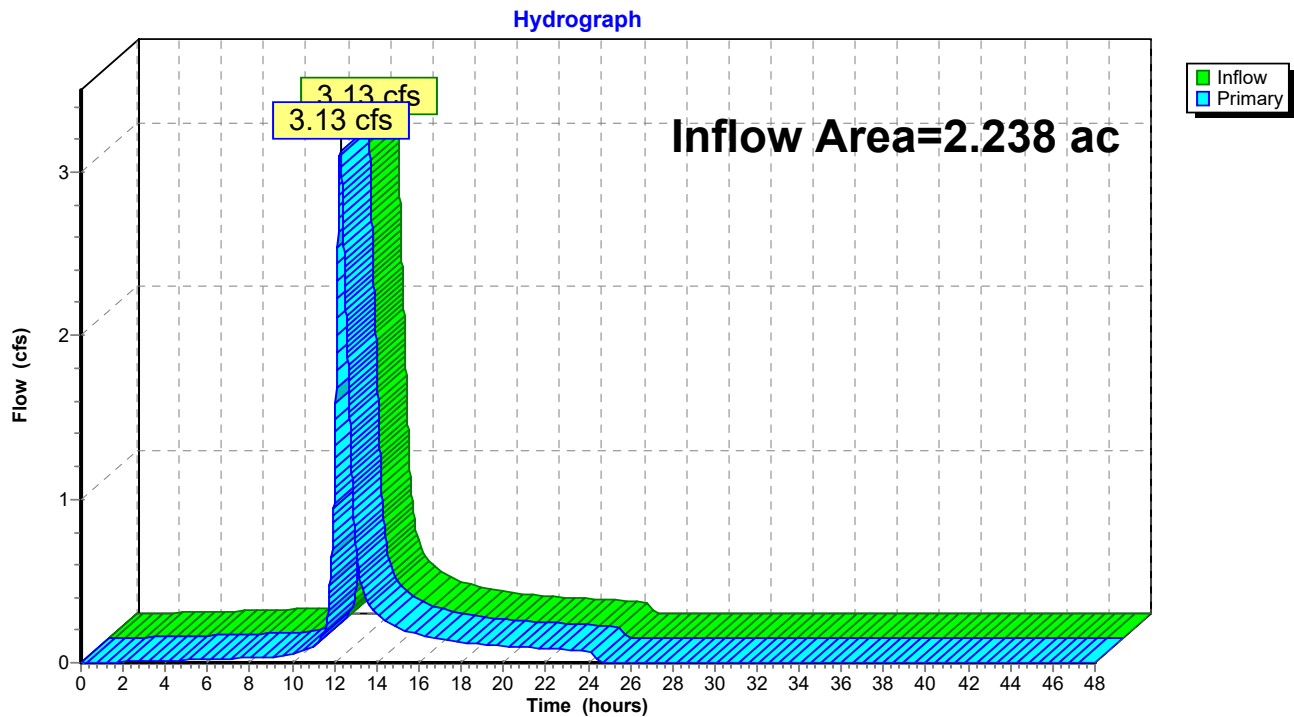
Hydrograph



**Summary for Link 2L: EX-1**

Inflow Area = 2.238 ac, Inflow Depth = 1.89" for 10-yr event  
Inflow = 3.13 cfs @ 12.28 hrs, Volume= 0.353 af  
Primary = 3.13 cfs @ 12.28 hrs, Volume= 0.353 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 2L: EX-1**

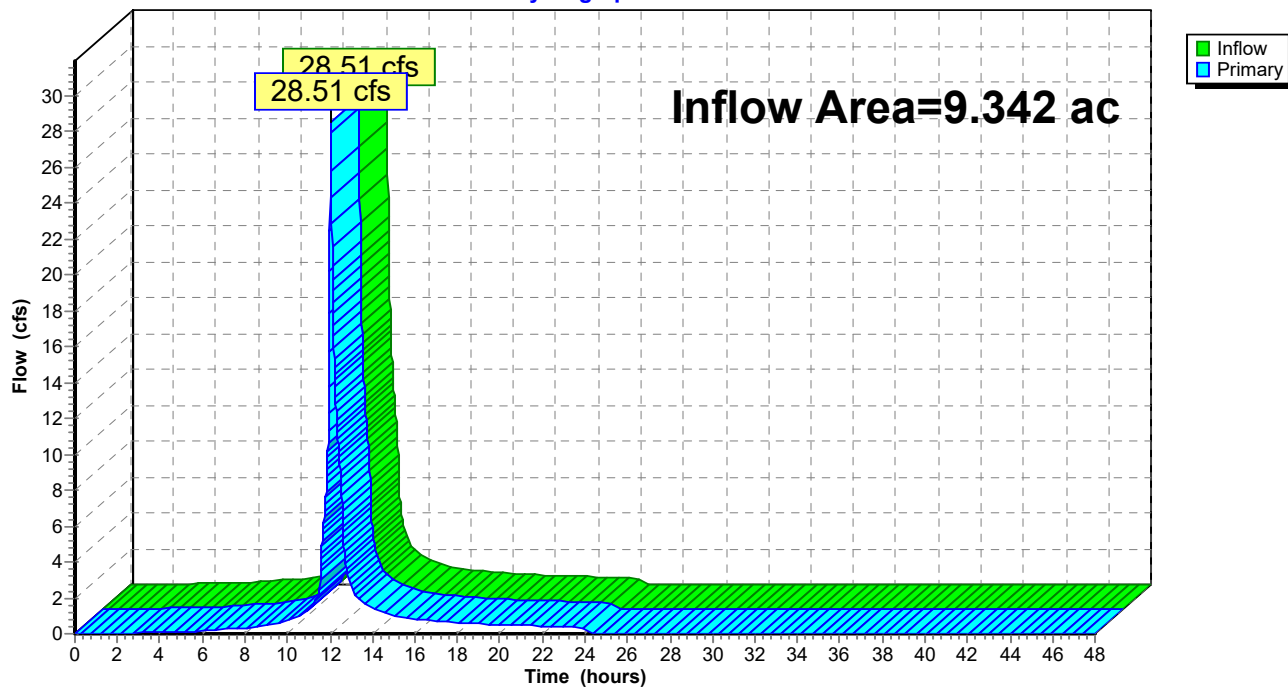
**Summary for Link 3L: POA #2**

Inflow Area = 9.342 ac, Inflow Depth = 2.75" for 10-yr event  
Inflow = 28.51 cfs @ 12.04 hrs, Volume= 2.139 af  
Primary = 28.51 cfs @ 12.04 hrs, Volume= 2.139 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 3L: POA #2**

Hydrograph



**PRE DEV**

VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q  
Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

**Subcatchment1S: DA #1**

Runoff Area=7.997 ac Runoff Depth=4.36"  
Flow Length=998' Tc=58.8 min CN=WQ Runoff=14.90 cfs 2.908 af

**Subcatchment2S: AREA DRAINING TO EX-1**

Runoff Area=2.238 ac Runoff Depth=3.84"  
Flow Length=285' Tc=22.7 min CN=WQ Runoff=5.80 cfs 0.716 af

**Subcatchment3S: AREA BYPASSING EX-1**

Runoff Area=7.104 ac Runoff Depth=5.29"  
Tc=6.0 min CN=WQ Runoff=39.62 cfs 3.132 af

**Link 1L: POA #1**

Inflow=14.90 cfs 2.908 af  
Primary=14.90 cfs 2.908 af

**Link 2L: EX-1**

Inflow=5.80 cfs 0.716 af  
Primary=5.80 cfs 0.716 af

**Link 3L: POA #2**

Inflow=42.49 cfs 3.848 af  
Primary=42.49 cfs 3.848 af

**Total Runoff Area = 17.339 ac Runoff Volume = 6.757 af Average Runoff Depth = 4.68"**



**PRE DEV**

VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

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**Summary for Subcatchment 1S: DA #1**

Runoff = 14.90 cfs @ 12.74 hrs, Volume= 2.908 af, Depth= 4.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

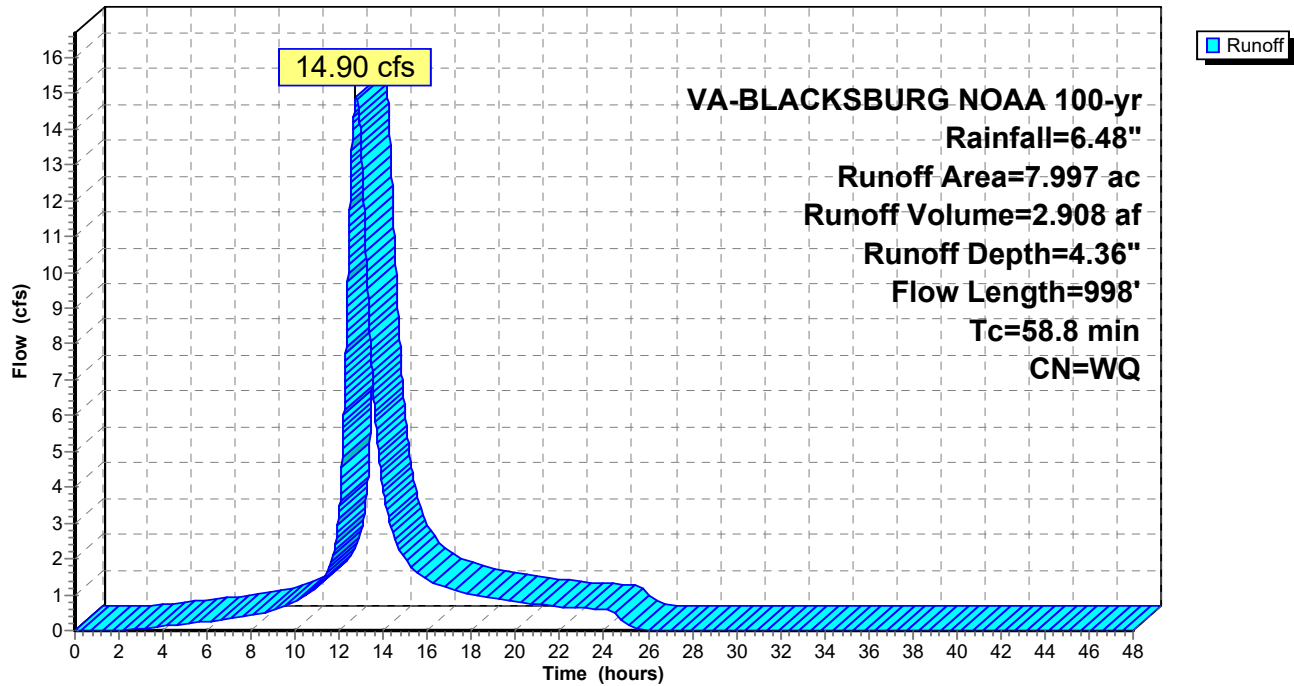
Area (ac)	CN	Description
0.451	61	>75% Grass cover, Good, HSG B
1.433	74	>75% Grass cover, Good, HSG C
0.923	55	Woods, Good, HSG B
0.285	70	Woods, Good, HSG C
0.164	70	1/2 acre lots, 25% imp, HSG B
0.371	80	1/2 acre lots, 25% imp, HSG C
0.282	75	1/4 acre lots, 38% imp, HSG B
0.496	83	1/4 acre lots, 38% imp, HSG C
0.044	85	1/8 acre lots, 65% imp, HSG B
0.685	92	Urban commercial, 85% imp, HSG B
2.402	94	Urban commercial, 85% imp, HSG C
0.047	98	Paved roads w/curbs & sewers, HSG B
0.209	98	Paved roads w/curbs & sewers, HSG C
0.104	98	Paved parking, HSG B
0.101	98	Paved parking, HSG C
7.997		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
49.6	150	0.0267	0.05		<b>Sheet Flow, Tc1</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
7.4	440	0.0398	1.00		<b>Shallow Concentrated Flow, Tc2</b> Woodland Kv= 5.0 fps
1.8	408	0.0564	3.82		<b>Shallow Concentrated Flow, Tc3</b> Unpaved Kv= 16.1 fps
58.8	998	Total			

## Subcatchment 1S: DA #1

Hydrograph



**PRE DEV**

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VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

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**Summary for Subcatchment 2S: AREA DRAINING TO EX-1**

Runoff = 5.80 cfs @ 12.28 hrs, Volume= 0.716 af, Depth= 3.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

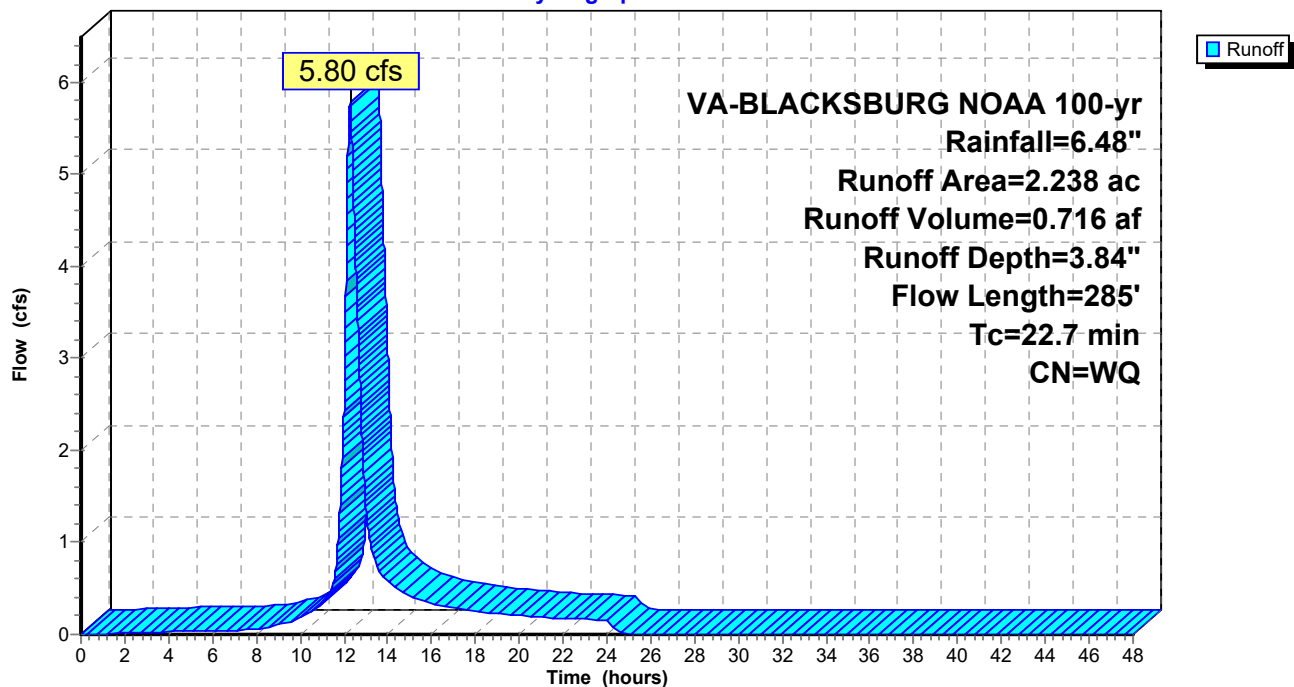
Area (ac)	CN	Description
1.017	74	>75% Grass cover, Good, HSG C
0.005	55	Woods, Good, HSG B
0.872	70	Woods, Good, HSG C
0.285	98	Paved roads w/curbs & sewers, HSG C
0.059	98	Paved parking, HSG C
2.238		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.8	60	0.0333	0.05		<b>Sheet Flow, Tc4</b>
					Woods: Dense underbrush n= 0.800 P2= 2.76"
0.9	225	0.0711	4.29		<b>Shallow Concentrated Flow, Tc5</b>
					Unpaved Kv= 16.1 fps
22.7	285	Total			

**Subcatchment 2S: AREA DRAINING TO EX-1**

Hydrograph



**PRE DEV**

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VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

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**Summary for Subcatchment 3S: AREA BYPASSING EX-1**

Runoff = 39.62 cfs @ 12.04 hrs, Volume= 3.132 af, Depth= 5.29"

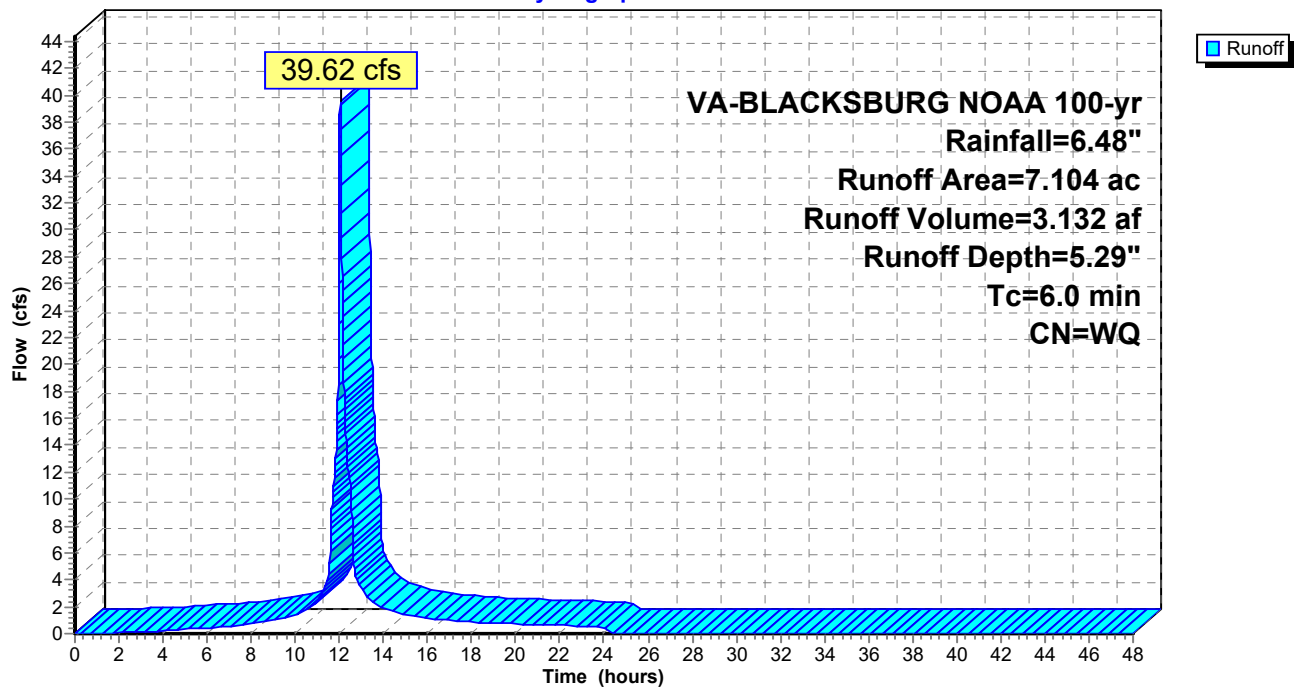
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

Area (ac)	CN	Description
0.106	61	>75% Grass cover, Good, HSG B
0.044	74	>75% Grass cover, Good, HSG C
0.076	55	Woods, Good, HSG B
0.287	70	Woods, Good, HSG C
0.326	85	1/8 acre lots, 65% imp, HSG B
4.881	90	1/8 acre lots, 65% imp, HSG C
0.028	98	Paved roads w/curbs & sewers, HSG B
1.356	98	Paved parking, HSG C
7.104		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 3S: AREA BYPASSING EX-1**

Hydrograph



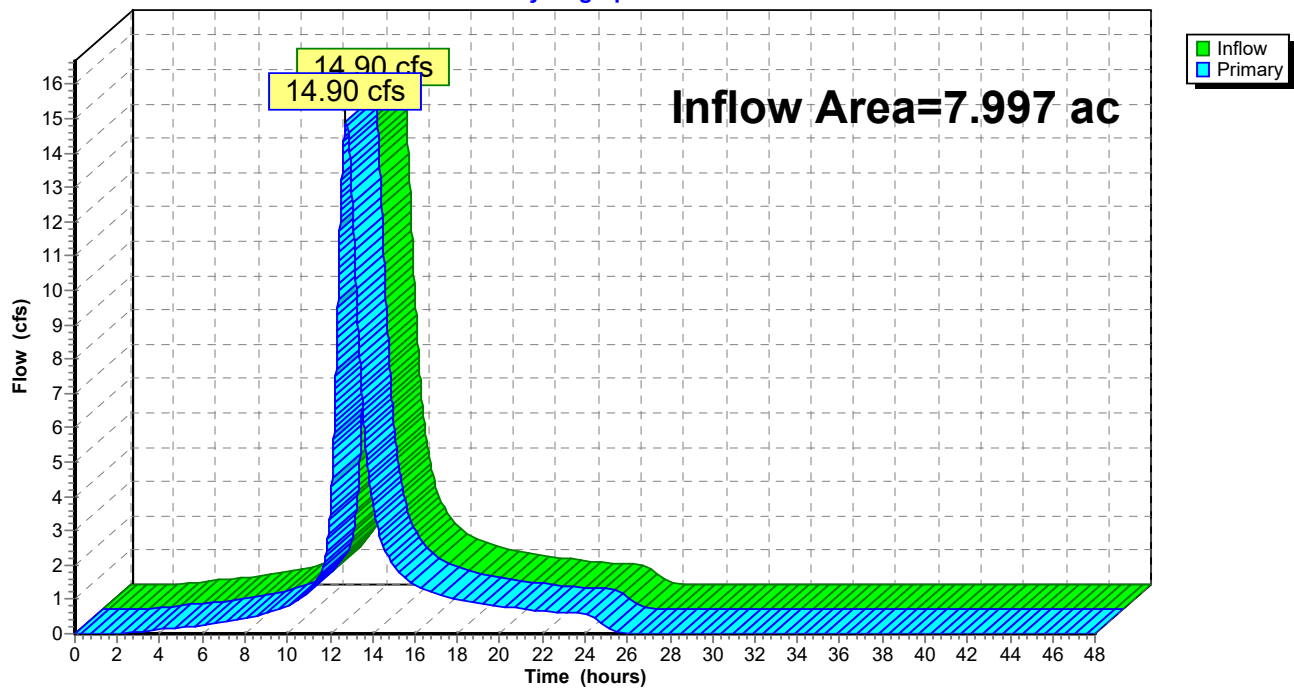
**Summary for Link 1L: POA #1**

Inflow Area = 7.997 ac, Inflow Depth = 4.36" for 100-yr event  
Inflow = 14.90 cfs @ 12.74 hrs, Volume= 2.908 af  
Primary = 14.90 cfs @ 12.74 hrs, Volume= 2.908 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 1L: POA #1**

Hydrograph



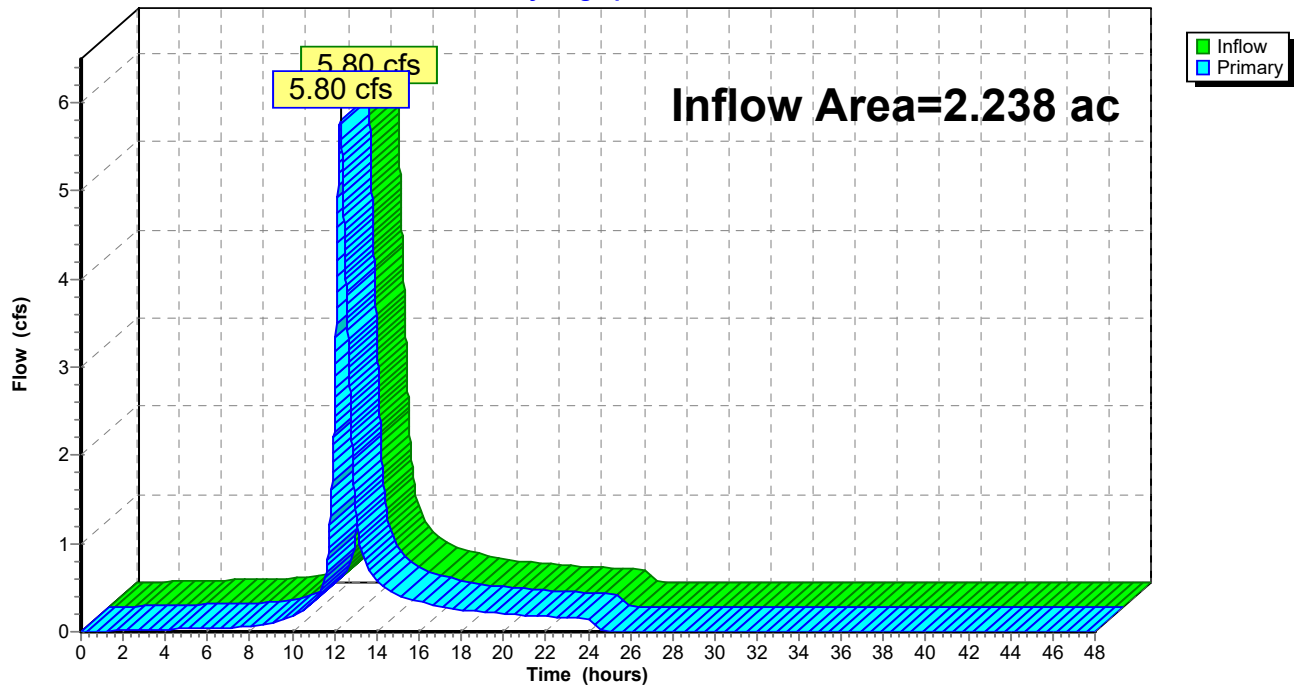
**Summary for Link 2L: EX-1**

Inflow Area = 2.238 ac, Inflow Depth = 3.84" for 100-yr event  
Inflow = 5.80 cfs @ 12.28 hrs, Volume= 0.716 af  
Primary = 5.80 cfs @ 12.28 hrs, Volume= 0.716 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 2L: EX-1**

Hydrograph



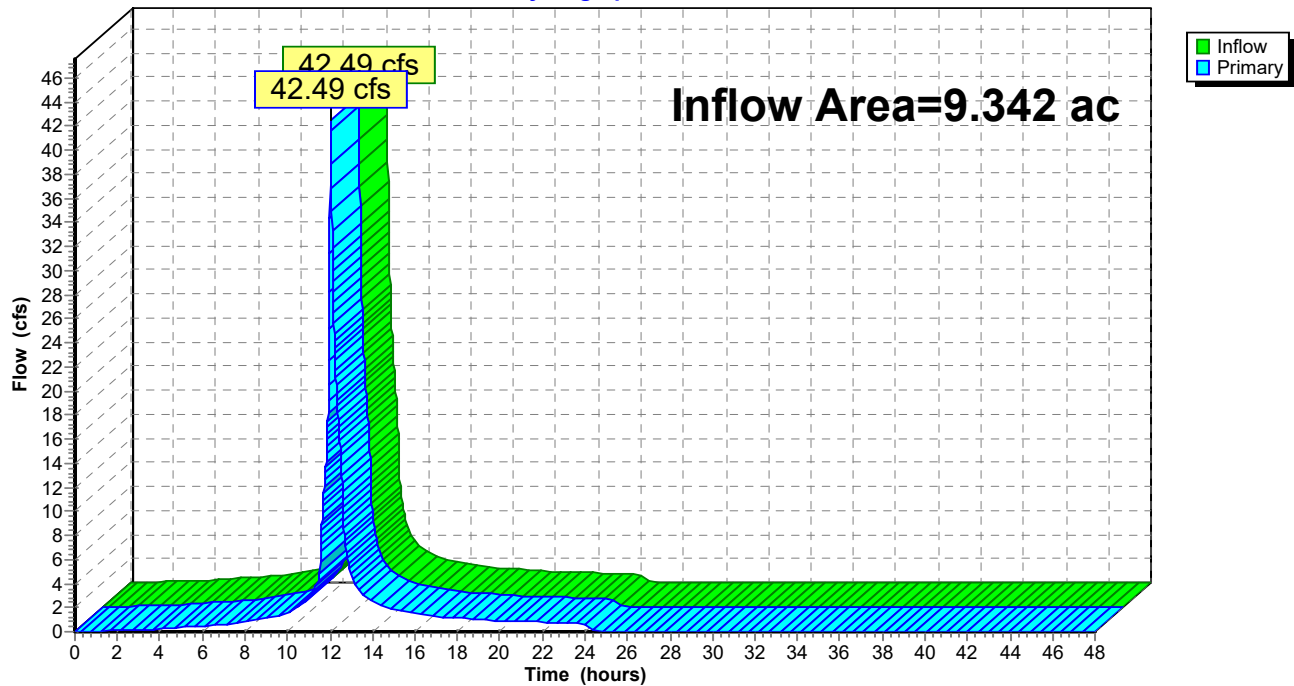
**Summary for Link 3L: POA #2**

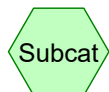
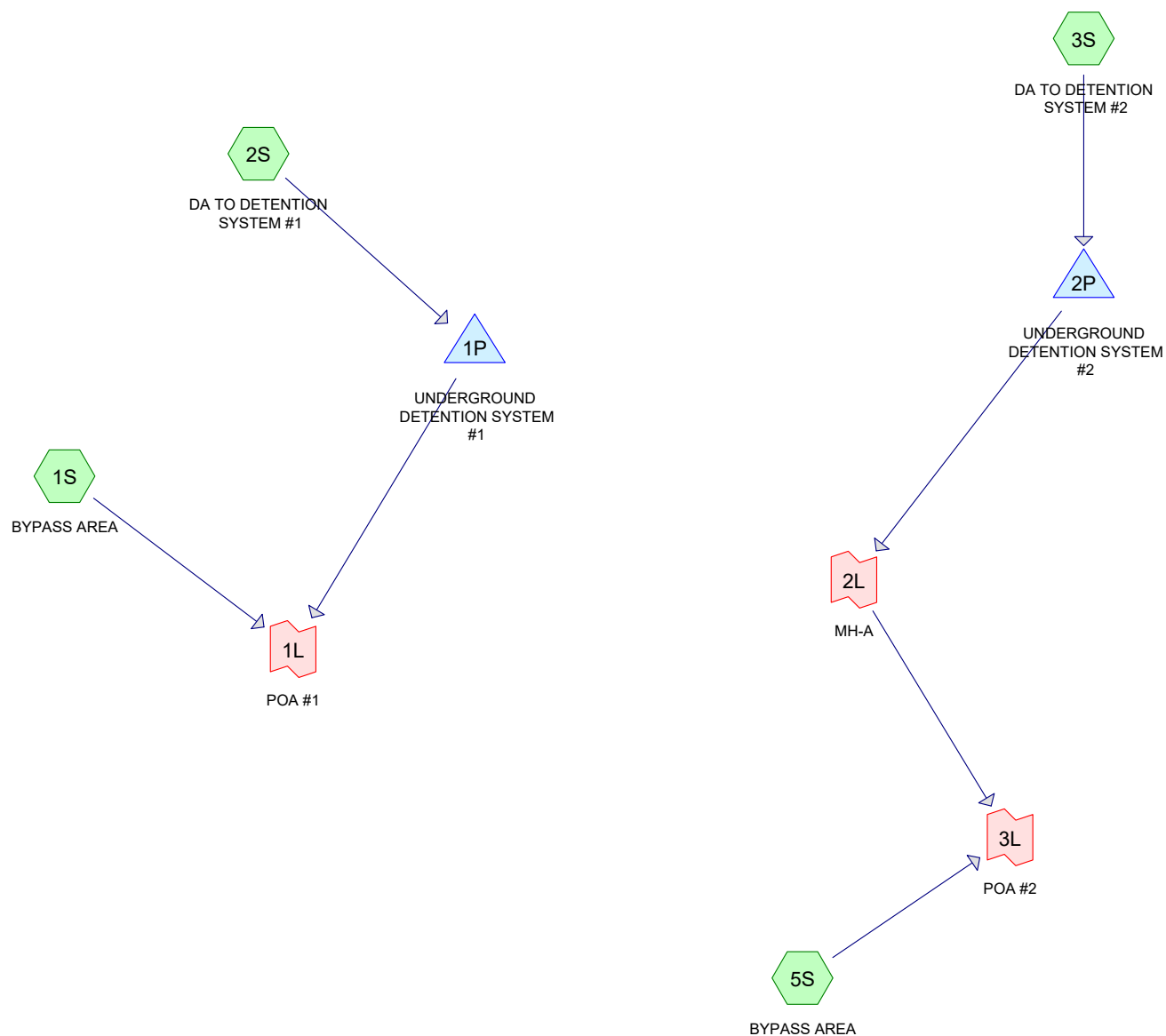
Inflow Area = 9.342 ac, Inflow Depth = 4.94" for 100-yr event  
Inflow = 42.49 cfs @ 12.04 hrs, Volume= 3.848 af  
Primary = 42.49 cfs @ 12.04 hrs, Volume= 3.848 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

**Link 3L: POA #2**

Hydrograph

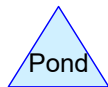




Subcat



Reach



Pond



Link

### Routing Diagram for POST DEV

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**POST DEV**

VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

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Page 2

Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q  
Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

**Subcatchment1S: BYPASS AREA**

Runoff Area=6.010 ac Runoff Depth=1.17"  
Flow Length=973' Tc=60.9 min CN=WQ Runoff=3.32 cfs 0.584 af

**Subcatchment2S: DA TO DETENTION SYSTEM #1**

Runoff Area=2.266 ac Runoff Depth=1.62"  
Tc=6.0 min CN=WQ Runoff=4.82 cfs 0.306 af

**Subcatchment3S: DA TO DETENTION SYSTEM #2**

Runoff Area=2.268 ac Runoff Depth=1.44"  
Tc=6.0 min CN=WQ Runoff=4.28 cfs 0.273 af

**Subcatchment5S: BYPASS AREA**

Runoff Area=6.766 ac Runoff Depth=1.44"  
Tc=6.0 min CN=WQ Runoff=13.70 cfs 0.810 af

**Pond 1P: UNDERGROUND DETENTION**

Peak Elev=2,159.90' Storage=0.210 af Inflow=4.82 cfs 0.306 af  
Outflow=0.13 cfs 0.228 af

**Pond 2P: UNDERGROUND DETENTION**

Peak Elev=2,157.10' Storage=0.158 af Inflow=4.28 cfs 0.273 af  
Outflow=0.12 cfs 0.273 af

**Link 1L: POA #1**

Inflow=3.39 cfs 0.812 af  
Primary=3.39 cfs 0.812 af

**Link 2L: MH-A**

Inflow=0.12 cfs 0.273 af  
Primary=0.12 cfs 0.273 af

**Link 3L: POA #2**

Inflow=13.79 cfs 1.083 af  
Primary=13.79 cfs 1.083 af

**Total Runoff Area = 17.310 ac Runoff Volume = 1.973 af Average Runoff Depth = 1.37"**

**POST DEV**

VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

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**Summary for Subcatchment 1S: BYPASS AREA**

Runoff = 3.32 cfs @ 12.79 hrs, Volume= 0.584 af, Depth= 1.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Area (ac)	CN	Description
0.433	61	>75% Grass cover, Good, HSG B
0.407	74	>75% Grass cover, Good, HSG C
0.270	55	Woods, Good, HSG B
0.076	70	Woods, Good, HSG C
0.164	70	1/2 acre lots, 25% imp, HSG B
0.371	80	1/2 acre lots, 25% imp, HSG C
0.282	75	1/4 acre lots, 38% imp, HSG B
0.496	83	1/4 acre lots, 38% imp, HSG C
0.044	85	1/8 acre lots, 65% imp, HSG B
0.685	92	Urban commercial, 85% imp, HSG B
2.402	94	Urban commercial, 85% imp, HSG C
0.047	98	Paved roads w/curbs & sewers, HSG B
0.209	98	Paved roads w/curbs & sewers, HSG C
0.068	98	Paved parking, HSG B
0.056	98	Paved parking, HSG C
6.010		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
52.4	150	0.0233	0.05		<b>Sheet Flow, Tc1</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
6.7	415	0.0422	1.03		<b>Shallow Concentrated Flow, Tc2</b> Woodland Kv= 5.0 fps
1.8	408	0.0564	3.82		<b>Shallow Concentrated Flow, Tc3</b> Unpaved Kv= 16.1 fps
60.9	973	Total			

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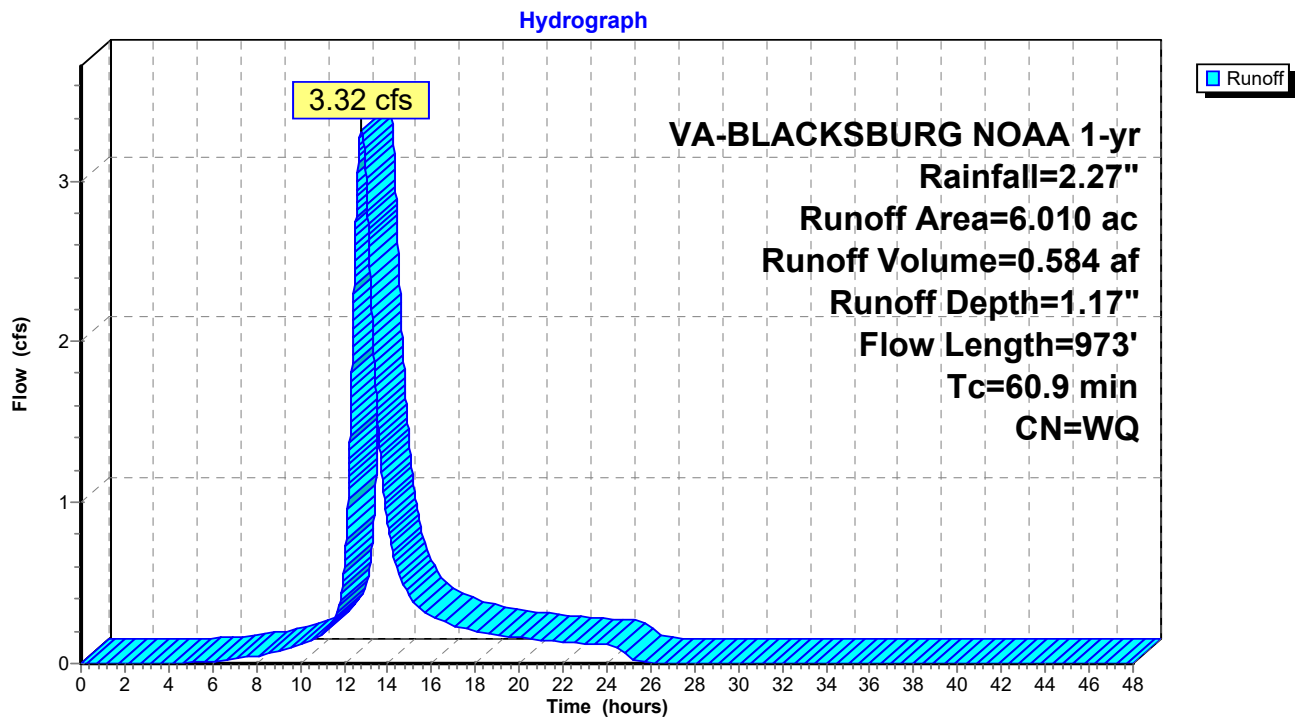
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## Subcatchment 1S: BYPASS AREA



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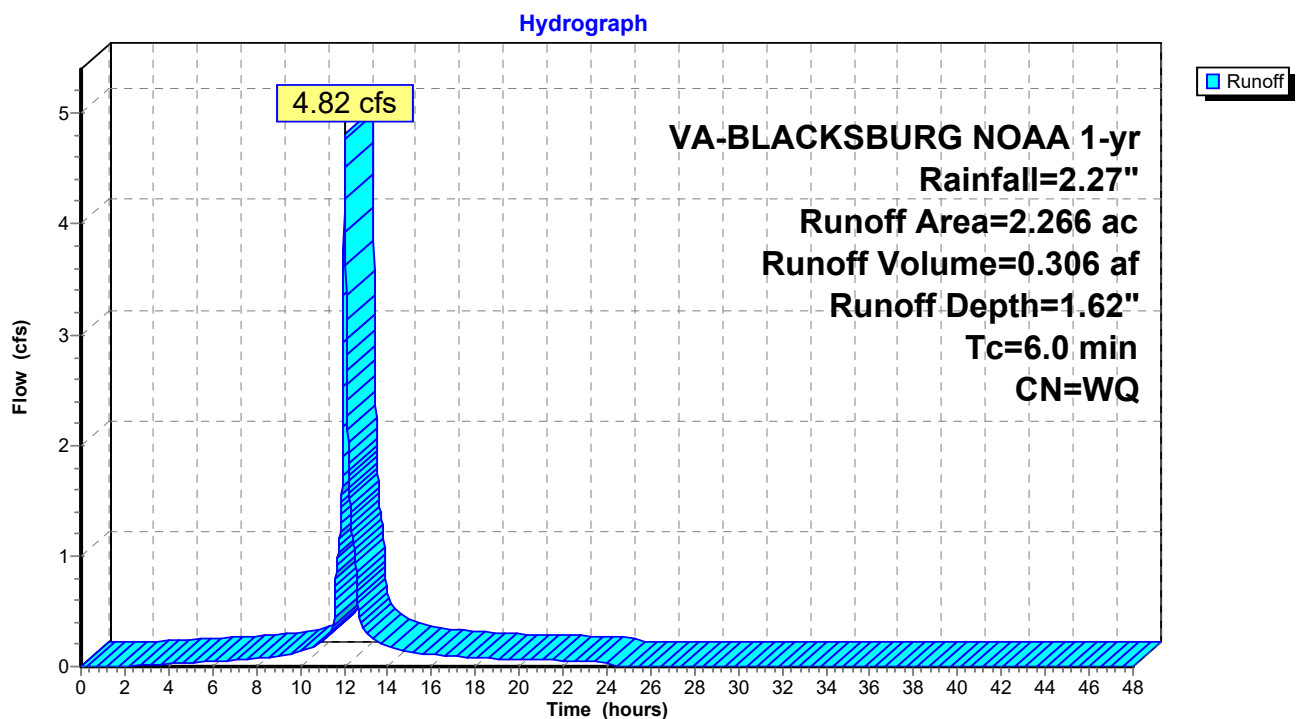
**Summary for Subcatchment 2S: DA TO DETENTION SYSTEM #1**

Runoff = 4.82 cfs @ 12.04 hrs, Volume= 0.306 af, Depth= 1.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Area (ac)	CN	Description
0.176	61	>75% Grass cover, Good, HSG B
0.401	74	>75% Grass cover, Good, HSG C
0.339	98	Paved parking, HSG B
1.350	98	Paved parking, HSG C
2.266		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 2S: DA TO DETENTION SYSTEM #1**

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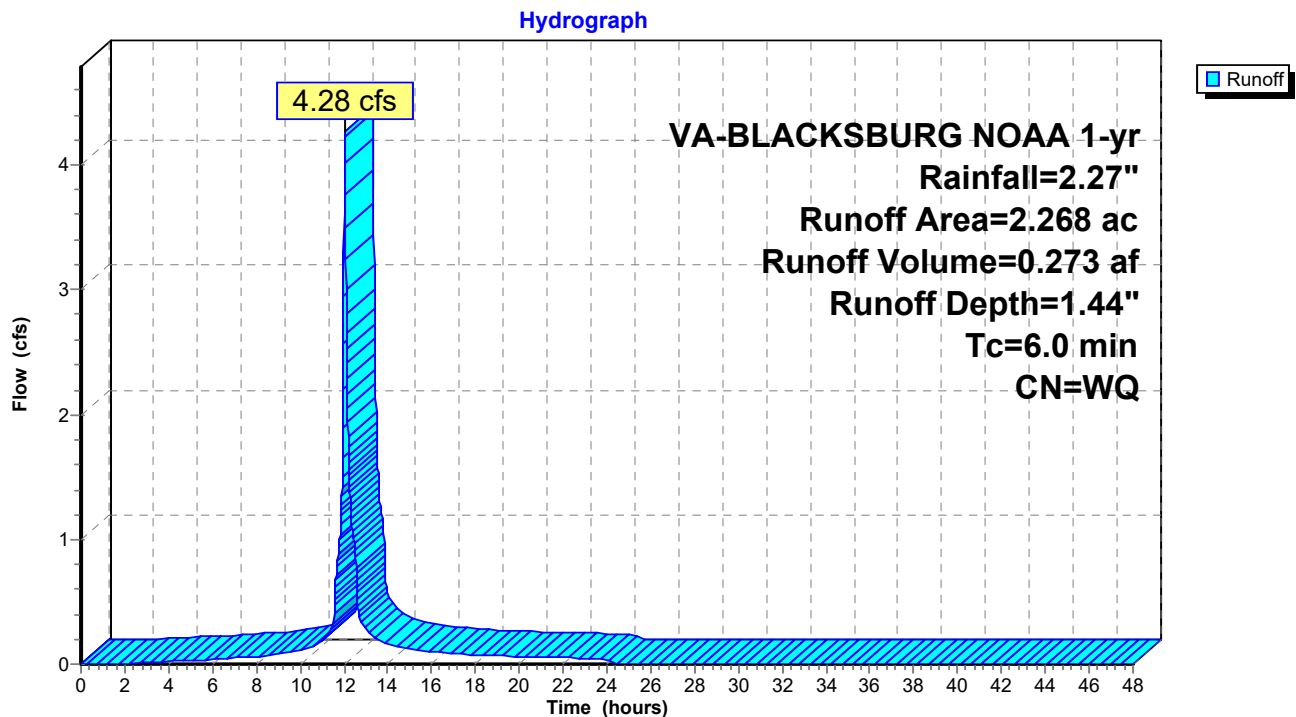
**Summary for Subcatchment 3S: DA TO DETENTION SYSTEM #2**

Runoff = 4.28 cfs @ 12.04 hrs, Volume= 0.273 af, Depth= 1.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Area (ac)	CN	Description
0.071	61	>75% Grass cover, Good, HSG B
0.621	74	>75% Grass cover, Good, HSG C
0.064	55	Woods, Good, HSG B
0.074	70	Woods, Good, HSG C
0.135	98	Paved roads w/curbs & sewers, HSG C
0.131	98	Paved parking, HSG B
1.172	98	Paved parking, HSG C
2.268		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 3S: DA TO DETENTION SYSTEM #2**

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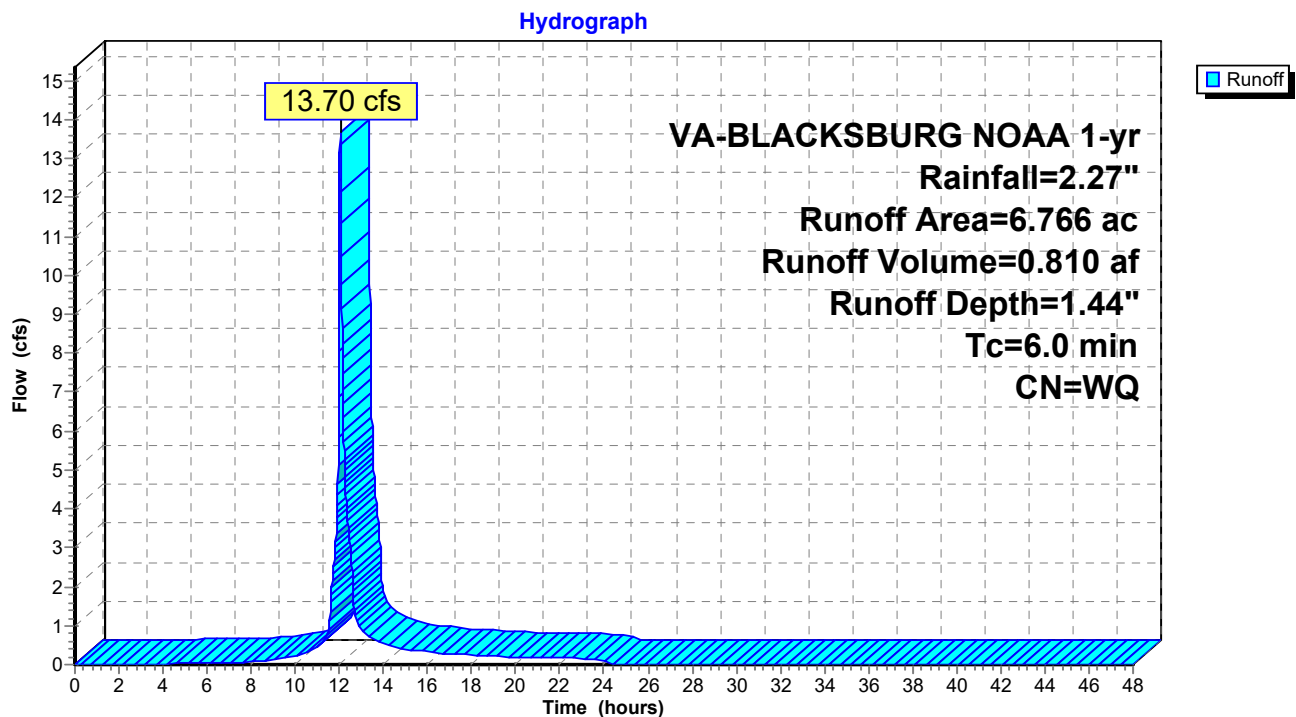
**Summary for Subcatchment 5S: BYPASS AREA**

Runoff = 13.70 cfs @ 12.04 hrs, Volume= 0.810 af, Depth= 1.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Area (ac)	CN	Description
0.106	61	>75% Grass cover, Good, HSG B
0.044	74	>75% Grass cover, Good, HSG C
0.326	85	1/8 acre lots, 65% imp, HSG B
4.878	90	1/8 acre lots, 65% imp, HSG C
0.028	98	Paved roads w/curbs & sewers, HSG B
1.384	98	Paved roads w/curbs & sewers, HSG C
6.766		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 5S: BYPASS AREA**

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**Summary for Pond 1P: UNDERGROUND DETENTION SYSTEM #1**

Inflow Area = 2.266 ac, Inflow Depth = 1.62" for 1-yr event  
 Inflow = 4.82 cfs @ 12.04 hrs, Volume= 0.306 af  
 Outflow = 0.13 cfs @ 15.00 hrs, Volume= 0.228 af, Atten= 97%, Lag= 178.0 min  
 Primary = 0.13 cfs @ 15.00 hrs, Volume= 0.228 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
 Peak Elev= 2,159.90' @ 15.00 hrs Surf.Area= 0.083 ac Storage= 0.210 af

Plug-Flow detention time= 893.0 min calculated for 0.228 af (75% of inflow)  
 Center-of-Mass det. time= 800.7 min ( 1,573.4 - 772.7 )

Volume	Invert	Avail.Storage	Storage Description
#1A	2,156.25'	0.097 af	<b>18.00'W x 202.00'L x 5.00'H Field A</b> 0.417 af Overall - 0.174 af Embedded = 0.243 af x 40.0% Voids
#2A	2,156.75'	0.174 af	<b>CMP Round 48 x 30 Inside #1</b> Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf Overall Size= 48.0"W x 48.0"H x 20.00'L Row Length Adjustment= -4.00' x 12.57 sf x 3 rows 16.00' Header x 12.57 sf x 1 = 201.1 cf Inside
		0.271 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	2,156.07'	<b>18.0" Round 18" HDPE</b> L= 82.4' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 2,156.07' / 2,155.51' S= 0.0068 ' S= 0.0068 ' Cc= 0.900 n= 0.011, Flow Area= 1.77 sf
#2	Device 1	2,156.07'	<b>1.2" Vert. 1" Orifice</b> C= 0.600
#3	Device 1	2,159.75'	<b>5.0" Vert. 3" Orifice</b> C= 0.600
#4	Device 1	2,160.25'	<b>5.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=0.13 cfs @ 15.00 hrs HW=2,159.90' (Free Discharge)

- 1=18" HDPE (Passes 0.13 cfs of 14.93 cfs potential flow)
- 2=1" Orifice (Orifice Controls 0.07 cfs @ 9.36 fps)
- 3=3" Orifice (Orifice Controls 0.06 cfs @ 1.31 fps)
- 4=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

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VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

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### Pond 1P: UNDERGROUND DETENTION SYSTEM #1 - Chamber Wizard Field A

#### Chamber Model = CMP Round 48 (Round Corrugated Metal Pipe)

Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf

Overall Size= 48.0"W x 48.0"H x 20.00'L

Row Length Adjustment= -4.00' x 12.57 sf x 3 rows

48.0" Wide + 24.0" Spacing = 72.0" C-C Row Spacing

10 Chambers/Row x 20.00' Long -4.00' Row Adjustment +4.00' Header x 1 = 200.00' Row Length +12.0"  
End Stone x 2 = 202.00' Base Length

3 Rows x 48.0" Wide + 24.0" Spacing x 2 + 12.0" Side Stone x 2 = 18.00' Base Width

6.0" Base + 48.0" Chamber Height + 6.0" Cover = 5.00' Field Height

30 Chambers x 251.3 cf -4.00' Row Adjustment x 12.57 sf x 3 Rows + 16.00' Header x 12.57 sf =  
7,590.1 cf Chamber Storage

18,180.0 cf Field - 7,590.1 cf Chambers = 10,589.9 cf Stone x 40.0% Voids = 4,236.0 cf Stone Storage

Chamber Storage + Stone Storage = 11,826.1 cf = 0.271 af

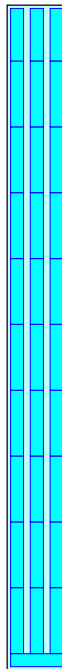
Overall Storage Efficiency = 65.0%

Overall System Size = 202.00' x 18.00' x 5.00'

30 Chambers

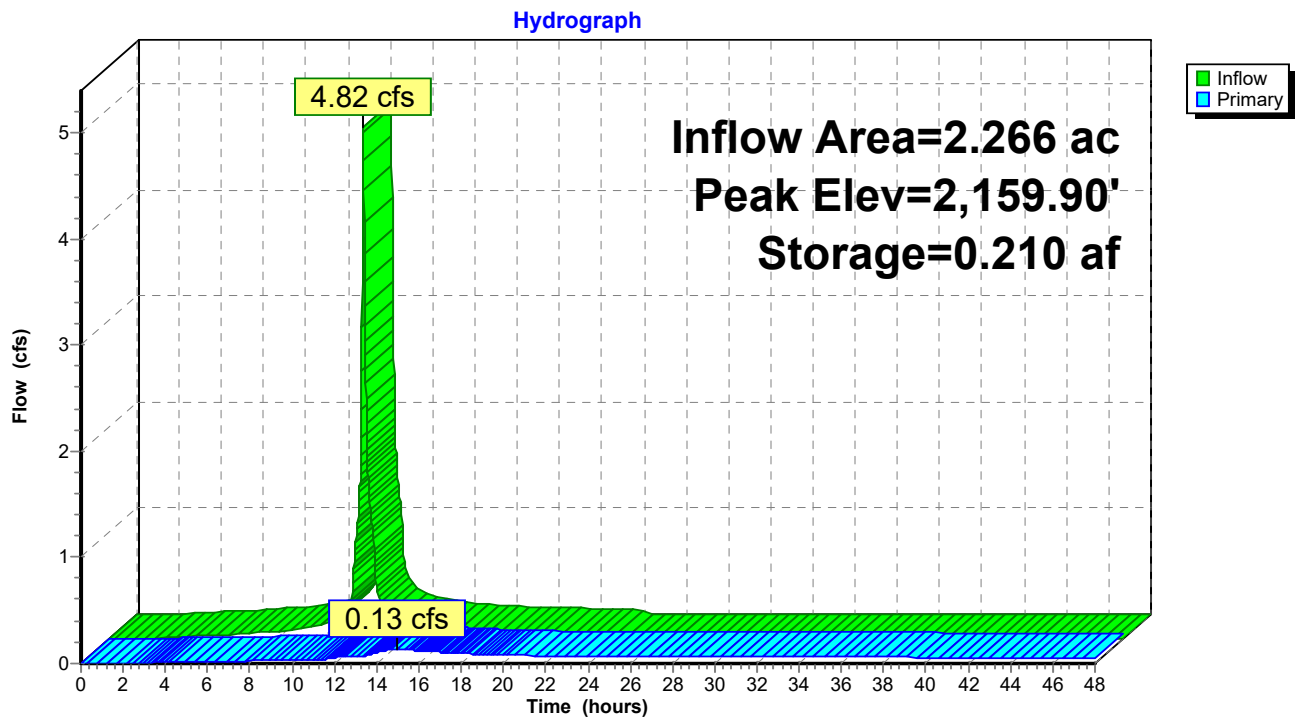
673.3 cy Field

392.2 cy Stone





# Pond 1P: UNDERGROUND DETENTION SYSTEM #1



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**Summary for Pond 2P: UNDERGROUND DETENTION SYSTEM #2**

Inflow Area = 2.268 ac, Inflow Depth = 1.44" for 1-yr event  
 Inflow = 4.28 cfs @ 12.04 hrs, Volume= 0.273 af  
 Outflow = 0.12 cfs @ 15.18 hrs, Volume= 0.273 af, Atten= 97%, Lag= 188.5 min  
 Primary = 0.12 cfs @ 15.18 hrs, Volume= 0.273 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
 Peak Elev= 2,157.10' @ 15.18 hrs Surf.Area= 0.075 ac Storage= 0.158 af

Plug-Flow detention time= 620.9 min calculated for 0.273 af (100% of inflow)  
 Center-of-Mass det. time= 620.8 min ( 1,399.1 - 778.3 )

Volume	Invert	Avail.Storage	Storage Description
#1A	2,154.00'	0.088 af	<b>18.00'W x 182.00'L x 5.00'H Field A</b> 0.376 af Overall - 0.157 af Embedded = 0.219 af x 40.0% Voids
#2A	2,154.50'	0.157 af	<b>CMP Round 48 x 27 Inside #1</b> Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf Overall Size= 48.0"W x 48.0"H x 20.00'L Row Length Adjustment= -4.00' x 12.57 sf x 3 rows 16.00' Header x 12.57 sf x 1 = 201.1 cf Inside
		0.245 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	2,153.85'	<b>15.0" Round 15" HDPE</b> L= 37.1' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 2,153.85' / 2,153.55' S= 0.0081 '/' Cc= 0.900 n= 0.011, Flow Area= 1.23 sf
#2	Device 1	2,153.85'	<b>Reg-U-Flo SXH 3.0-in</b>
#3	Device 1	2,158.00'	<b>8.0" W x 4.0" H Vert. Orifice/Grate C= 0.600</b>
#4	Device 1	2,158.15'	<b>5.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=0.12 cfs @ 15.18 hrs HW=2,157.10' (Free Discharge)

- 1=15" HDPE (Passes 0.12 cfs of 9.58 cfs potential flow)
- 2=Reg-U-Flo SXH 3.0-in (Custom Controls 0.12 cfs)
- 3=Orifice/Grate ( Controls 0.00 cfs)
- 4=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

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### Pond 2P: UNDERGROUND DETENTION SYSTEM #2 - Chamber Wizard Field A

#### Chamber Model = CMP Round 48 (Round Corrugated Metal Pipe)

Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf

Overall Size= 48.0"W x 48.0"H x 20.00'L

Row Length Adjustment= -4.00' x 12.57 sf x 3 rows

48.0" Wide + 24.0" Spacing = 72.0" C-C Row Spacing

9 Chambers/Row x 20.00' Long -4.00' Row Adjustment +4.00' Header x 1 = 180.00' Row Length +12.0"

End Stone x 2 = 182.00' Base Length

3 Rows x 48.0" Wide + 24.0" Spacing x 2 + 12.0" Side Stone x 2 = 18.00' Base Width

6.0" Base + 48.0" Chamber Height + 6.0" Cover = 5.00' Field Height

27 Chambers x 251.3 cf -4.00' Row Adjustment x 12.57 sf x 3 Rows + 16.00' Header x 12.57 sf =  
6,836.1 cf Chamber Storage

16,380.0 cf Field - 6,836.1 cf Chambers = 9,543.9 cf Stone x 40.0% Voids = 3,817.6 cf Stone Storage

Chamber Storage + Stone Storage = 10,653.7 cf = 0.245 af

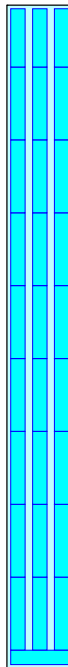
Overall Storage Efficiency = 65.0%

Overall System Size = 182.00' x 18.00' x 5.00'

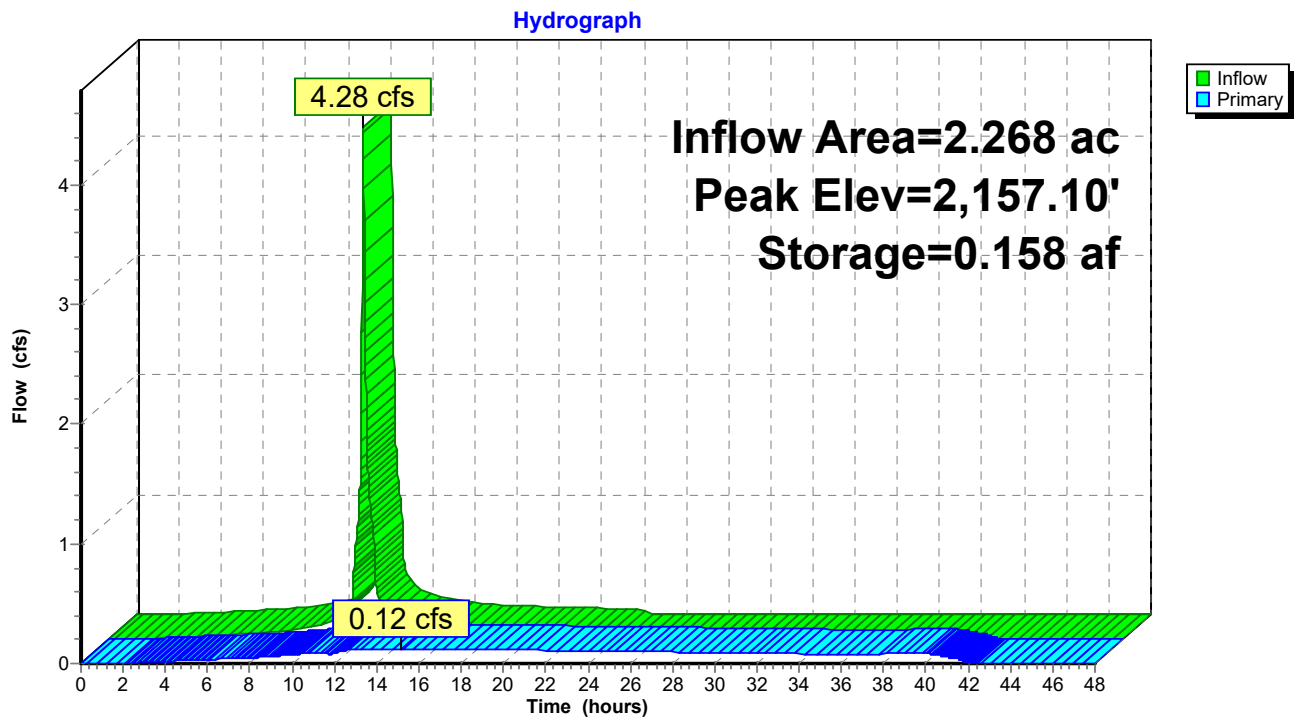
27 Chambers

606.7 cy Field

353.5 cy Stone



## Pond 2P: UNDERGROUND DETENTION SYSTEM #2



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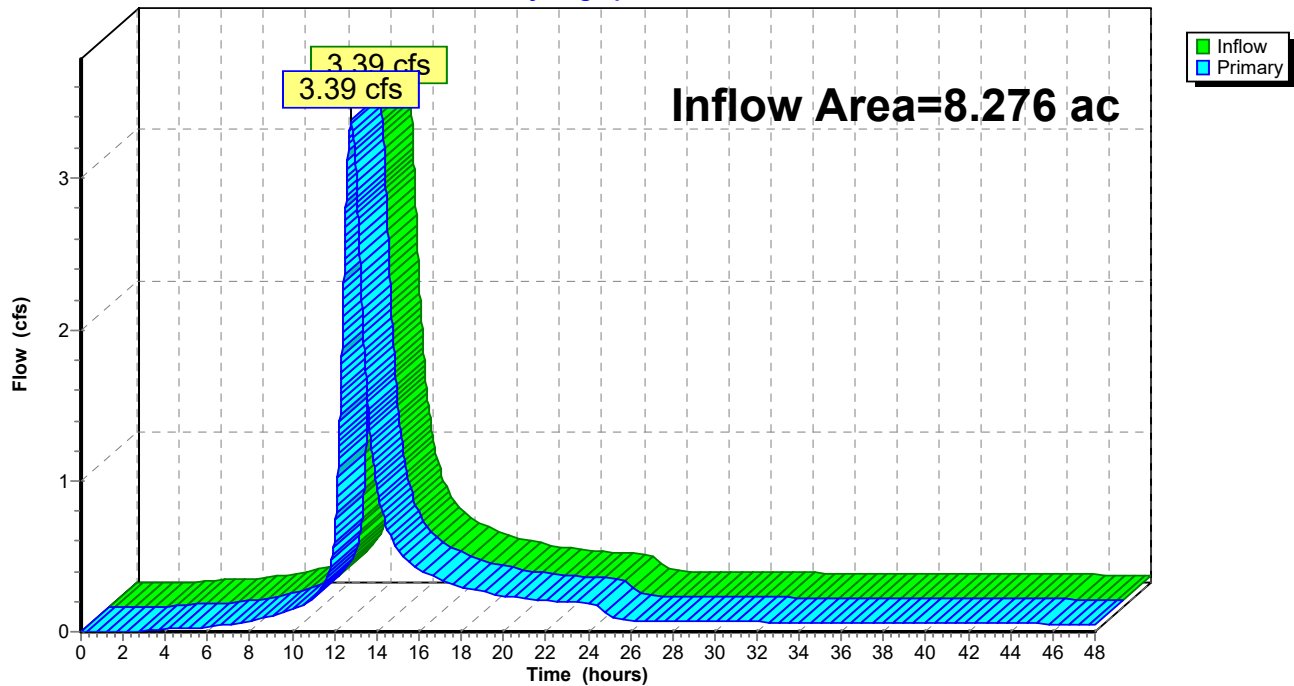
### Summary for Link 1L: POA #1

Inflow Area = 8.276 ac, Inflow Depth > 1.18" for 1-yr event  
Inflow = 3.39 cfs @ 12.79 hrs, Volume= 0.812 af  
Primary = 3.39 cfs @ 12.79 hrs, Volume= 0.812 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 1L: POA #1

Hydrograph



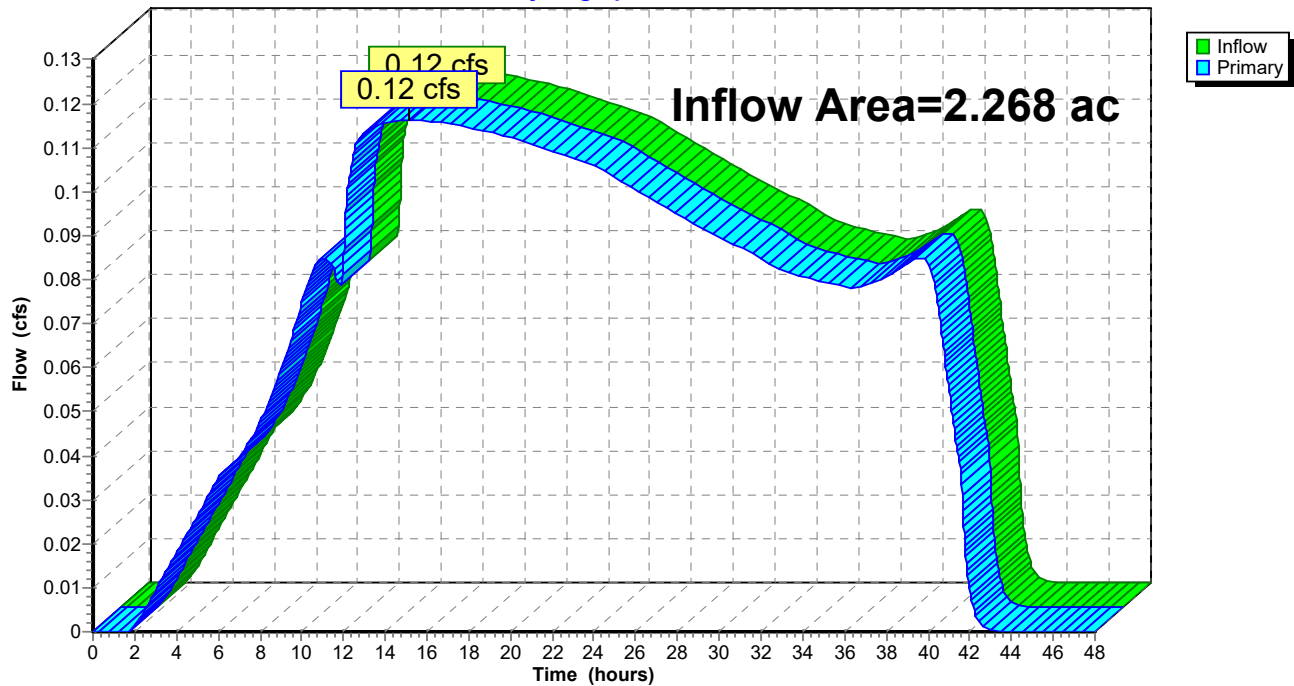
### Summary for Link 2L: MH-A

Inflow Area = 2.268 ac, Inflow Depth = 1.44" for 1-yr event  
 Inflow = 0.12 cfs @ 15.18 hrs, Volume= 0.273 af  
 Primary = 0.12 cfs @ 15.18 hrs, Volume= 0.273 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 2L: MH-A

Hydrograph



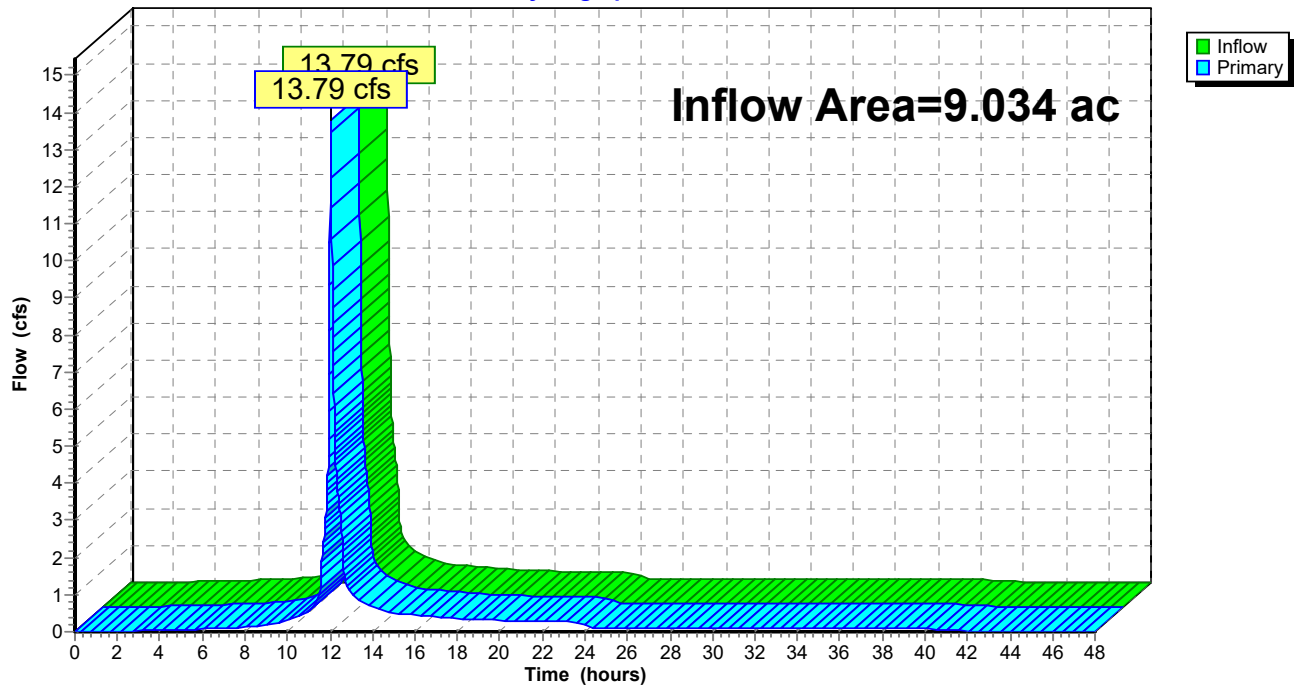
### Summary for Link 3L: POA #2

Inflow Area = 9.034 ac, Inflow Depth = 1.44" for 1-yr event  
 Inflow = 13.79 cfs @ 12.04 hrs, Volume= 1.083 af  
 Primary = 13.79 cfs @ 12.04 hrs, Volume= 1.083 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 3L: POA #2

Hydrograph



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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q  
Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

**Subcatchment1S: BYPASS AREA**

Runoff Area=6.010 ac Runoff Depth=1.54"  
Flow Length=973' Tc=60.9 min CN=WQ Runoff=4.39 cfs 0.770 af

**Subcatchment2S: DA TO DETENTION SYSTEM #1**

Runoff Area=2.266 ac Runoff Depth=2.03"  
Tc=6.0 min CN=WQ Runoff=6.00 cfs 0.384 af

**Subcatchment3S: DA TO DETENTION SYSTEM #2**

Runoff Area=2.268 ac Runoff Depth=1.84"  
Tc=6.0 min CN=WQ Runoff=5.42 cfs 0.347 af

**Subcatchment5S: BYPASS AREA**

Runoff Area=6.766 ac Runoff Depth=1.87"  
Tc=6.0 min CN=WQ Runoff=17.73 cfs 1.053 af

**Pond 1P: UNDERGROUND DETENTION**

Peak Elev=2,160.28' Storage=0.232 af Inflow=6.00 cfs 0.384 af  
Outflow=0.53 cfs 0.303 af

**Pond 2P: UNDERGROUND DETENTION**

Peak Elev=2,158.03' Storage=0.209 af Inflow=5.42 cfs 0.347 af  
Outflow=0.14 cfs 0.347 af

**Link 1L: POA #1**

Inflow=4.89 cfs 1.074 af  
Primary=4.89 cfs 1.074 af

**Link 2L: MH-A**

Inflow=0.14 cfs 0.347 af  
Primary=0.14 cfs 0.347 af

**Link 3L: POA #2**

Inflow=17.83 cfs 1.400 af  
Primary=17.83 cfs 1.400 af

**Total Runoff Area = 17.310 ac Runoff Volume = 2.554 af Average Runoff Depth = 1.77"**



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**Summary for Subcatchment 1S: BYPASS AREA**

Runoff = 4.39 cfs @ 12.79 hrs, Volume= 0.770 af, Depth= 1.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

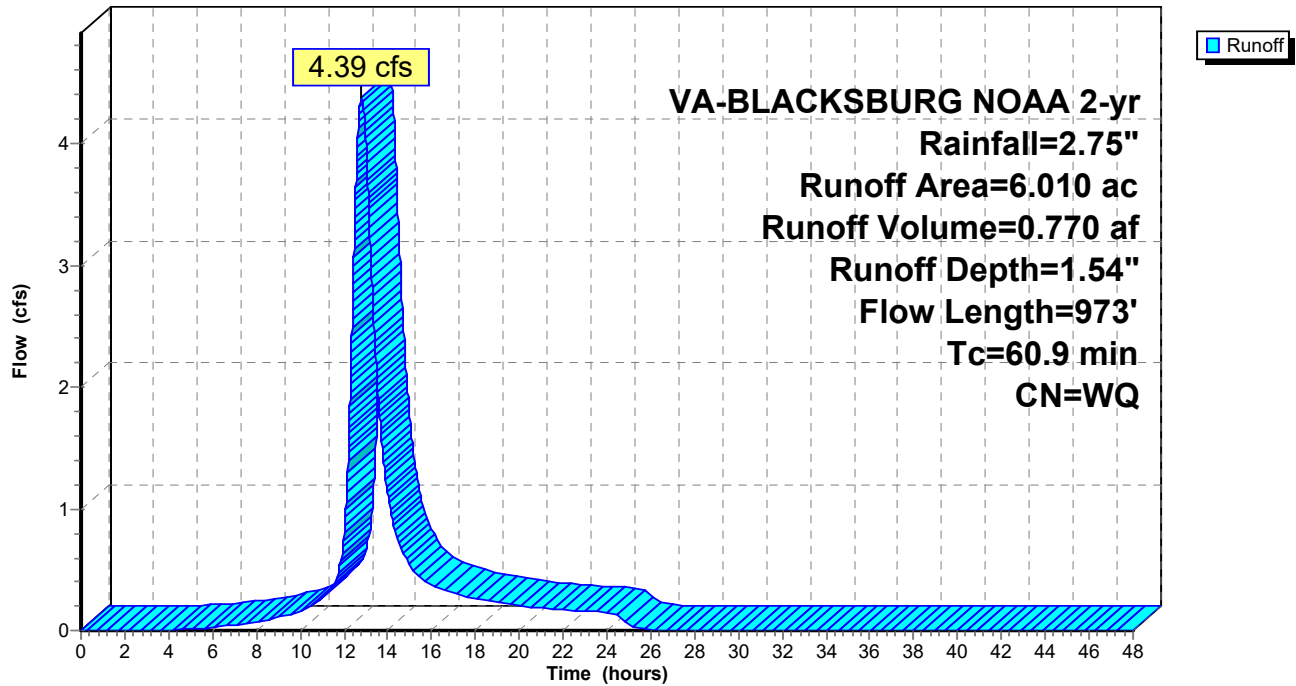
Area (ac)	CN	Description
0.433	61	>75% Grass cover, Good, HSG B
0.407	74	>75% Grass cover, Good, HSG C
0.270	55	Woods, Good, HSG B
0.076	70	Woods, Good, HSG C
0.164	70	1/2 acre lots, 25% imp, HSG B
0.371	80	1/2 acre lots, 25% imp, HSG C
0.282	75	1/4 acre lots, 38% imp, HSG B
0.496	83	1/4 acre lots, 38% imp, HSG C
0.044	85	1/8 acre lots, 65% imp, HSG B
0.685	92	Urban commercial, 85% imp, HSG B
2.402	94	Urban commercial, 85% imp, HSG C
0.047	98	Paved roads w/curbs & sewers, HSG B
0.209	98	Paved roads w/curbs & sewers, HSG C
0.068	98	Paved parking, HSG B
0.056	98	Paved parking, HSG C
6.010		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
52.4	150	0.0233	0.05		<b>Sheet Flow, Tc1</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
6.7	415	0.0422	1.03		<b>Shallow Concentrated Flow, Tc2</b> Woodland Kv= 5.0 fps
1.8	408	0.0564	3.82		<b>Shallow Concentrated Flow, Tc3</b> Unpaved Kv= 16.1 fps
60.9	973	Total			

# Subcatchment 1S: BYPASS AREA

Hydrograph



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VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

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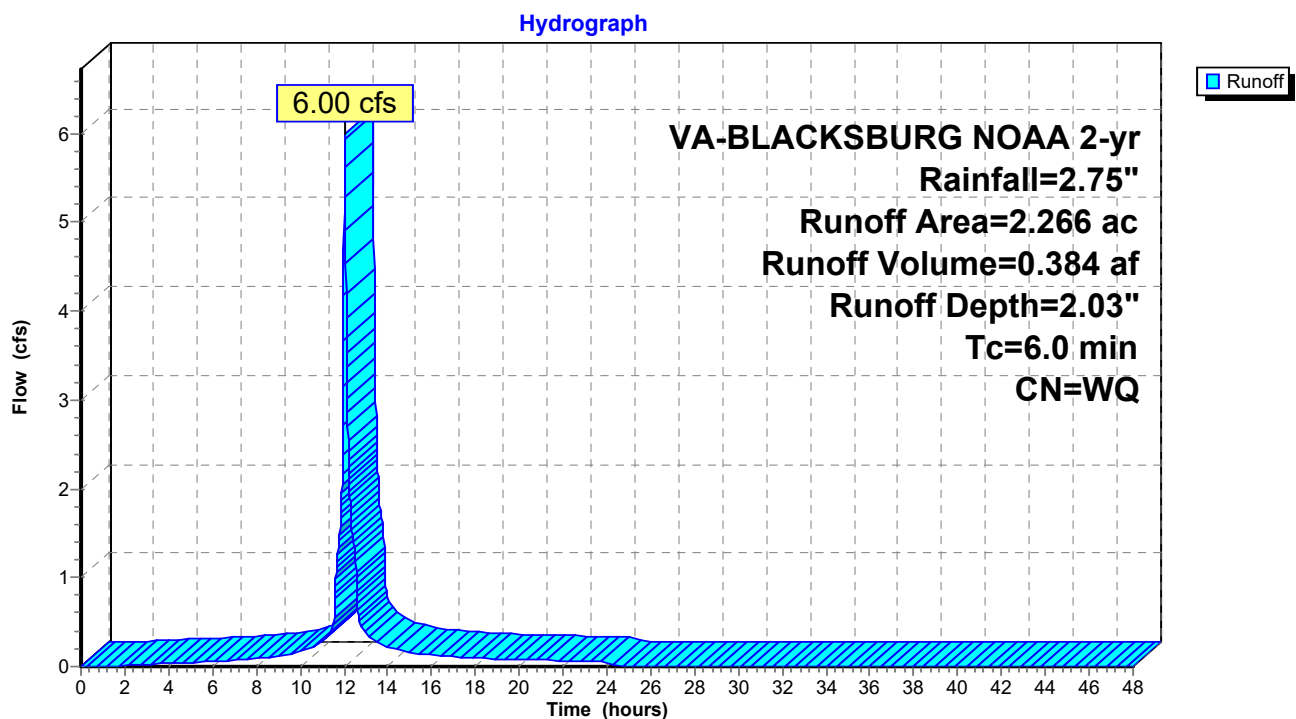
**Summary for Subcatchment 2S: DA TO DETENTION SYSTEM #1**

Runoff = 6.00 cfs @ 12.04 hrs, Volume= 0.384 af, Depth= 2.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

Area (ac)	CN	Description
0.176	61	>75% Grass cover, Good, HSG B
0.401	74	>75% Grass cover, Good, HSG C
0.339	98	Paved parking, HSG B
1.350	98	Paved parking, HSG C
2.266		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 2S: DA TO DETENTION SYSTEM #1**

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VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

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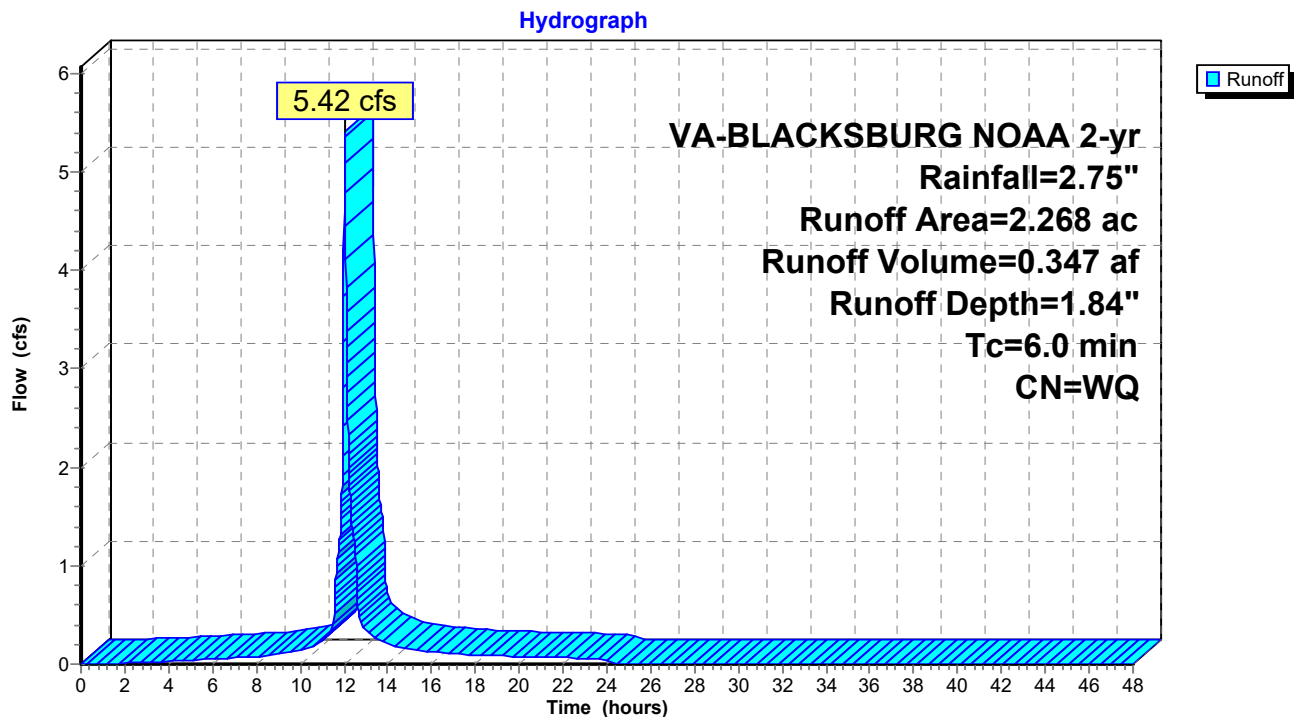
**Summary for Subcatchment 3S: DA TO DETENTION SYSTEM #2**

Runoff = 5.42 cfs @ 12.04 hrs, Volume= 0.347 af, Depth= 1.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

Area (ac)	CN	Description
0.071	61	>75% Grass cover, Good, HSG B
0.621	74	>75% Grass cover, Good, HSG C
0.064	55	Woods, Good, HSG B
0.074	70	Woods, Good, HSG C
0.135	98	Paved roads w/curbs & sewers, HSG C
0.131	98	Paved parking, HSG B
1.172	98	Paved parking, HSG C
2.268		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 3S: DA TO DETENTION SYSTEM #2**

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VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

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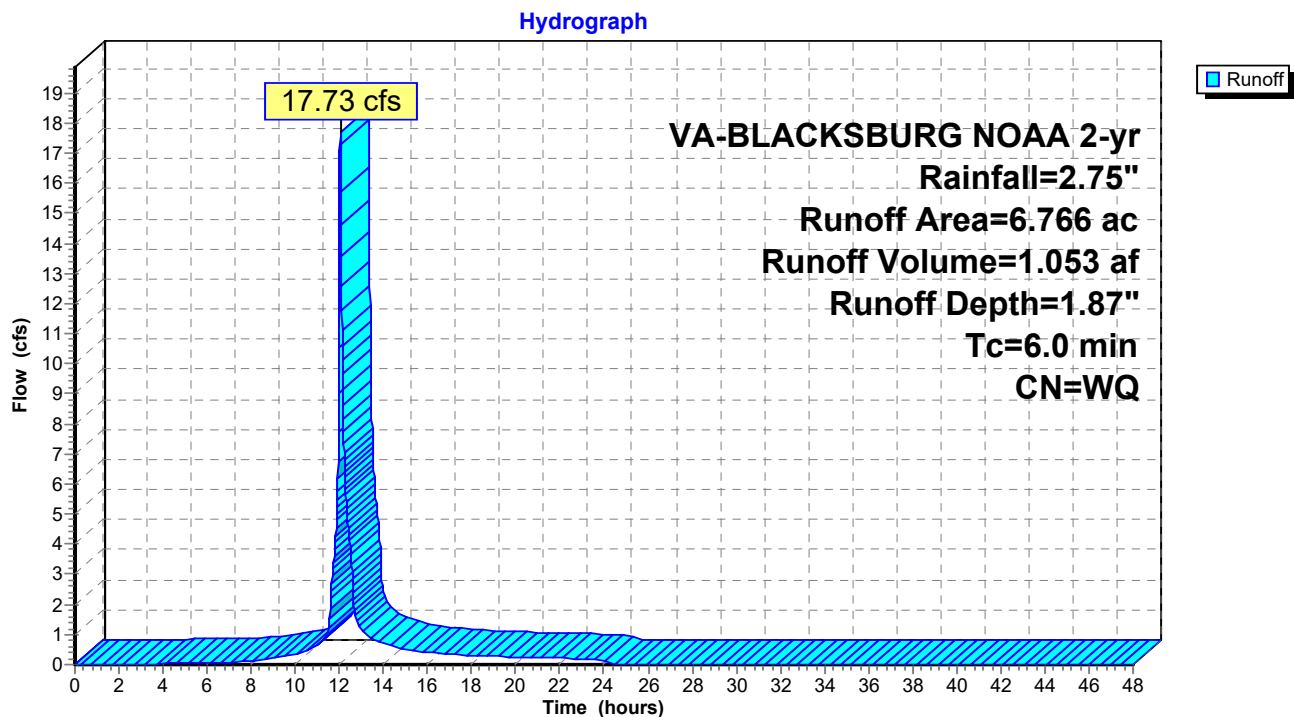
**Summary for Subcatchment 5S: BYPASS AREA**

Runoff = 17.73 cfs @ 12.04 hrs, Volume= 1.053 af, Depth= 1.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

Area (ac)	CN	Description
0.106	61	>75% Grass cover, Good, HSG B
0.044	74	>75% Grass cover, Good, HSG C
0.326	85	1/8 acre lots, 65% imp, HSG B
4.878	90	1/8 acre lots, 65% imp, HSG C
0.028	98	Paved roads w/curbs & sewers, HSG B
1.384	98	Paved roads w/curbs & sewers, HSG C
6.766		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 5S: BYPASS AREA**

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VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

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**Summary for Pond 1P: UNDERGROUND DETENTION SYSTEM #1**

Inflow Area = 2.266 ac, Inflow Depth = 2.03" for 2-yr event  
 Inflow = 6.00 cfs @ 12.04 hrs, Volume= 0.384 af  
 Outflow = 0.53 cfs @ 12.69 hrs, Volume= 0.303 af, Atten= 91%, Lag= 39.4 min  
 Primary = 0.53 cfs @ 12.69 hrs, Volume= 0.303 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
 Peak Elev= 2,160.28' @ 12.69 hrs Surf.Area= 0.083 ac Storage= 0.232 af

Plug-Flow detention time= 711.1 min calculated for 0.303 af (79% of inflow)  
 Center-of-Mass det. time= 627.3 min ( 1,396.5 - 769.2 )

Volume	Invert	Avail.Storage	Storage Description
#1A	2,156.25'	0.097 af	<b>18.00'W x 202.00'L x 5.00'H Field A</b> 0.417 af Overall - 0.174 af Embedded = 0.243 af x 40.0% Voids
#2A	2,156.75'	0.174 af	<b>CMP Round 48 x 30 Inside #1</b> Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf Overall Size= 48.0"W x 48.0"H x 20.00'L Row Length Adjustment= -4.00' x 12.57 sf x 3 rows 16.00' Header x 12.57 sf x 1 = 201.1 cf Inside
		0.271 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	2,156.07'	<b>18.0" Round 18" HDPE</b> L= 82.4' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 2,156.07' / 2,155.51' S= 0.0068 ' S= 0.0068 ' Cc= 0.900 n= 0.011, Flow Area= 1.77 sf
#2	Device 1	2,156.07'	<b>1.2" Vert. 1" Orifice</b> C= 0.600
#3	Device 1	2,159.75'	<b>5.0" Vert. 3" Orifice</b> C= 0.600
#4	Device 1	2,160.25'	<b>5.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=0.52 cfs @ 12.69 hrs HW=2,160.28' (Free Discharge)

- 1=18" HDPE (Passes 0.52 cfs of 15.83 cfs potential flow)
- 2=1" Orifice (Orifice Controls 0.08 cfs @ 9.82 fps)
- 3=3" Orifice (Orifice Controls 0.37 cfs @ 2.73 fps)
- 4=Broad-Crested Rectangular Weir (Weir Controls 0.07 cfs @ 0.48 fps)

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VA-BLACKSBURG NOAA 2-yr Rainfall=2.75"

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### Pond 1P: UNDERGROUND DETENTION SYSTEM #1 - Chamber Wizard Field A

#### Chamber Model = CMP Round 48 (Round Corrugated Metal Pipe)

Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf

Overall Size= 48.0"W x 48.0"H x 20.00'L

Row Length Adjustment= -4.00' x 12.57 sf x 3 rows

48.0" Wide + 24.0" Spacing = 72.0" C-C Row Spacing

10 Chambers/Row x 20.00' Long -4.00' Row Adjustment +4.00' Header x 1 = 200.00' Row Length +12.0"  
End Stone x 2 = 202.00' Base Length

3 Rows x 48.0" Wide + 24.0" Spacing x 2 + 12.0" Side Stone x 2 = 18.00' Base Width

6.0" Base + 48.0" Chamber Height + 6.0" Cover = 5.00' Field Height

30 Chambers x 251.3 cf -4.00' Row Adjustment x 12.57 sf x 3 Rows + 16.00' Header x 12.57 sf =  
7,590.1 cf Chamber Storage

18,180.0 cf Field - 7,590.1 cf Chambers = 10,589.9 cf Stone x 40.0% Voids = 4,236.0 cf Stone Storage

Chamber Storage + Stone Storage = 11,826.1 cf = 0.271 af

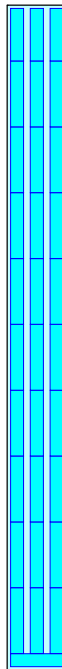
Overall Storage Efficiency = 65.0%

Overall System Size = 202.00' x 18.00' x 5.00'

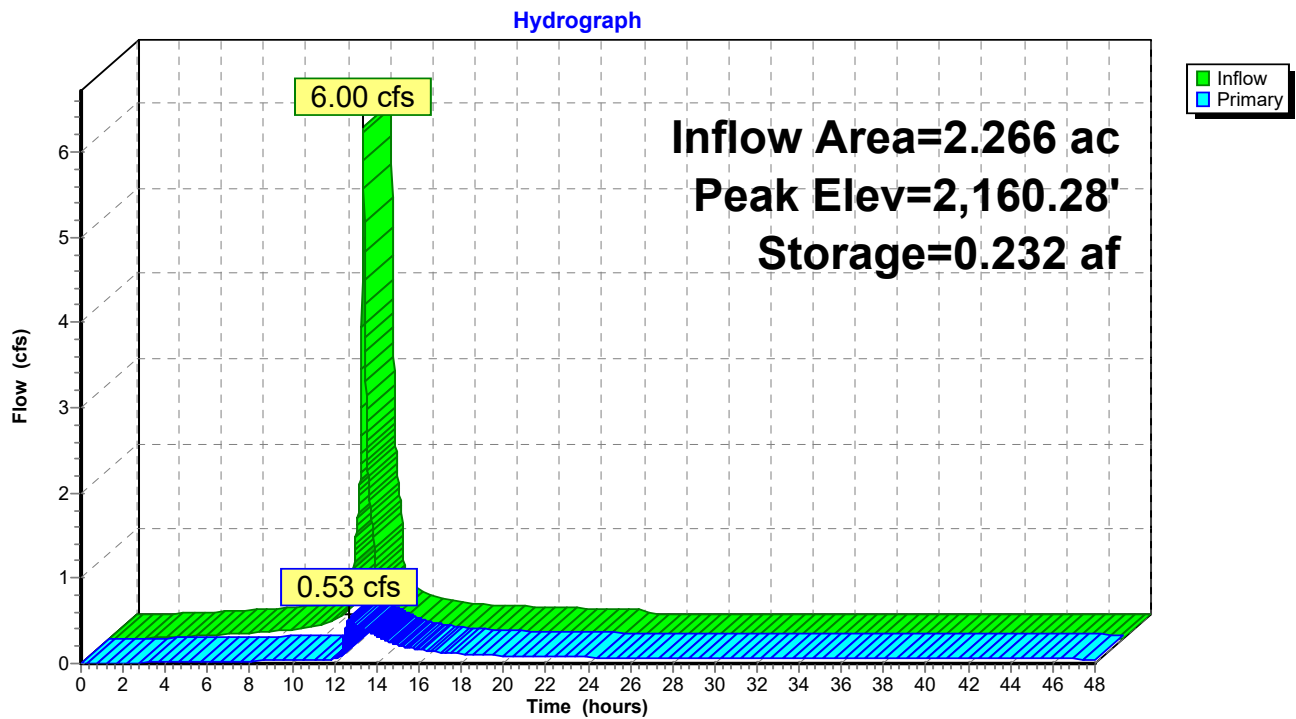
30 Chambers

673.3 cy Field

392.2 cy Stone



# Pond 1P: UNDERGROUND DETENTION SYSTEM #1





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**Summary for Pond 2P: UNDERGROUND DETENTION SYSTEM #2**

Inflow Area = 2.268 ac, Inflow Depth = 1.84" for 2-yr event  
 Inflow = 5.42 cfs @ 12.04 hrs, Volume= 0.347 af  
 Outflow = 0.14 cfs @ 15.25 hrs, Volume= 0.347 af, Atten= 97%, Lag= 192.8 min  
 Primary = 0.14 cfs @ 15.25 hrs, Volume= 0.347 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
 Peak Elev= 2,158.03' @ 15.25 hrs Surf.Area= 0.075 ac Storage= 0.209 af

Plug-Flow detention time= 736.9 min calculated for 0.347 af (100% of inflow)  
 Center-of-Mass det. time= 736.8 min ( 1,512.2 - 775.4 )

Volume	Invert	Avail.Storage	Storage Description
#1A	2,154.00'	0.088 af	<b>18.00'W x 182.00'L x 5.00'H Field A</b> 0.376 af Overall - 0.157 af Embedded = 0.219 af x 40.0% Voids
#2A	2,154.50'	0.157 af	<b>CMP Round 48 x 27 Inside #1</b> Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf Overall Size= 48.0"W x 48.0"H x 20.00'L Row Length Adjustment= -4.00' x 12.57 sf x 3 rows 16.00' Header x 12.57 sf x 1 = 201.1 cf Inside
		0.245 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	2,153.85'	<b>15.0" Round 15" HDPE</b> L= 37.1' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 2,153.85' / 2,153.55' S= 0.0081 '/' Cc= 0.900 n= 0.011, Flow Area= 1.23 sf
#2	Device 1	2,153.85'	<b>Reg-U-Flo SXH 3.0-in</b>
#3	Device 1	2,158.00'	<b>8.0" W x 4.0" H Vert. Orifice/Grate C= 0.600</b>
#4	Device 1	2,158.15'	<b>5.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=0.14 cfs @ 15.25 hrs HW=2,158.03' (Free Discharge)

- 1=15" HDPE (Passes 0.14 cfs of 11.14 cfs potential flow)
- 2=Reg-U-Flo SXH 3.0-in (Custom Controls 0.13 cfs)
- 3=Orifice/Grate (Orifice Controls 0.01 cfs @ 0.57 fps)
- 4=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)

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### Pond 2P: UNDERGROUND DETENTION SYSTEM #2 - Chamber Wizard Field A

#### Chamber Model = CMP Round 48 (Round Corrugated Metal Pipe)

Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf

Overall Size= 48.0"W x 48.0"H x 20.00'L

Row Length Adjustment= -4.00' x 12.57 sf x 3 rows

48.0" Wide + 24.0" Spacing = 72.0" C-C Row Spacing

9 Chambers/Row x 20.00' Long -4.00' Row Adjustment +4.00' Header x 1 = 180.00' Row Length +12.0"

End Stone x 2 = 182.00' Base Length

3 Rows x 48.0" Wide + 24.0" Spacing x 2 + 12.0" Side Stone x 2 = 18.00' Base Width

6.0" Base + 48.0" Chamber Height + 6.0" Cover = 5.00' Field Height

27 Chambers x 251.3 cf -4.00' Row Adjustment x 12.57 sf x 3 Rows + 16.00' Header x 12.57 sf =  
6,836.1 cf Chamber Storage

16,380.0 cf Field - 6,836.1 cf Chambers = 9,543.9 cf Stone x 40.0% Voids = 3,817.6 cf Stone Storage

Chamber Storage + Stone Storage = 10,653.7 cf = 0.245 af

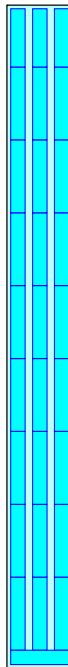
Overall Storage Efficiency = 65.0%

Overall System Size = 182.00' x 18.00' x 5.00'

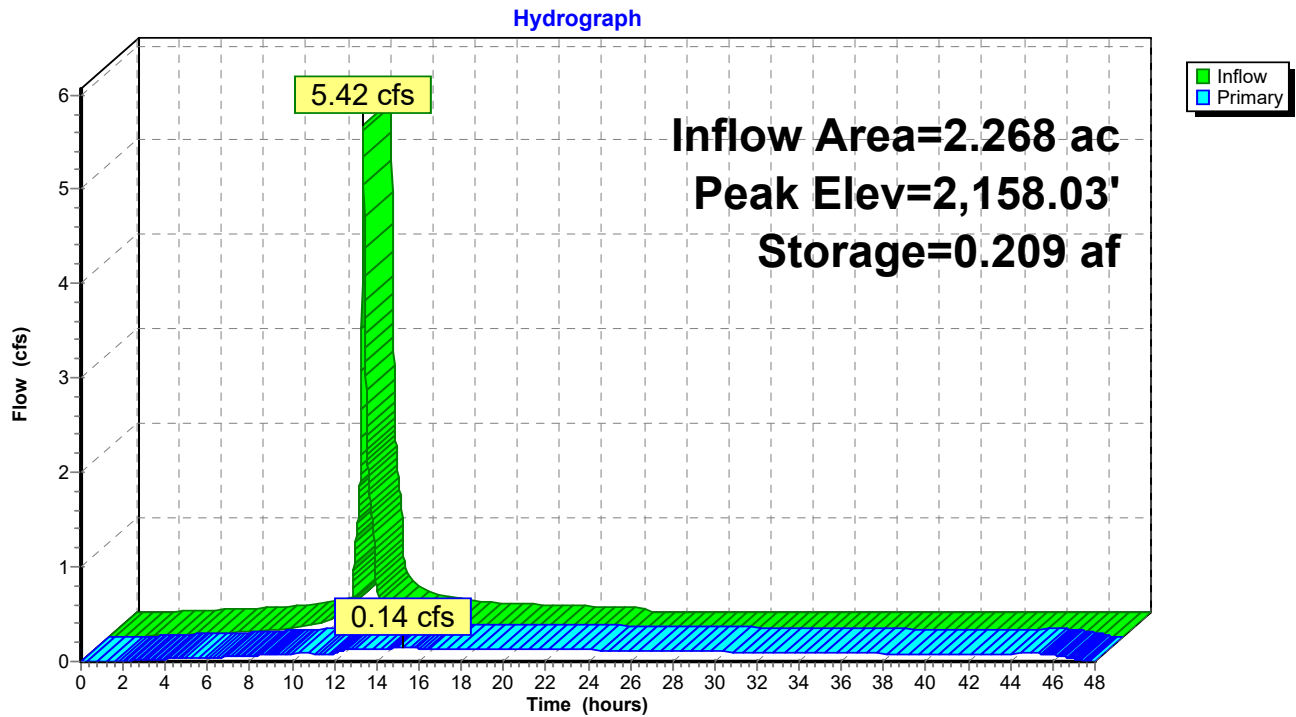
27 Chambers

606.7 cy Field

353.5 cy Stone



## Pond 2P: UNDERGROUND DETENTION SYSTEM #2



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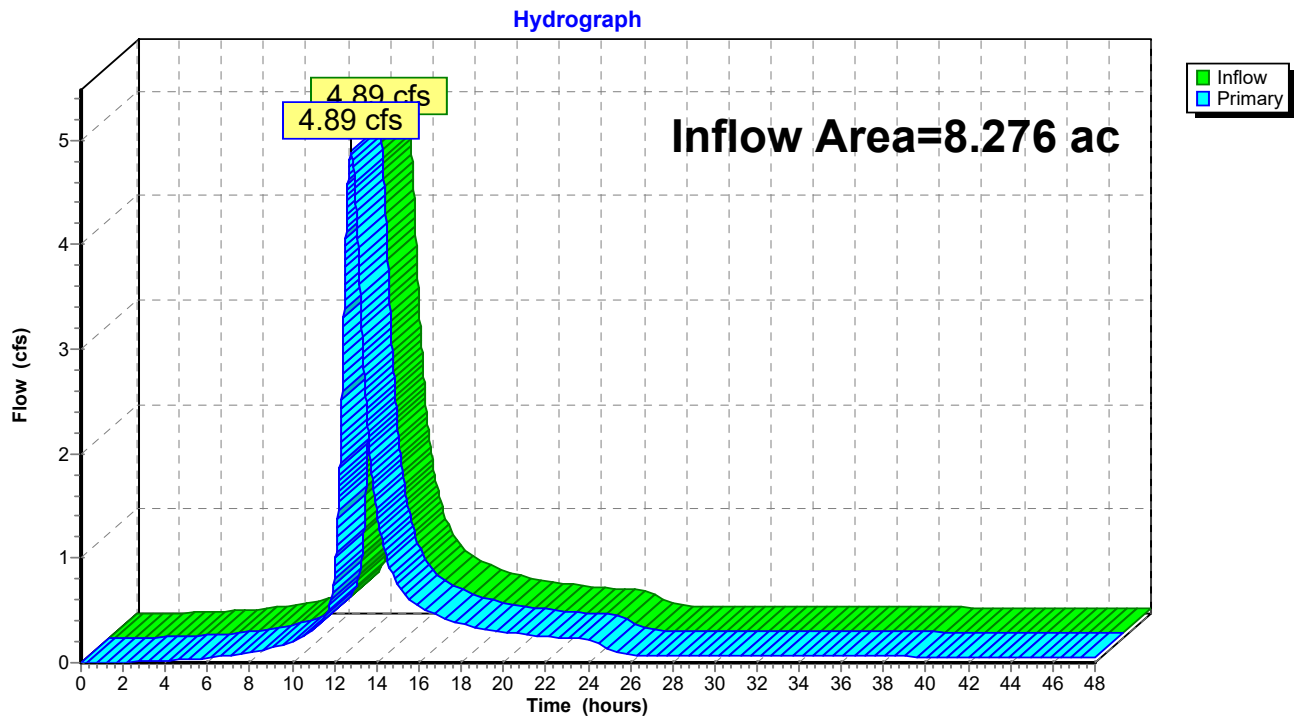
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### Summary for Link 1L: POA #1

Inflow Area = 8.276 ac, Inflow Depth > 1.56" for 2-yr event  
Inflow = 4.89 cfs @ 12.79 hrs, Volume= 1.074 af  
Primary = 4.89 cfs @ 12.79 hrs, Volume= 1.074 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 1L: POA #1



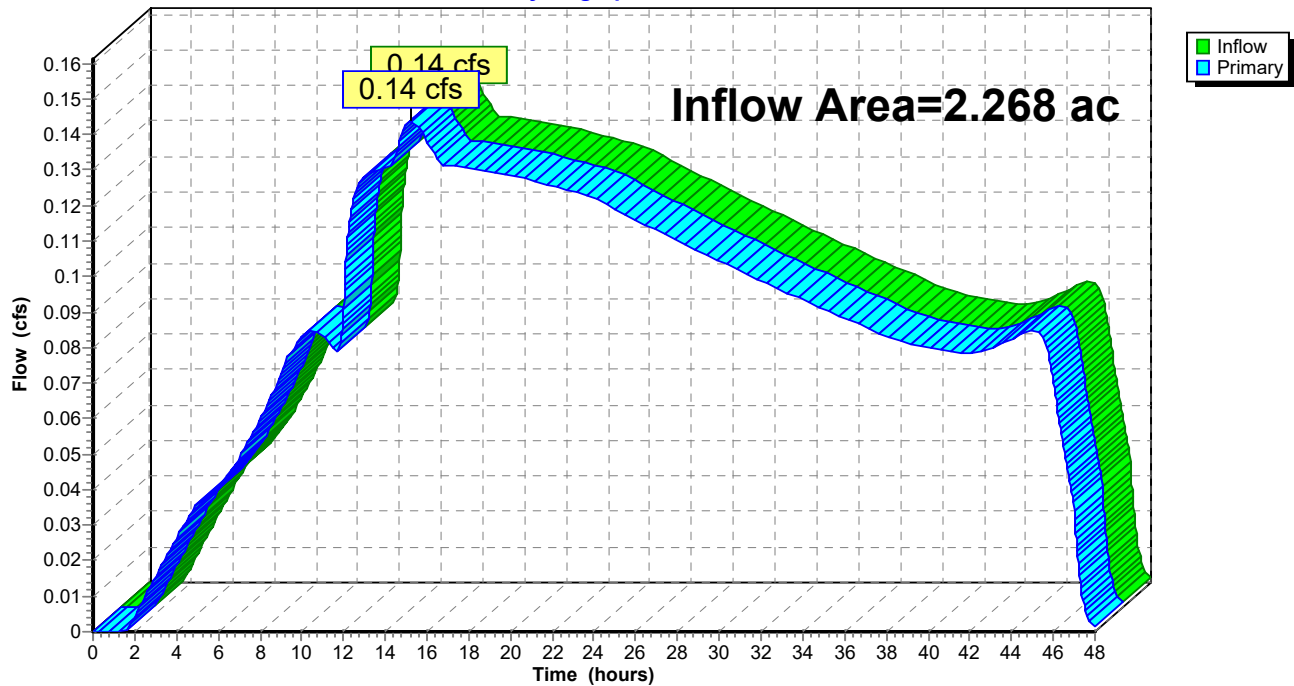
### Summary for Link 2L: MH-A

Inflow Area = 2.268 ac, Inflow Depth > 1.83" for 2-yr event  
 Inflow = 0.14 cfs @ 15.25 hrs, Volume= 0.347 af  
 Primary = 0.14 cfs @ 15.25 hrs, Volume= 0.347 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 2L: MH-A

Hydrograph



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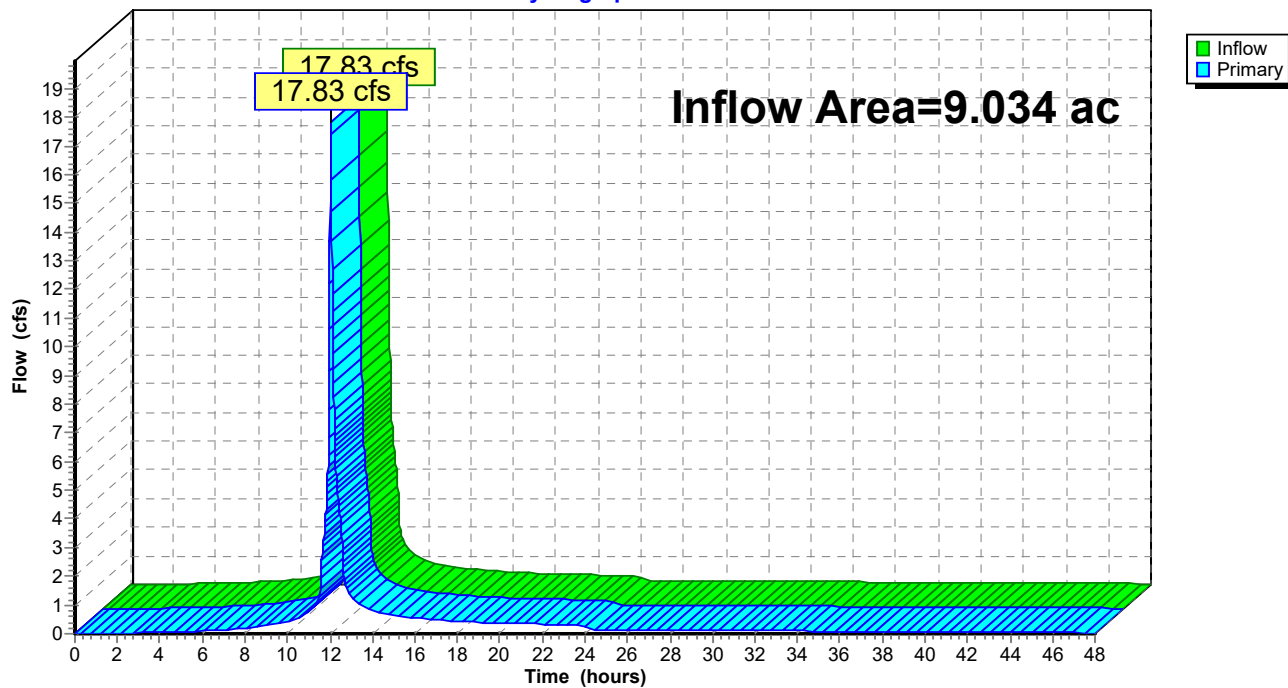
### Summary for Link 3L: POA #2

Inflow Area = 9.034 ac, Inflow Depth = 1.86" for 2-yr event  
Inflow = 17.83 cfs @ 12.04 hrs, Volume= 1.400 af  
Primary = 17.83 cfs @ 12.04 hrs, Volume= 1.400 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 3L: POA #2

Hydrograph



**POST DEV**

VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q  
Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

**Subcatchment1S: BYPASS AREA**

Runoff Area=6.010 ac Runoff Depth=2.65"  
Flow Length=973' Tc=60.9 min CN=WQ Runoff=7.36 cfs 1.329 af

**Subcatchment2S: DA TO DETENTION SYSTEM #1**

Runoff Area=2.266 ac Runoff Depth=3.23"  
Tc=6.0 min CN=WQ Runoff=8.71 cfs 0.611 af

**Subcatchment3S: DA TO DETENTION SYSTEM #2**

Runoff Area=2.268 ac Runoff Depth=2.99"  
Tc=6.0 min CN=WQ Runoff=8.09 cfs 0.565 af

**Subcatchment5S: BYPASS AREA**

Runoff Area=6.766 ac Runoff Depth=3.12"  
Tc=6.0 min CN=WQ Runoff=26.79 cfs 1.758 af

**Pond 1P: UNDERGROUND DETENTION**

Peak Elev=2,160.72' Storage=0.254 af Inflow=8.71 cfs 0.611 af  
Outflow=5.50 cfs 0.527 af

**Pond 2P: UNDERGROUND DETENTION**

Peak Elev=2,158.48' Storage=0.229 af Inflow=8.09 cfs 0.565 af  
Outflow=3.51 cfs 0.558 af

**Link 1L: POA #1**

Inflow=8.46 cfs 1.856 af  
Primary=8.46 cfs 1.856 af

**Link 2L: MH-A**

Inflow=3.51 cfs 0.558 af  
Primary=3.51 cfs 0.558 af

**Link 3L: POA #2**

Inflow=26.91 cfs 2.316 af  
Primary=26.91 cfs 2.316 af

**Total Runoff Area = 17.310 ac Runoff Volume = 4.262 af Average Runoff Depth = 2.95"**

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**Summary for Subcatchment 1S: BYPASS AREA**

Runoff = 7.36 cfs @ 12.79 hrs, Volume= 1.329 af, Depth= 2.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

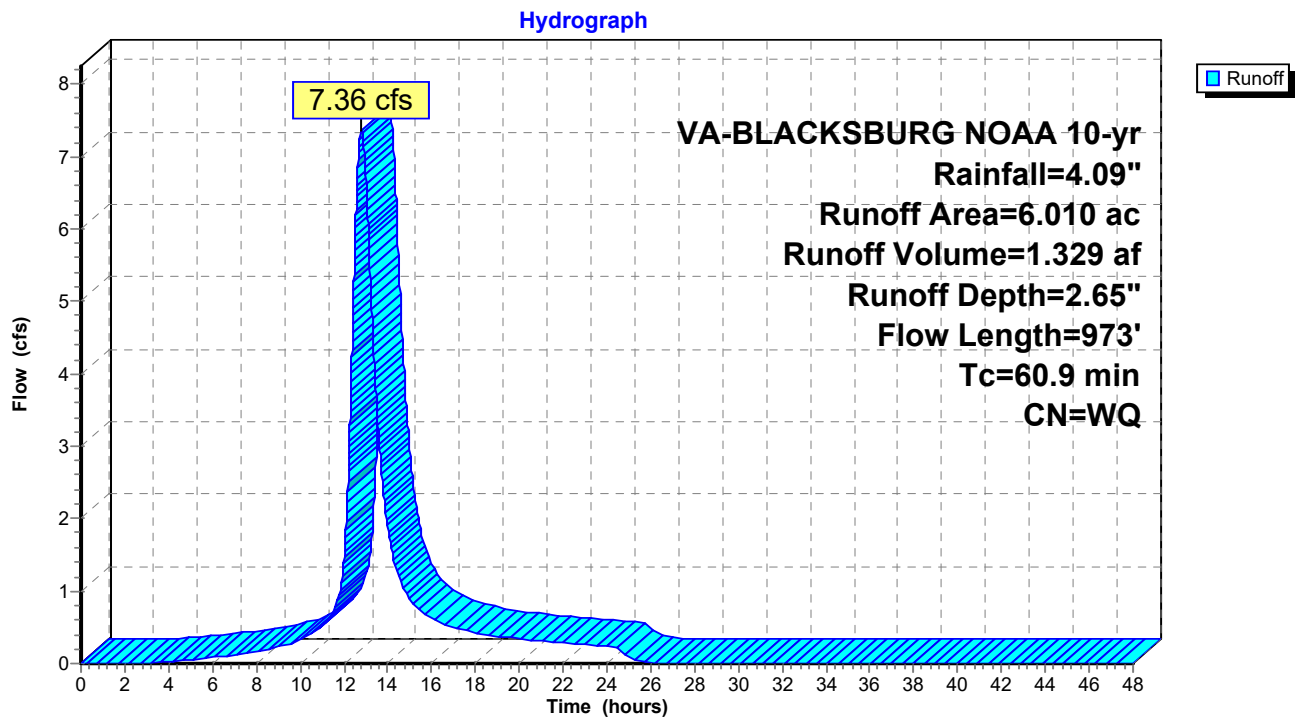
Area (ac)	CN	Description
0.433	61	>75% Grass cover, Good, HSG B
0.407	74	>75% Grass cover, Good, HSG C
0.270	55	Woods, Good, HSG B
0.076	70	Woods, Good, HSG C
0.164	70	1/2 acre lots, 25% imp, HSG B
0.371	80	1/2 acre lots, 25% imp, HSG C
0.282	75	1/4 acre lots, 38% imp, HSG B
0.496	83	1/4 acre lots, 38% imp, HSG C
0.044	85	1/8 acre lots, 65% imp, HSG B
0.685	92	Urban commercial, 85% imp, HSG B
2.402	94	Urban commercial, 85% imp, HSG C
0.047	98	Paved roads w/curbs & sewers, HSG B
0.209	98	Paved roads w/curbs & sewers, HSG C
0.068	98	Paved parking, HSG B
0.056	98	Paved parking, HSG C
6.010		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
52.4	150	0.0233	0.05		<b>Sheet Flow, Tc1</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
6.7	415	0.0422	1.03		<b>Shallow Concentrated Flow, Tc2</b> Woodland Kv= 5.0 fps
1.8	408	0.0564	3.82		<b>Shallow Concentrated Flow, Tc3</b> Unpaved Kv= 16.1 fps
60.9	973	Total			



# Subcatchment 1S: BYPASS AREA



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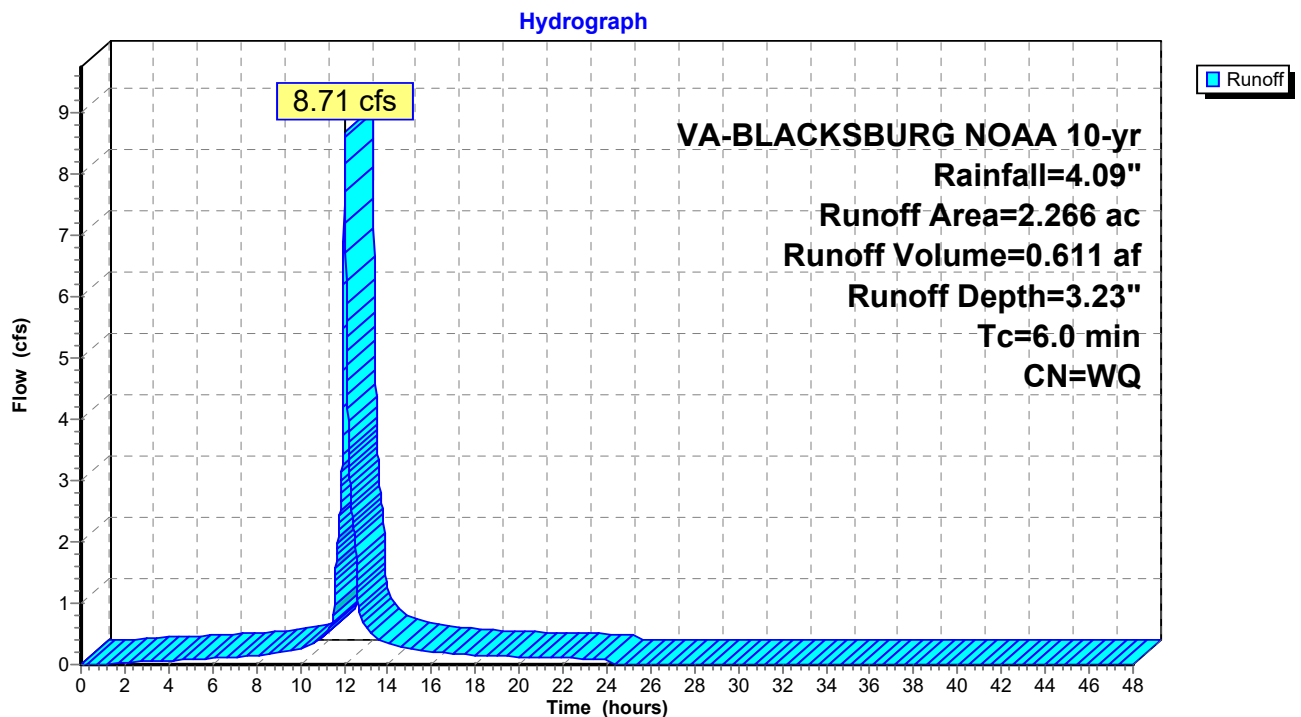
**Summary for Subcatchment 2S: DA TO DETENTION SYSTEM #1**

Runoff = 8.71 cfs @ 12.04 hrs, Volume= 0.611 af, Depth= 3.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

Area (ac)	CN	Description
0.176	61	>75% Grass cover, Good, HSG B
0.401	74	>75% Grass cover, Good, HSG C
0.339	98	Paved parking, HSG B
1.350	98	Paved parking, HSG C
2.266		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 2S: DA TO DETENTION SYSTEM #1**

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VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

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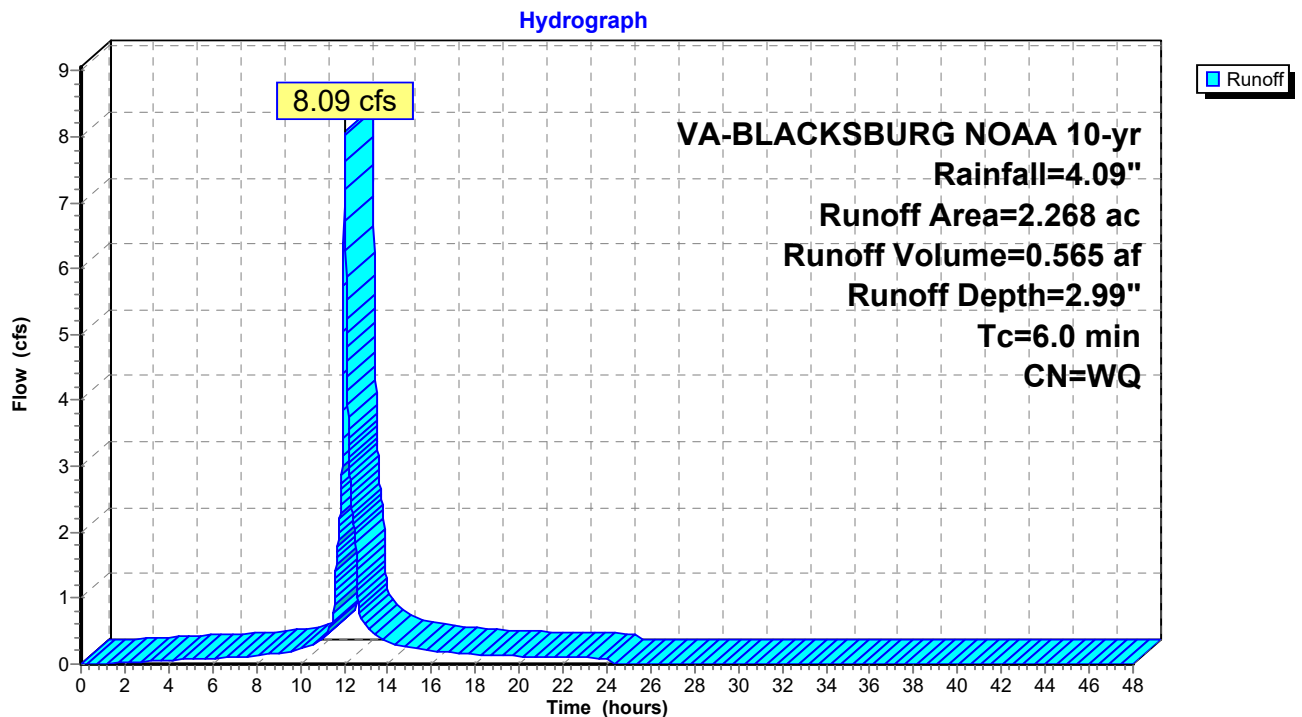
**Summary for Subcatchment 3S: DA TO DETENTION SYSTEM #2**

Runoff = 8.09 cfs @ 12.04 hrs, Volume= 0.565 af, Depth= 2.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

Area (ac)	CN	Description
0.071	61	>75% Grass cover, Good, HSG B
0.621	74	>75% Grass cover, Good, HSG C
0.064	55	Woods, Good, HSG B
0.074	70	Woods, Good, HSG C
0.135	98	Paved roads w/curbs & sewers, HSG C
0.131	98	Paved parking, HSG B
1.172	98	Paved parking, HSG C
2.268		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 3S: DA TO DETENTION SYSTEM #2**

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VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

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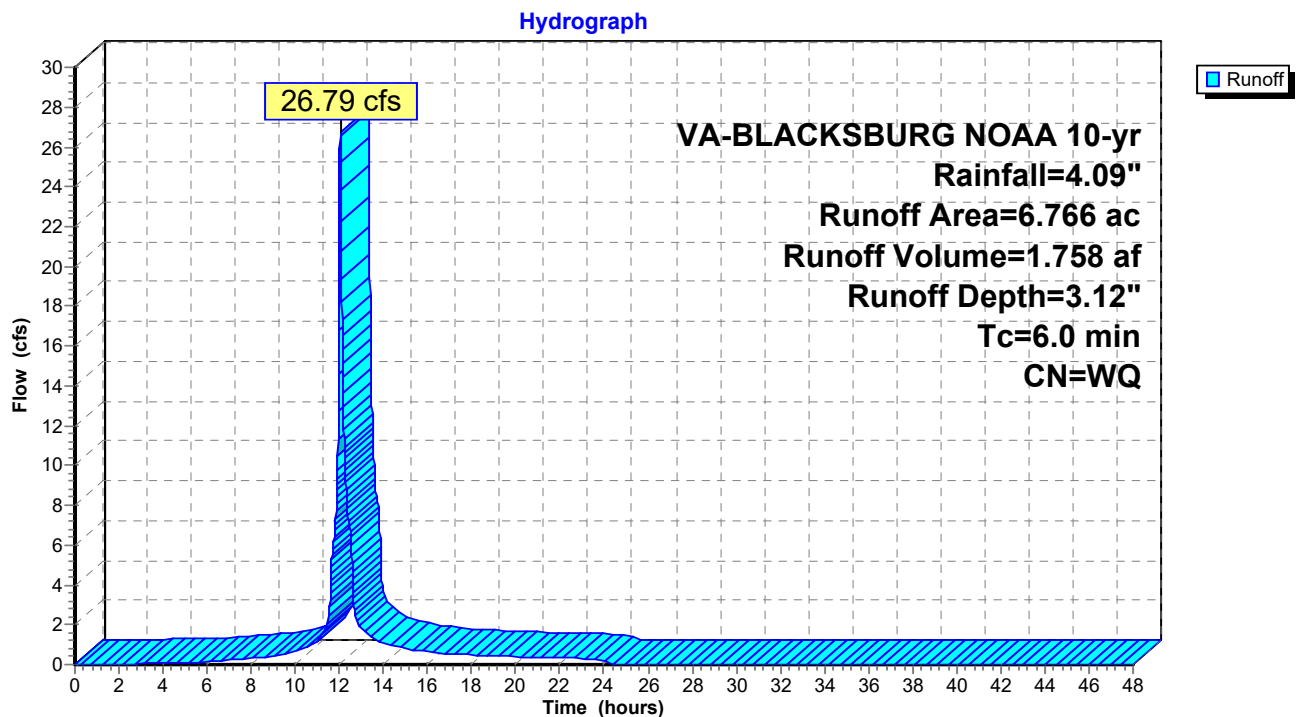
**Summary for Subcatchment 5S: BYPASS AREA**

Runoff = 26.79 cfs @ 12.04 hrs, Volume= 1.758 af, Depth= 3.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

Area (ac)	CN	Description
0.106	61	>75% Grass cover, Good, HSG B
0.044	74	>75% Grass cover, Good, HSG C
0.326	85	1/8 acre lots, 65% imp, HSG B
4.878	90	1/8 acre lots, 65% imp, HSG C
0.028	98	Paved roads w/curbs & sewers, HSG B
1.384	98	Paved roads w/curbs & sewers, HSG C
6.766		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 5S: BYPASS AREA**

**POST DEV**

VA-BLACKSBURG NOAA 10-yr Rainfall=4.09"

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**Summary for Pond 1P: UNDERGROUND DETENTION SYSTEM #1**

Inflow Area = 2.266 ac, Inflow Depth = 3.23" for 10-yr event  
 Inflow = 8.71 cfs @ 12.04 hrs, Volume= 0.611 af  
 Outflow = 5.50 cfs @ 12.12 hrs, Volume= 0.527 af, Atten= 37%, Lag= 5.3 min  
 Primary = 5.50 cfs @ 12.12 hrs, Volume= 0.527 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
 Peak Elev= 2,160.72' @ 12.12 hrs Surf.Area= 0.083 ac Storage= 0.254 af

Plug-Flow detention time= 453.6 min calculated for 0.527 af (86% of inflow)  
 Center-of-Mass det. time= 387.3 min ( 1,150.8 - 763.5 )

Volume	Invert	Avail.Storage	Storage Description
#1A	2,156.25'	0.097 af	<b>18.00'W x 202.00'L x 5.00'H Field A</b> 0.417 af Overall - 0.174 af Embedded = 0.243 af x 40.0% Voids
#2A	2,156.75'	0.174 af	<b>CMP Round 48 x 30 Inside #1</b> Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf Overall Size= 48.0"W x 48.0"H x 20.00'L Row Length Adjustment= -4.00' x 12.57 sf x 3 rows 16.00' Header x 12.57 sf x 1 = 201.1 cf Inside
		0.271 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	2,156.07'	<b>18.0" Round 18" HDPE</b> L= 82.4' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 2,156.07' / 2,155.51' S= 0.0068 ' S= 0.0068 ' Cc= 0.900 n= 0.011, Flow Area= 1.77 sf
#2	Device 1	2,156.07'	<b>1.2" Vert. 1" Orifice</b> C= 0.600
#3	Device 1	2,159.75'	<b>5.0" Vert. 3" Orifice</b> C= 0.600
#4	Device 1	2,160.25'	<b>5.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=5.48 cfs @ 12.12 hrs HW=2,160.72' (Free Discharge)

- 1=18" HDPE (Passes 5.48 cfs of 16.81 cfs potential flow)
- 2=1" Orifice (Orifice Controls 0.08 cfs @ 10.33 fps)
- 3=3" Orifice (Orifice Controls 0.57 cfs @ 4.21 fps)
- 4=Broad-Crested Rectangular Weir (Weir Controls 4.82 cfs @ 2.04 fps)

## POST DEV

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### Pond 1P: UNDERGROUND DETENTION SYSTEM #1 - Chamber Wizard Field A

#### Chamber Model = CMP Round 48 (Round Corrugated Metal Pipe)

Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf

Overall Size= 48.0"W x 48.0"H x 20.00'L

Row Length Adjustment= -4.00' x 12.57 sf x 3 rows

48.0" Wide + 24.0" Spacing = 72.0" C-C Row Spacing

10 Chambers/Row x 20.00' Long -4.00' Row Adjustment +4.00' Header x 1 = 200.00' Row Length +12.0"  
End Stone x 2 = 202.00' Base Length

3 Rows x 48.0" Wide + 24.0" Spacing x 2 + 12.0" Side Stone x 2 = 18.00' Base Width

6.0" Base + 48.0" Chamber Height + 6.0" Cover = 5.00' Field Height

30 Chambers x 251.3 cf -4.00' Row Adjustment x 12.57 sf x 3 Rows + 16.00' Header x 12.57 sf =  
7,590.1 cf Chamber Storage

18,180.0 cf Field - 7,590.1 cf Chambers = 10,589.9 cf Stone x 40.0% Voids = 4,236.0 cf Stone Storage

Chamber Storage + Stone Storage = 11,826.1 cf = 0.271 af

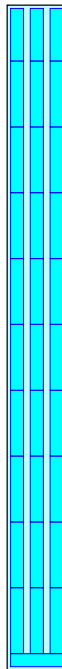
Overall Storage Efficiency = 65.0%

Overall System Size = 202.00' x 18.00' x 5.00'

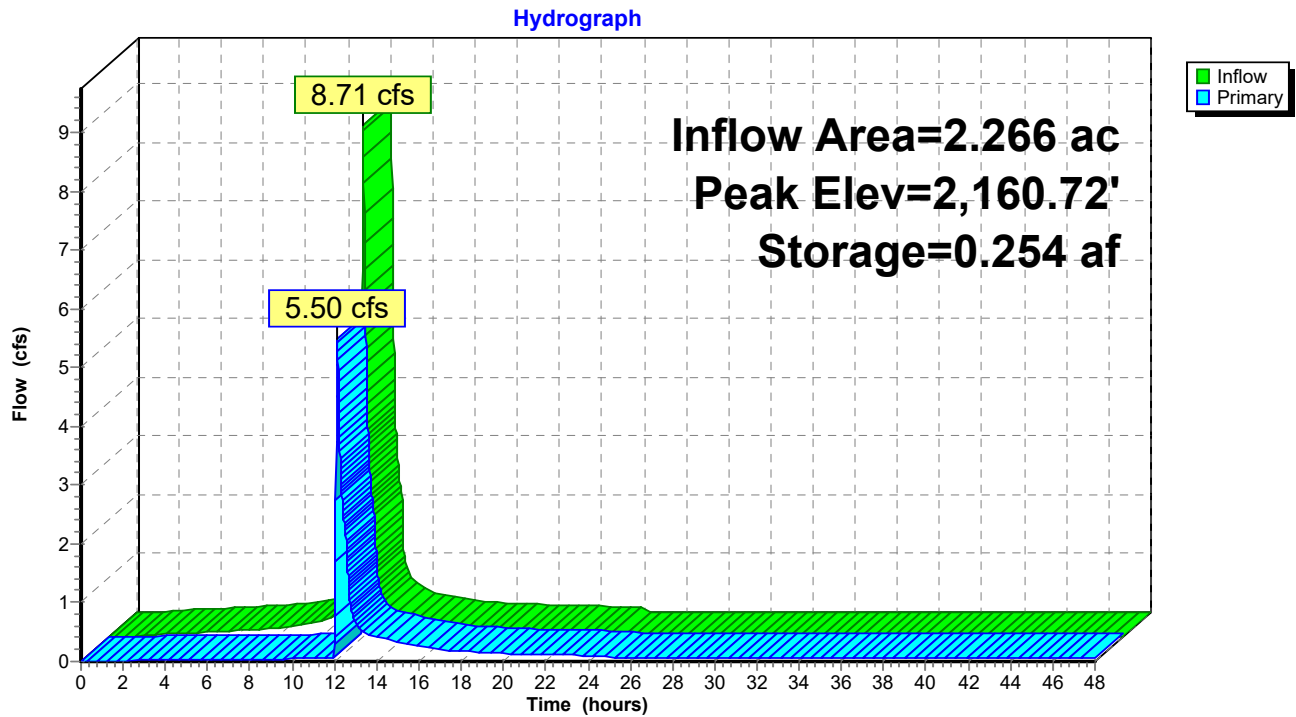
30 Chambers

673.3 cy Field

392.2 cy Stone



# Pond 1P: UNDERGROUND DETENTION SYSTEM #1



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**Summary for Pond 2P: UNDERGROUND DETENTION SYSTEM #2**

Inflow Area = 2.268 ac, Inflow Depth = 2.99" for 10-yr event  
 Inflow = 8.09 cfs @ 12.04 hrs, Volume= 0.565 af  
 Outflow = 3.51 cfs @ 12.20 hrs, Volume= 0.558 af, Atten= 57%, Lag= 10.0 min  
 Primary = 3.51 cfs @ 12.20 hrs, Volume= 0.558 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
 Peak Elev= 2,158.48' @ 12.20 hrs Surf.Area= 0.075 ac Storage= 0.229 af

Plug-Flow detention time= 514.3 min calculated for 0.558 af (99% of inflow)  
 Center-of-Mass det. time= 506.7 min ( 1,277.3 - 770.6 )

Volume	Invert	Avail.Storage	Storage Description
#1A	2,154.00'	0.088 af	<b>18.00'W x 182.00'L x 5.00'H Field A</b> 0.376 af Overall - 0.157 af Embedded = 0.219 af x 40.0% Voids
#2A	2,154.50'	0.157 af	<b>CMP Round 48 x 27 Inside #1</b> Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf Overall Size= 48.0"W x 48.0"H x 20.00'L Row Length Adjustment= -4.00' x 12.57 sf x 3 rows 16.00' Header x 12.57 sf x 1 = 201.1 cf Inside
		0.245 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	2,153.85'	<b>15.0" Round 15" HDPE</b> L= 37.1' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 2,153.85' / 2,153.55' S= 0.0081 '/' Cc= 0.900 n= 0.011, Flow Area= 1.23 sf
#2	Device 1	2,153.85'	<b>Reg-U-Flo SXH 3.0-in</b>
#3	Device 1	2,158.00'	<b>8.0" W x 4.0" H Vert. Orifice/Grate C= 0.600</b>
#4	Device 1	2,158.15'	<b>5.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=3.50 cfs @ 12.20 hrs HW=2,158.48' (Free Discharge)

- 1=15" HDPE (Passes 3.50 cfs of 11.83 cfs potential flow)
- 2=Reg-U-Flo SXH 3.0-in (Custom Controls 0.14 cfs)
- 3=Orifice/Grate (Orifice Controls 0.59 cfs @ 2.68 fps)
- 4=Broad-Crested Rectangular Weir (Weir Controls 2.77 cfs @ 1.66 fps)



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### Pond 2P: UNDERGROUND DETENTION SYSTEM #2 - Chamber Wizard Field A

#### Chamber Model = CMP Round 48 (Round Corrugated Metal Pipe)

Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf

Overall Size= 48.0"W x 48.0"H x 20.00'L

Row Length Adjustment= -4.00' x 12.57 sf x 3 rows

48.0" Wide + 24.0" Spacing = 72.0" C-C Row Spacing

9 Chambers/Row x 20.00' Long -4.00' Row Adjustment +4.00' Header x 1 = 180.00' Row Length +12.0"

End Stone x 2 = 182.00' Base Length

3 Rows x 48.0" Wide + 24.0" Spacing x 2 + 12.0" Side Stone x 2 = 18.00' Base Width

6.0" Base + 48.0" Chamber Height + 6.0" Cover = 5.00' Field Height

27 Chambers x 251.3 cf -4.00' Row Adjustment x 12.57 sf x 3 Rows + 16.00' Header x 12.57 sf =  
6,836.1 cf Chamber Storage

16,380.0 cf Field - 6,836.1 cf Chambers = 9,543.9 cf Stone x 40.0% Voids = 3,817.6 cf Stone Storage

Chamber Storage + Stone Storage = 10,653.7 cf = 0.245 af

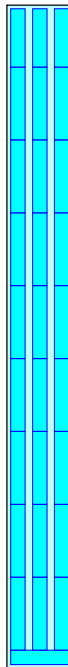
Overall Storage Efficiency = 65.0%

Overall System Size = 182.00' x 18.00' x 5.00'

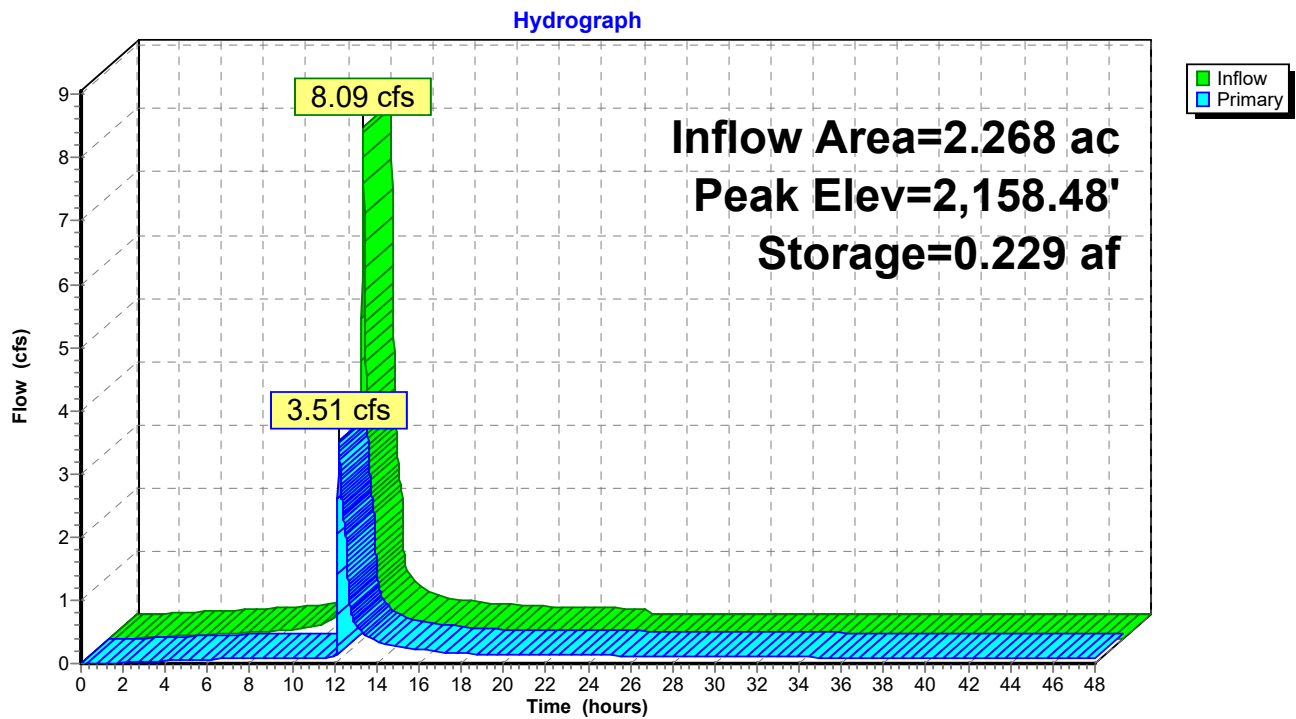
27 Chambers

606.7 cy Field

353.5 cy Stone



## Pond 2P: UNDERGROUND DETENTION SYSTEM #2



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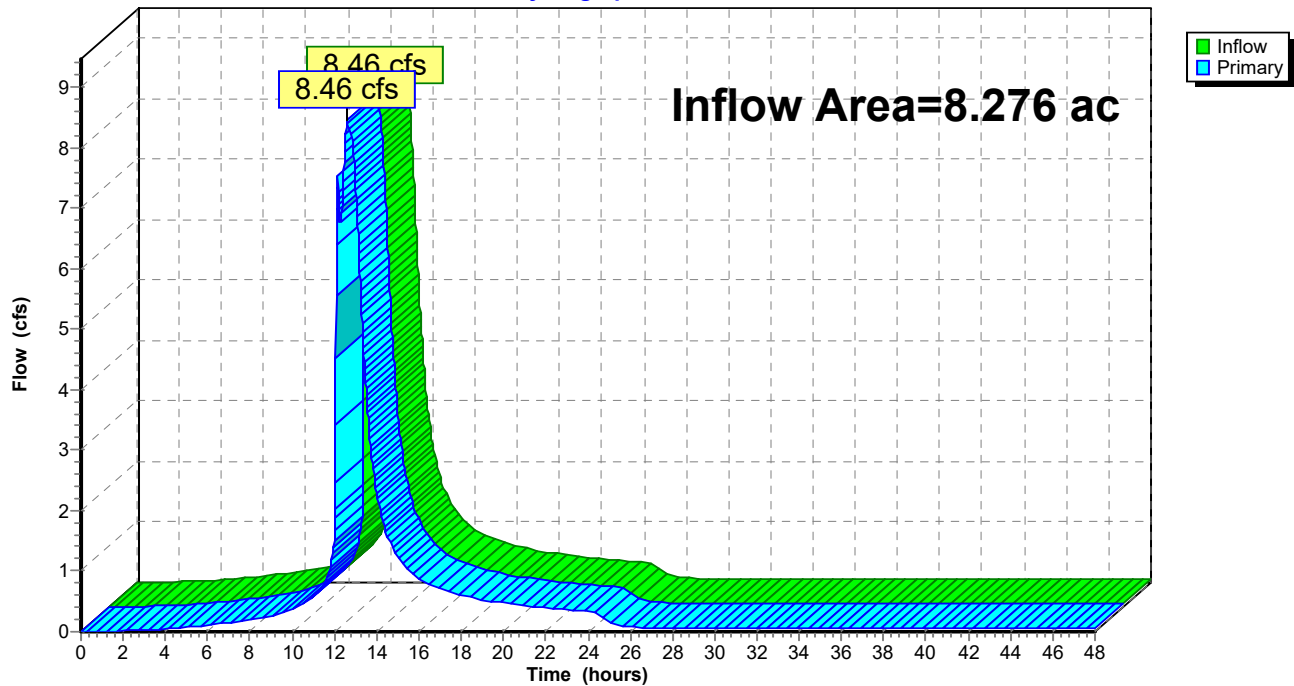
### Summary for Link 1L: POA #1

Inflow Area = 8.276 ac, Inflow Depth > 2.69" for 10-yr event  
Inflow = 8.46 cfs @ 12.59 hrs, Volume= 1.856 af  
Primary = 8.46 cfs @ 12.59 hrs, Volume= 1.856 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 1L: POA #1

Hydrograph



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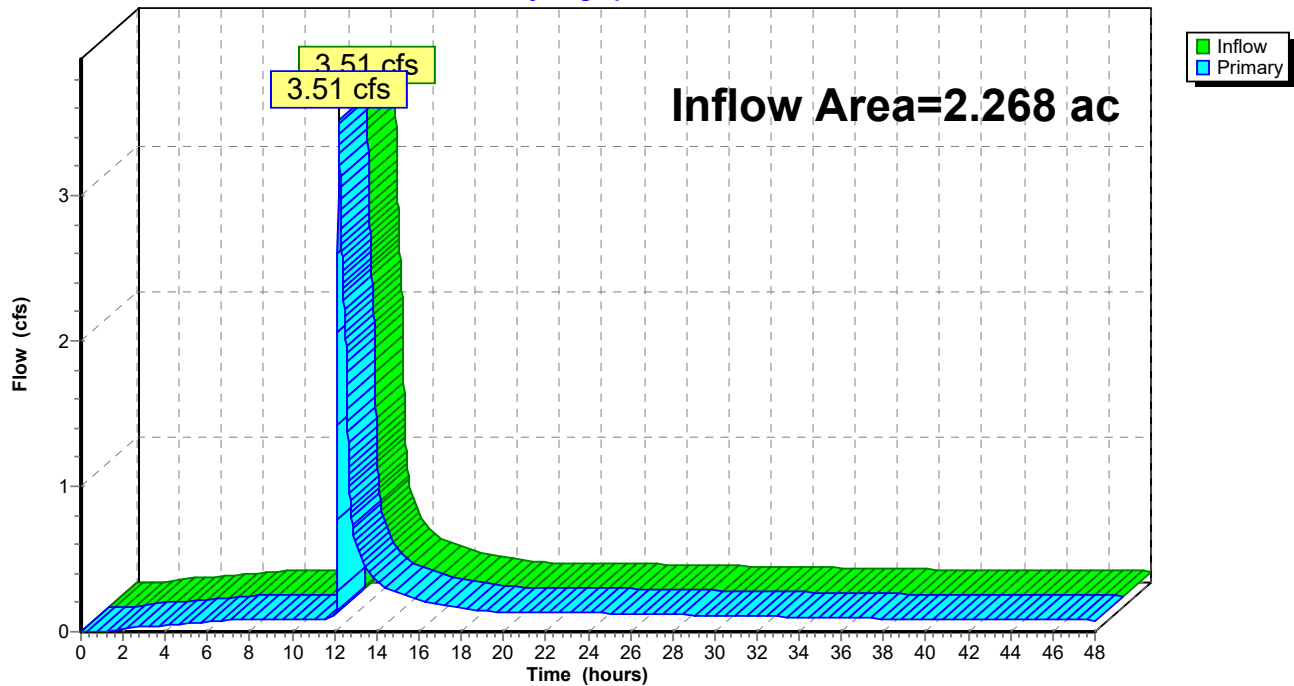
### Summary for Link 2L: MH-A

Inflow Area = 2.268 ac, Inflow Depth > 2.95" for 10-yr event  
Inflow = 3.51 cfs @ 12.20 hrs, Volume= 0.558 af  
Primary = 3.51 cfs @ 12.20 hrs, Volume= 0.558 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 2L: MH-A

Hydrograph



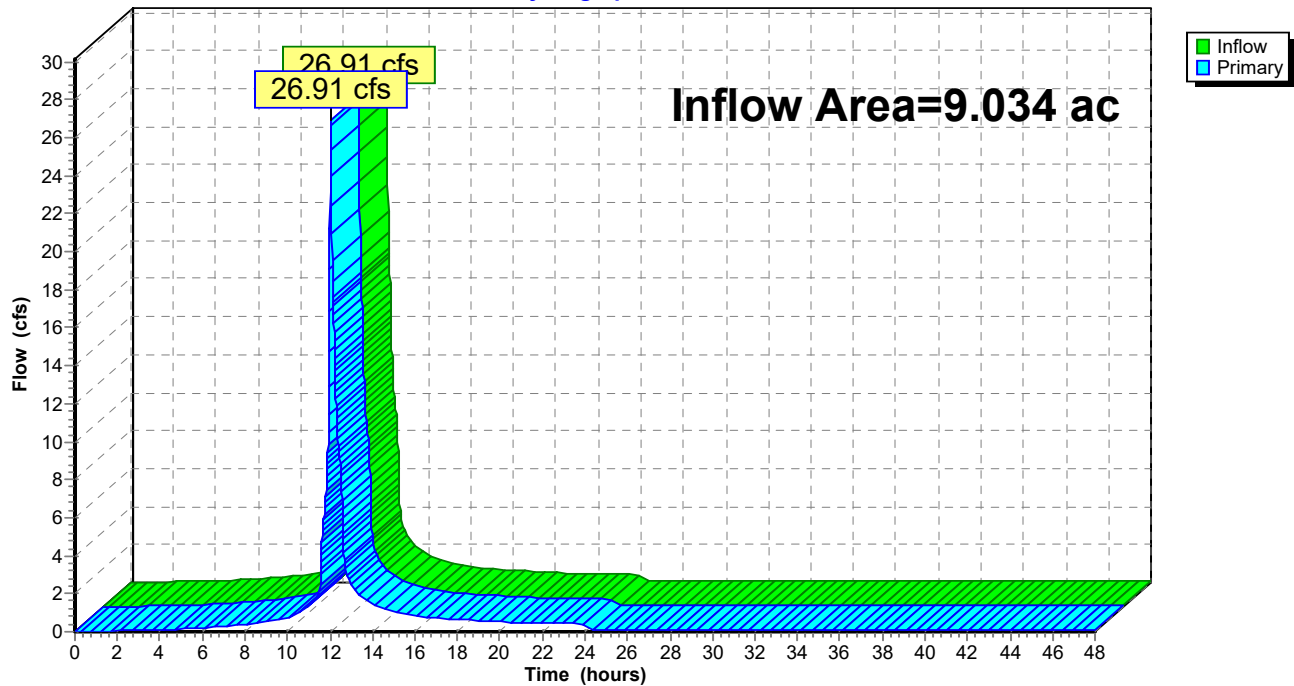
### Summary for Link 3L: POA #2

Inflow Area = 9.034 ac, Inflow Depth > 3.08" for 10-yr event  
 Inflow = 26.91 cfs @ 12.04 hrs, Volume= 2.316 af  
 Primary = 26.91 cfs @ 12.04 hrs, Volume= 2.316 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 3L: POA #2

Hydrograph



**POST DEV**

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q  
Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

**Subcatchment1S: BYPASS AREA**

Runoff Area=6.010 ac Runoff Depth=4.80"  
Flow Length=973' Tc=60.9 min CN=WQ Runoff=12.05 cfs 2.402 af

**Subcatchment2S: DA TO DETENTION SYSTEM #1**

Runoff Area=2.266 ac Runoff Depth=5.47"  
Tc=6.0 min CN=WQ Runoff=12.43 cfs 1.033 af

**Subcatchment3S: DA TO DETENTION SYSTEM #2**

Runoff Area=2.268 ac Runoff Depth=5.17"  
Tc=6.0 min CN=WQ Runoff=11.88 cfs 0.977 af

**Subcatchment5S: BYPASS AREA**

Runoff Area=6.766 ac Runoff Depth=5.42"  
Tc=6.0 min CN=WQ Runoff=38.63 cfs 3.058 af

**Pond 1P: UNDERGROUND DETENTION**

Peak Elev=2,161.03' Storage=0.264 af Inflow=12.43 cfs 1.033 af  
Outflow=12.12 cfs 0.946 af

**Pond 2P: UNDERGROUND DETENTION**

Peak Elev=2,158.90' Storage=0.242 af Inflow=11.88 cfs 0.977 af  
Outflow=11.63 cfs 0.963 af

**Link 1L: POA #1**

Inflow=15.35 cfs 3.349 af  
Primary=15.35 cfs 3.349 af

**Link 2L: MH-A**

Inflow=11.63 cfs 0.963 af  
Primary=11.63 cfs 0.963 af

**Link 3L: POA #2**

Inflow=50.06 cfs 4.020 af  
Primary=50.06 cfs 4.020 af

**Total Runoff Area = 17.310 ac Runoff Volume = 7.469 af Average Runoff Depth = 5.18"**

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**Summary for Subcatchment 1S: BYPASS AREA**

Runoff = 12.05 cfs @ 12.79 hrs, Volume= 2.402 af, Depth= 4.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

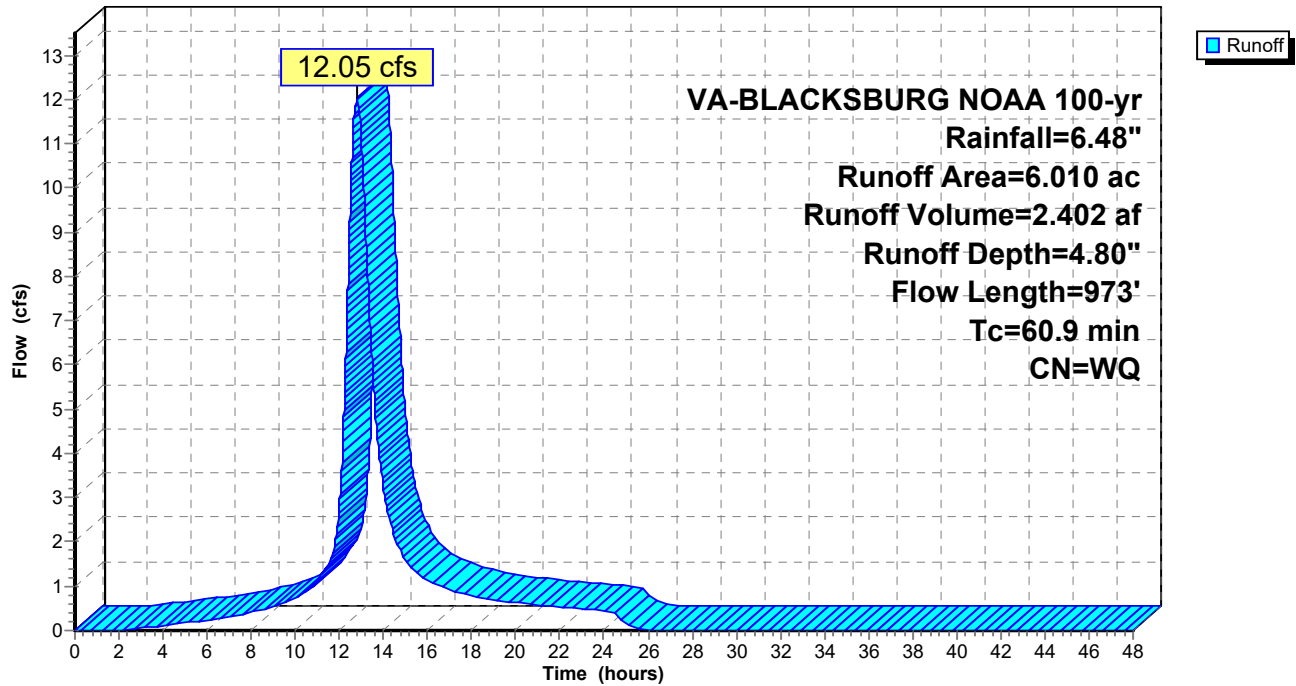
Area (ac)	CN	Description
0.433	61	>75% Grass cover, Good, HSG B
0.407	74	>75% Grass cover, Good, HSG C
0.270	55	Woods, Good, HSG B
0.076	70	Woods, Good, HSG C
0.164	70	1/2 acre lots, 25% imp, HSG B
0.371	80	1/2 acre lots, 25% imp, HSG C
0.282	75	1/4 acre lots, 38% imp, HSG B
0.496	83	1/4 acre lots, 38% imp, HSG C
0.044	85	1/8 acre lots, 65% imp, HSG B
0.685	92	Urban commercial, 85% imp, HSG B
2.402	94	Urban commercial, 85% imp, HSG C
0.047	98	Paved roads w/curbs & sewers, HSG B
0.209	98	Paved roads w/curbs & sewers, HSG C
0.068	98	Paved parking, HSG B
0.056	98	Paved parking, HSG C
6.010		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
52.4	150	0.0233	0.05		<b>Sheet Flow, Tc1</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
6.7	415	0.0422	1.03		<b>Shallow Concentrated Flow, Tc2</b> Woodland Kv= 5.0 fps
1.8	408	0.0564	3.82		<b>Shallow Concentrated Flow, Tc3</b> Unpaved Kv= 16.1 fps
60.9	973	Total			

# Subcatchment 1S: BYPASS AREA

Hydrograph





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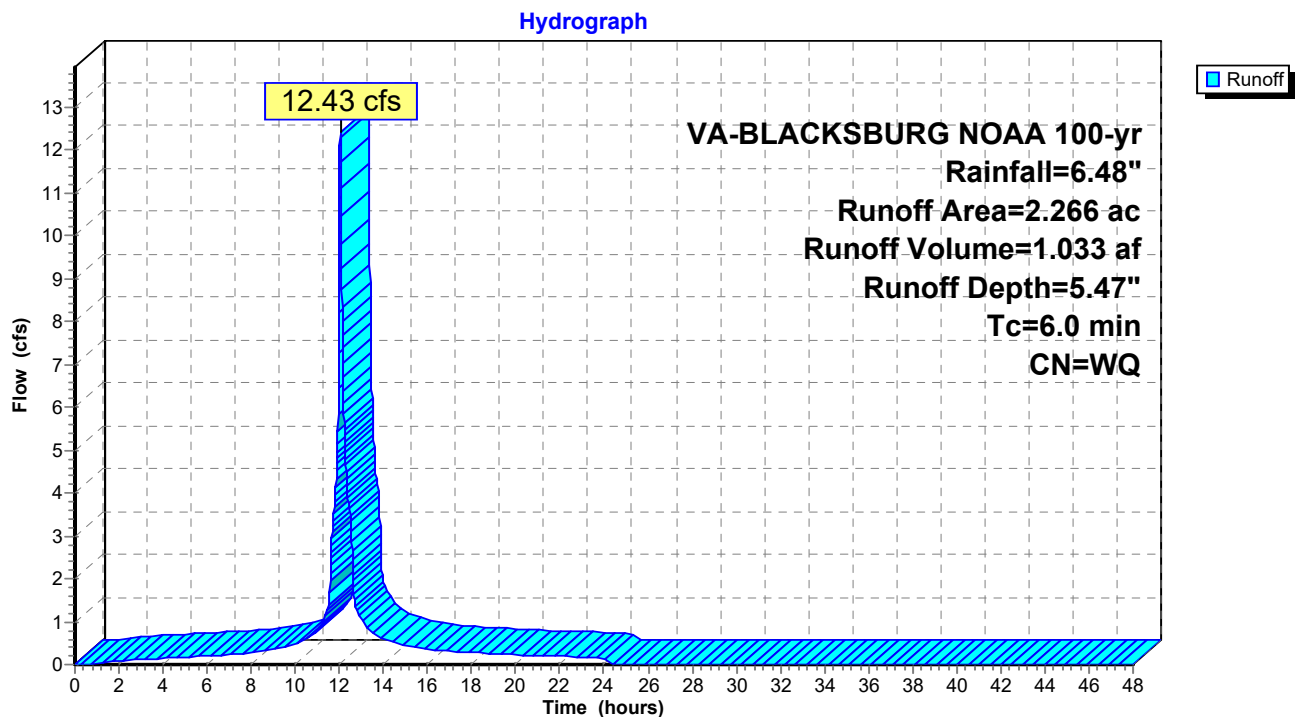
**Summary for Subcatchment 2S: DA TO DETENTION SYSTEM #1**

Runoff = 12.43 cfs @ 12.04 hrs, Volume= 1.033 af, Depth= 5.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

Area (ac)	CN	Description
0.176	61	>75% Grass cover, Good, HSG B
0.401	74	>75% Grass cover, Good, HSG C
0.339	98	Paved parking, HSG B
1.350	98	Paved parking, HSG C
2.266		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 2S: DA TO DETENTION SYSTEM #1**

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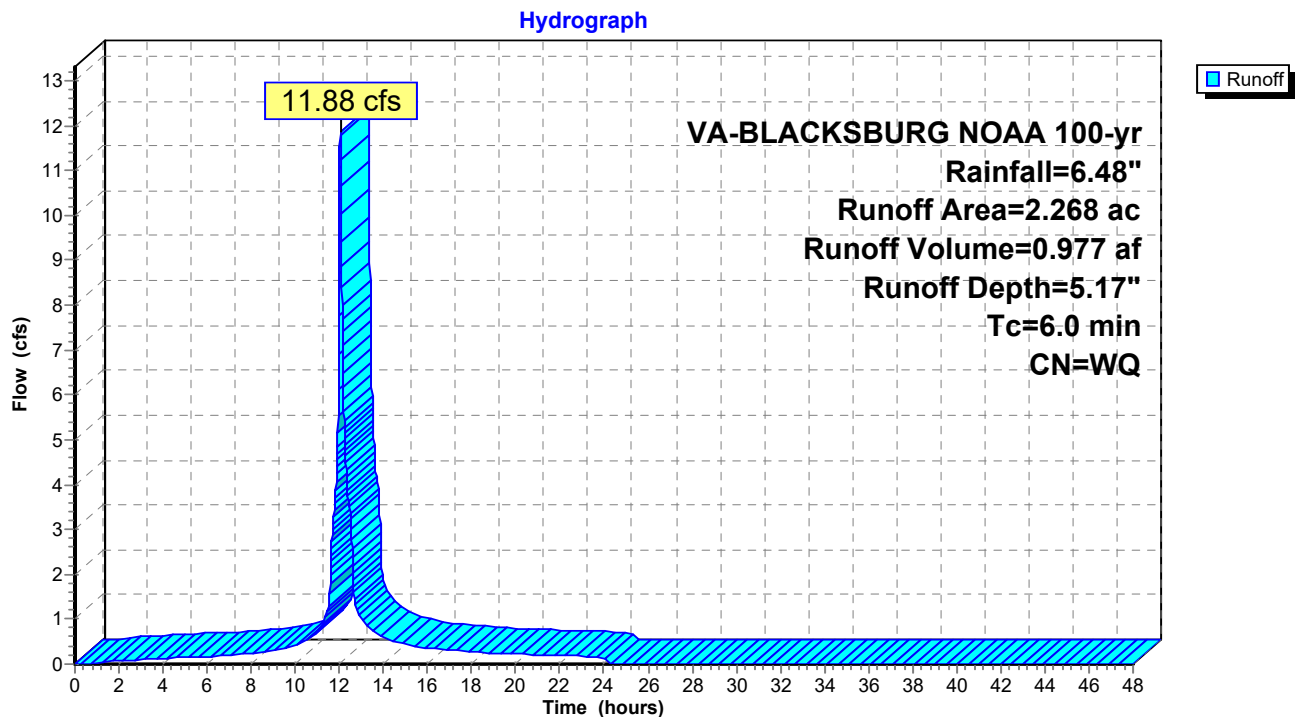
**Summary for Subcatchment 3S: DA TO DETENTION SYSTEM #2**

Runoff = 11.88 cfs @ 12.04 hrs, Volume= 0.977 af, Depth= 5.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

Area (ac)	CN	Description
0.071	61	>75% Grass cover, Good, HSG B
0.621	74	>75% Grass cover, Good, HSG C
0.064	55	Woods, Good, HSG B
0.074	70	Woods, Good, HSG C
0.135	98	Paved roads w/curbs & sewers, HSG C
0.131	98	Paved parking, HSG B
1.172	98	Paved parking, HSG C
2.268		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 3S: DA TO DETENTION SYSTEM #2**

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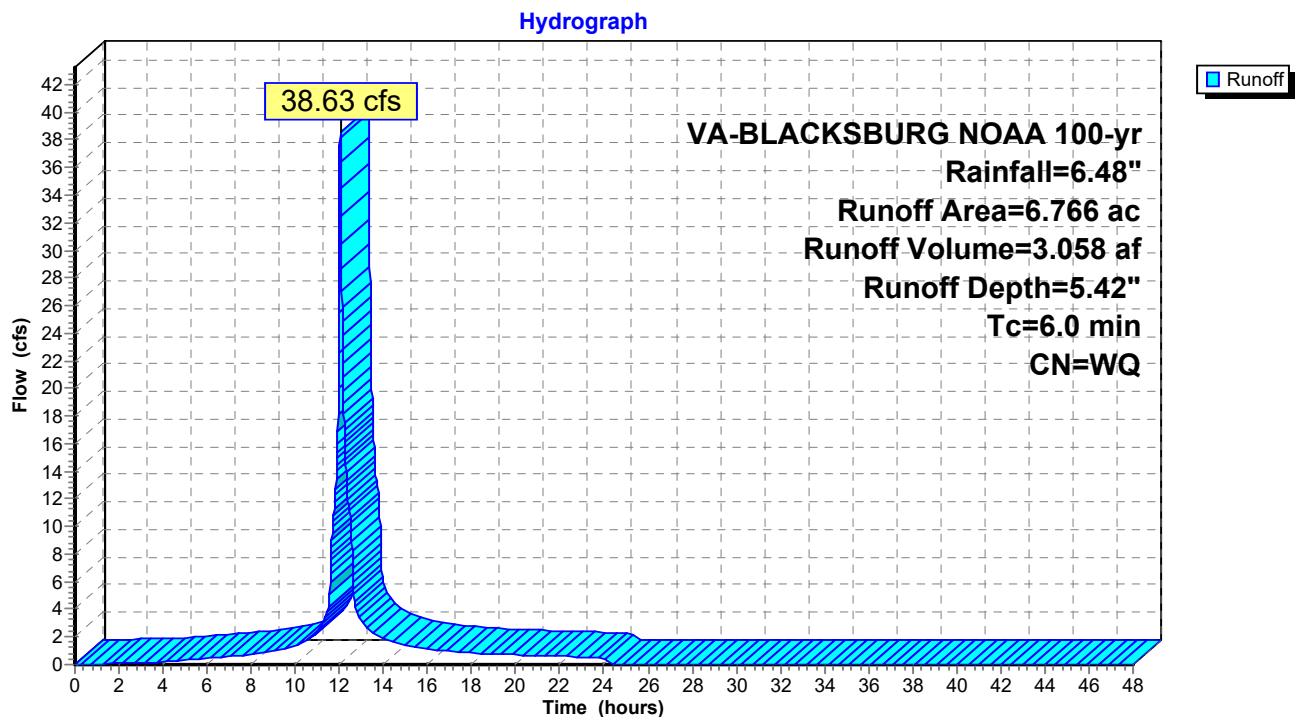
**Summary for Subcatchment 5S: BYPASS AREA**

Runoff = 38.63 cfs @ 12.04 hrs, Volume= 3.058 af, Depth= 5.42"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

Area (ac)	CN	Description
0.106	61	>75% Grass cover, Good, HSG B
0.044	74	>75% Grass cover, Good, HSG C
0.326	85	1/8 acre lots, 65% imp, HSG B
4.878	90	1/8 acre lots, 65% imp, HSG C
0.028	98	Paved roads w/curbs & sewers, HSG B
1.384	98	Paved roads w/curbs & sewers, HSG C
6.766		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 5S: BYPASS AREA**

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**Summary for Pond 1P: UNDERGROUND DETENTION SYSTEM #1**

Inflow Area = 2.266 ac, Inflow Depth = 5.47" for 100-yr event  
 Inflow = 12.43 cfs @ 12.04 hrs, Volume= 1.033 af  
 Outflow = 12.12 cfs @ 12.05 hrs, Volume= 0.946 af, Atten= 2%, Lag= 0.9 min  
 Primary = 12.12 cfs @ 12.05 hrs, Volume= 0.946 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
 Peak Elev= 2,161.03' @ 12.05 hrs Surf.Area= 0.083 ac Storage= 0.264 af

Plug-Flow detention time= 293.2 min calculated for 0.946 af (92% of inflow)  
 Center-of-Mass det. time= 245.7 min ( 1,004.6 - 758.9 )

Volume	Invert	Avail.Storage	Storage Description
#1A	2,156.25'	0.097 af	<b>18.00'W x 202.00'L x 5.00'H Field A</b> 0.417 af Overall - 0.174 af Embedded = 0.243 af x 40.0% Voids
#2A	2,156.75'	0.174 af	<b>CMP Round 48 x 30 Inside #1</b> Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf Overall Size= 48.0"W x 48.0"H x 20.00'L Row Length Adjustment= -4.00' x 12.57 sf x 3 rows 16.00' Header x 12.57 sf x 1 = 201.1 cf Inside
		0.271 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	2,156.07'	<b>18.0" Round 18" HDPE</b> L= 82.4' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 2,156.07' / 2,155.51' S= 0.0068 ' S= 0.0068 ' Cc= 0.900 n= 0.011, Flow Area= 1.77 sf
#2	Device 1	2,156.07'	<b>1.2" Vert. 1" Orifice</b> C= 0.600
#3	Device 1	2,159.75'	<b>5.0" Vert. 3" Orifice</b> C= 0.600
#4	Device 1	2,160.25'	<b>5.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=12.09 cfs @ 12.05 hrs HW=2,161.03' (Free Discharge)

- 1=18" HDPE (Passes 12.09 cfs of 17.46 cfs potential flow)
- 2=1" Orifice (Orifice Controls 0.08 cfs @ 10.67 fps)
- 3=3" Orifice (Orifice Controls 0.68 cfs @ 4.99 fps)
- 4=Broad-Crested Rectangular Weir (Weir Controls 11.33 cfs @ 2.90 fps)

## POST DEV

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VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

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### Pond 1P: UNDERGROUND DETENTION SYSTEM #1 - Chamber Wizard Field A

#### Chamber Model = CMP Round 48 (Round Corrugated Metal Pipe)

Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf

Overall Size= 48.0"W x 48.0"H x 20.00'L

Row Length Adjustment= -4.00' x 12.57 sf x 3 rows

48.0" Wide + 24.0" Spacing = 72.0" C-C Row Spacing

10 Chambers/Row x 20.00' Long -4.00' Row Adjustment +4.00' Header x 1 = 200.00' Row Length +12.0"  
End Stone x 2 = 202.00' Base Length

3 Rows x 48.0" Wide + 24.0" Spacing x 2 + 12.0" Side Stone x 2 = 18.00' Base Width

6.0" Base + 48.0" Chamber Height + 6.0" Cover = 5.00' Field Height

30 Chambers x 251.3 cf -4.00' Row Adjustment x 12.57 sf x 3 Rows + 16.00' Header x 12.57 sf =  
7,590.1 cf Chamber Storage

18,180.0 cf Field - 7,590.1 cf Chambers = 10,589.9 cf Stone x 40.0% Voids = 4,236.0 cf Stone Storage

Chamber Storage + Stone Storage = 11,826.1 cf = 0.271 af

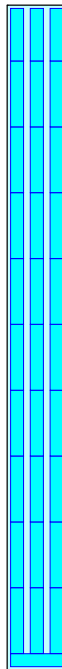
Overall Storage Efficiency = 65.0%

Overall System Size = 202.00' x 18.00' x 5.00'

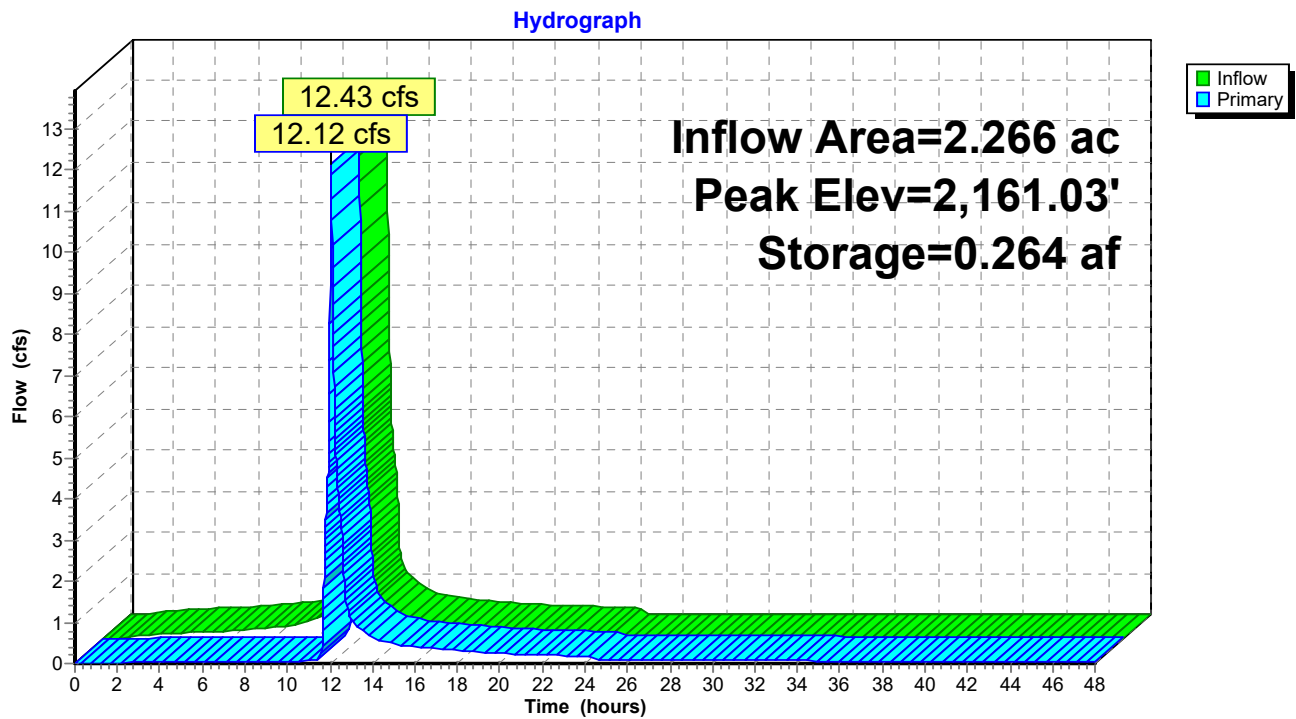
30 Chambers

673.3 cy Field

392.2 cy Stone



# Pond 1P: UNDERGROUND DETENTION SYSTEM #1



**POST DEV**

VA-BLACKSBURG NOAA 100-yr Rainfall=6.48"

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**Summary for Pond 2P: UNDERGROUND DETENTION SYSTEM #2**

Inflow Area = 2.268 ac, Inflow Depth = 5.17" for 100-yr event  
 Inflow = 11.88 cfs @ 12.04 hrs, Volume= 0.977 af  
 Outflow = 11.63 cfs @ 12.05 hrs, Volume= 0.963 af, Atten= 2%, Lag= 0.8 min  
 Primary = 11.63 cfs @ 12.05 hrs, Volume= 0.963 af

Routing by Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
 Peak Elev= 2,158.90' @ 12.05 hrs Surf.Area= 0.075 ac Storage= 0.242 af

Plug-Flow detention time= 323.1 min calculated for 0.963 af (99% of inflow)  
 Center-of-Mass det. time= 313.5 min ( 1,080.3 - 766.8 )

Volume	Invert	Avail.Storage	Storage Description
#1A	2,154.00'	0.088 af	<b>18.00'W x 182.00'L x 5.00'H Field A</b> 0.376 af Overall - 0.157 af Embedded = 0.219 af x 40.0% Voids
#2A	2,154.50'	0.157 af	<b>CMP Round 48 x 27 Inside #1</b> Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf Overall Size= 48.0"W x 48.0"H x 20.00'L Row Length Adjustment= -4.00' x 12.57 sf x 3 rows 16.00' Header x 12.57 sf x 1 = 201.1 cf Inside
		0.245 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	2,153.85'	<b>15.0" Round 15" HDPE</b> L= 37.1' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 2,153.85' / 2,153.55' S= 0.0081 '/' Cc= 0.900 n= 0.011, Flow Area= 1.23 sf
#2	Device 1	2,153.85'	<b>Reg-U-Flo SXH 3.0-in</b>
#3	Device 1	2,158.00'	<b>8.0" W x 4.0" H Vert. Orifice/Grate C= 0.600</b>
#4	Device 1	2,158.15'	<b>5.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=11.61 cfs @ 12.05 hrs HW=2,158.90' (Free Discharge)

- 1=15" HDPE (Passes 11.61 cfs of 12.43 cfs potential flow)
- 2=Reg-U-Flo SXH 3.0-in (Custom Controls 0.15 cfs)
- 3=Orifice/Grate (Orifice Controls 0.91 cfs @ 4.12 fps)
- 4=Broad-Crested Rectangular Weir (Weir Controls 10.55 cfs @ 2.81 fps)

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### Pond 2P: UNDERGROUND DETENTION SYSTEM #2 - Chamber Wizard Field A

#### Chamber Model = CMP Round 48 (Round Corrugated Metal Pipe)

Effective Size= 48.0"W x 48.0"H => 12.57 sf x 20.00'L = 251.3 cf

Overall Size= 48.0"W x 48.0"H x 20.00'L

Row Length Adjustment= -4.00' x 12.57 sf x 3 rows

48.0" Wide + 24.0" Spacing = 72.0" C-C Row Spacing

9 Chambers/Row x 20.00' Long -4.00' Row Adjustment +4.00' Header x 1 = 180.00' Row Length +12.0"

End Stone x 2 = 182.00' Base Length

3 Rows x 48.0" Wide + 24.0" Spacing x 2 + 12.0" Side Stone x 2 = 18.00' Base Width

6.0" Base + 48.0" Chamber Height + 6.0" Cover = 5.00' Field Height

27 Chambers x 251.3 cf -4.00' Row Adjustment x 12.57 sf x 3 Rows + 16.00' Header x 12.57 sf =  
6,836.1 cf Chamber Storage

16,380.0 cf Field - 6,836.1 cf Chambers = 9,543.9 cf Stone x 40.0% Voids = 3,817.6 cf Stone Storage

Chamber Storage + Stone Storage = 10,653.7 cf = 0.245 af

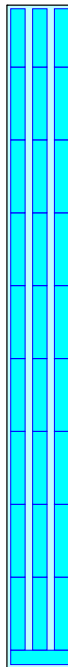
Overall Storage Efficiency = 65.0%

Overall System Size = 182.00' x 18.00' x 5.00'

27 Chambers

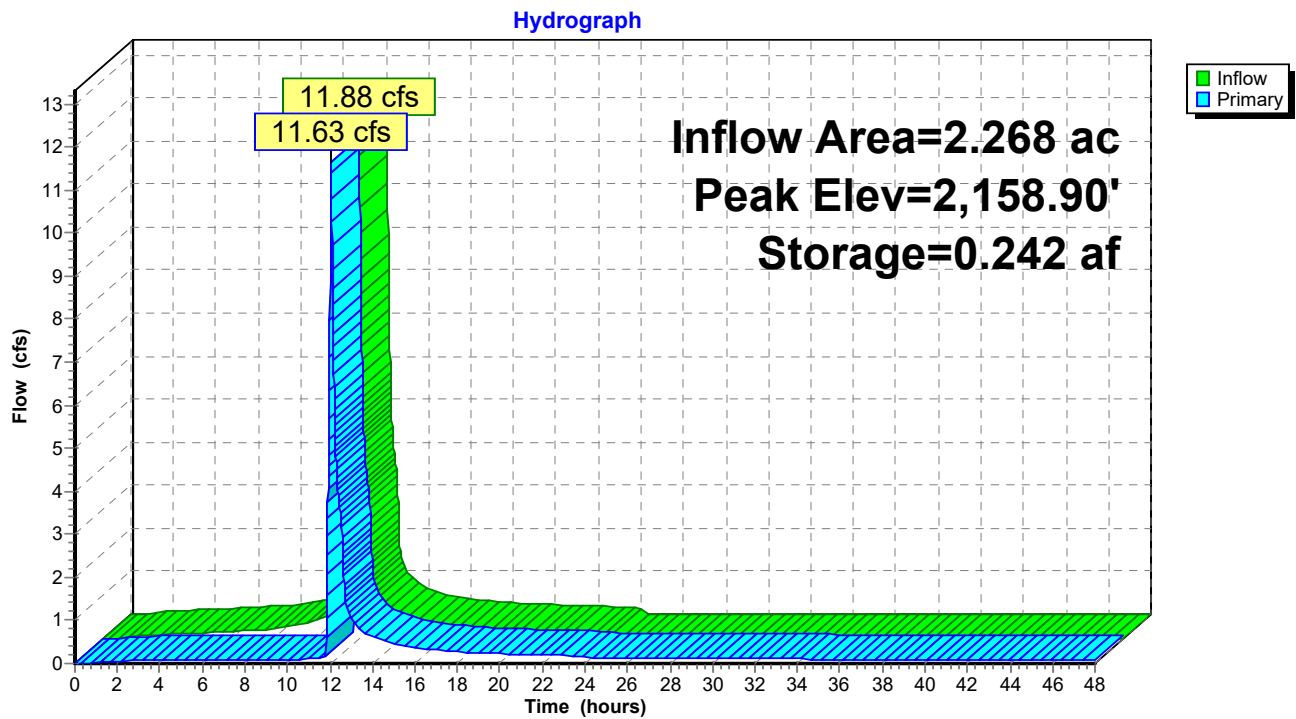
606.7 cy Field

353.5 cy Stone





## Pond 2P: UNDERGROUND DETENTION SYSTEM #2



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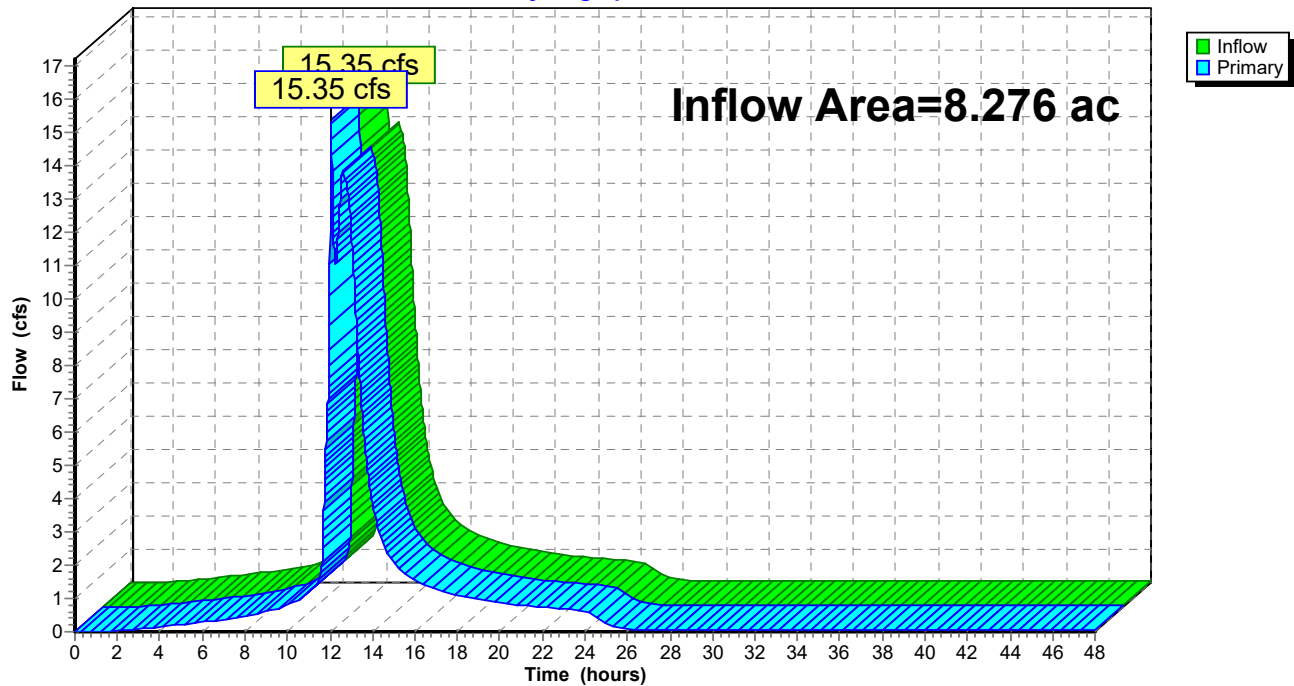
### Summary for Link 1L: POA #1

Inflow Area = 8.276 ac, Inflow Depth > 4.86" for 100-yr event  
Inflow = 15.35 cfs @ 12.06 hrs, Volume= 3.349 af  
Primary = 15.35 cfs @ 12.06 hrs, Volume= 3.349 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 1L: POA #1

Hydrograph



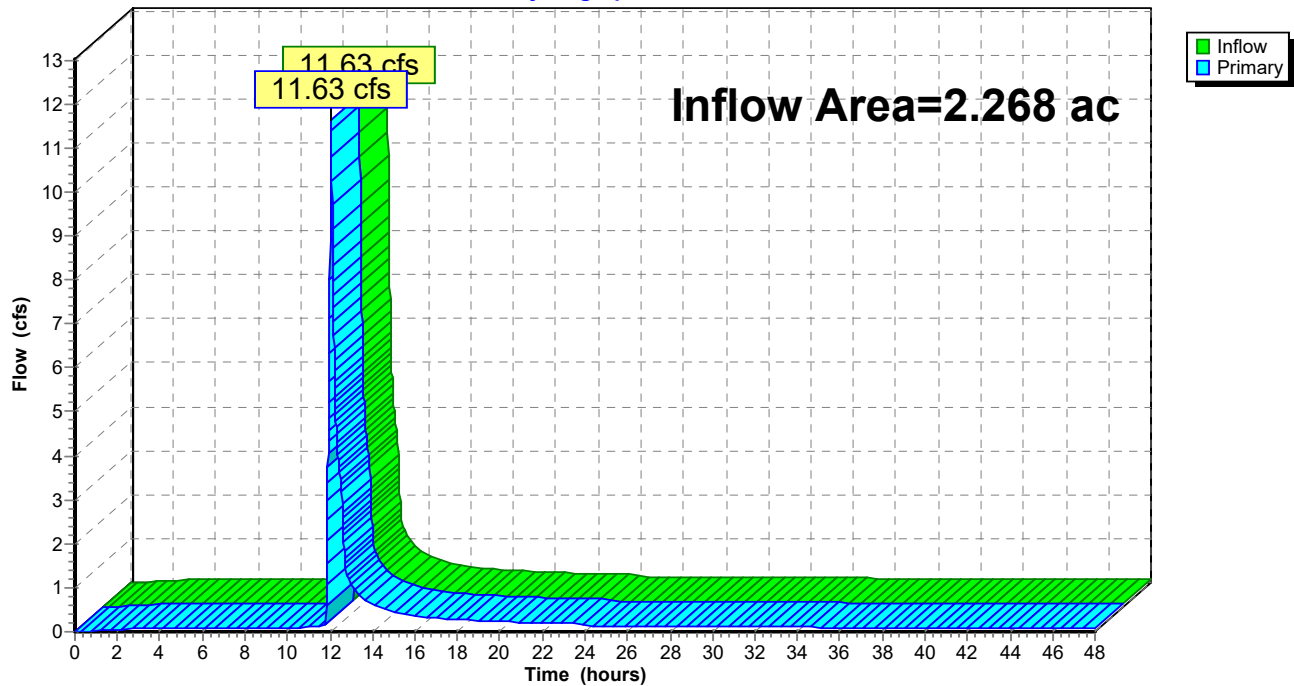
### Summary for Link 2L: MH-A

Inflow Area = 2.268 ac, Inflow Depth > 5.09" for 100-yr event  
 Inflow = 11.63 cfs @ 12.05 hrs, Volume= 0.963 af  
 Primary = 11.63 cfs @ 12.05 hrs, Volume= 0.963 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 2L: MH-A

Hydrograph



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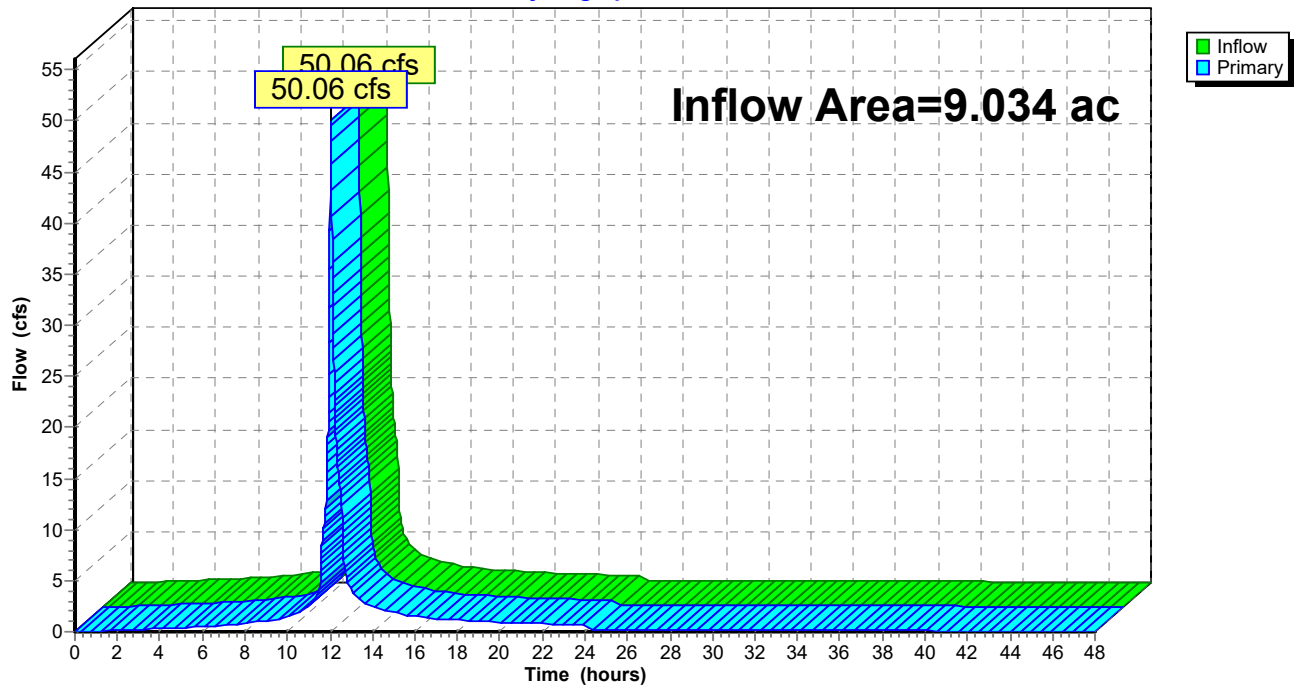
### Summary for Link 3L: POA #2

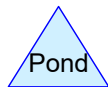
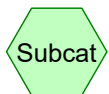
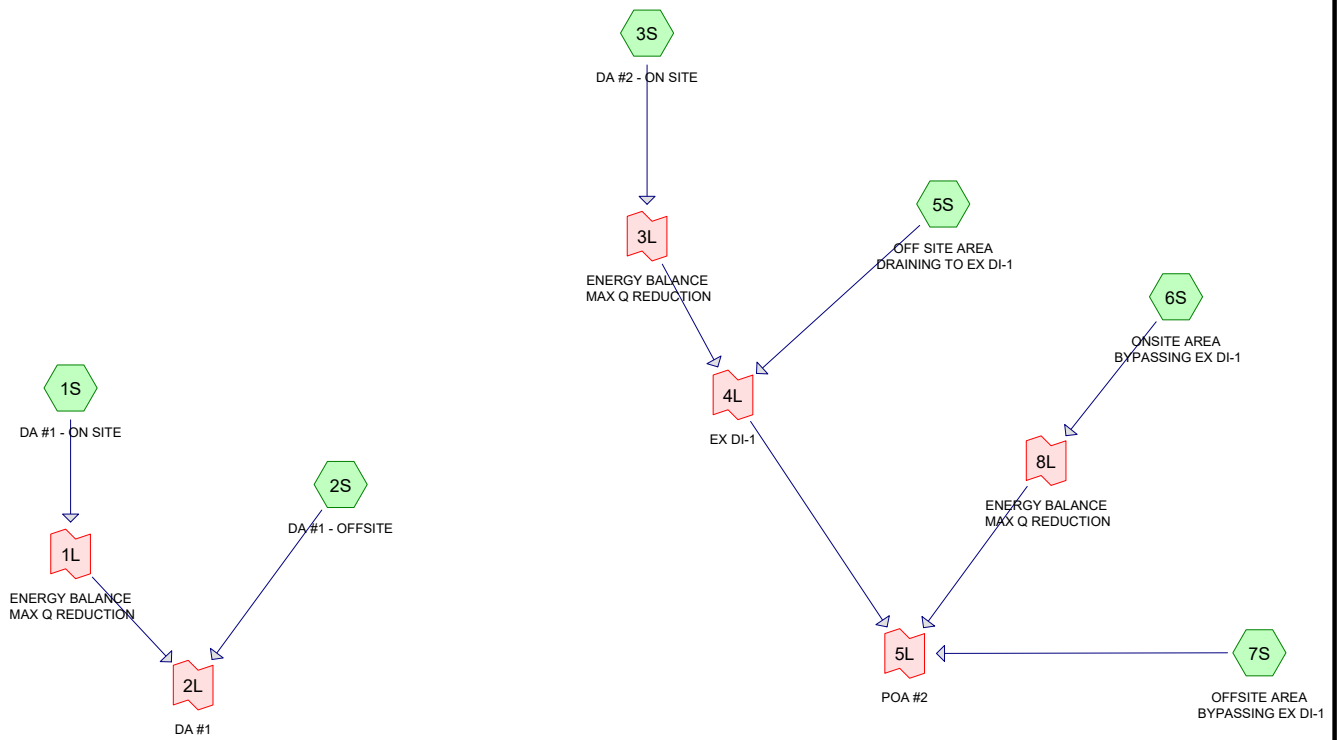
Inflow Area = 9.034 ac, Inflow Depth > 5.34" for 100-yr event  
Inflow = 50.06 cfs @ 12.04 hrs, Volume= 4.020 af  
Primary = 50.06 cfs @ 12.04 hrs, Volume= 4.020 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 3L: POA #2

Hydrograph





## CHANNEL PROTECTION

VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q  
Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

### Subcatchment1S: DA #1 - ON SITE

Runoff Area=2.018 ac Runoff Depth=0.40"  
Flow Length=998' Tc=58.8 min CN=WQ Runoff=0.33 cfs 0.068 af

### Subcatchment2S: DA #1 - OFFSITE

Runoff Area=5.979 ac Runoff Depth=1.16"  
Flow Length=998' Tc=58.8 min CN=WQ Runoff=3.36 cfs 0.580 af

### Subcatchment3S: DA #2 - ON SITE

Runoff Area=2.083 ac Runoff Depth=0.62"  
Flow Length=285' Tc=22.7 min CN=WQ Runoff=0.87 cfs 0.108 af

### Subcatchment5S: OFF SITE AREA DRAINING TO EX DI-1

Runoff Area=0.155 ac Runoff Depth=1.29"  
Flow Length=285' Tc=22.7 min CN=WQ Runoff=0.15 cfs 0.017 af

### Subcatchment6S: ONSITE AREA BYPASSING EX DI-1

Runoff Area=0.354 ac Runoff Depth=0.87"  
Tc=6.0 min CN=WQ Runoff=0.43 cfs 0.026 af

### Subcatchment7S: OFFSITE AREA BYPASSING EX DI-1

Runoff Area=6.750 ac Runoff Depth=1.43"  
Tc=6.0 min CN=WQ Runoff=13.63 cfs 0.806 af

### Link 1L: ENERGY BALANCE MAX Q REDUCTION

x 0.18 Inflow=0.33 cfs 0.068 af  
Primary=0.06 cfs 0.012 af Secondary=0.27 cfs 0.056 af

### Link 2L: DA #1

Inflow=3.41 cfs 0.592 af  
Primary=3.41 cfs 0.592 af

### Link 3L: ENERGY BALANCE MAX Q REDUCTION

x 0.34 Inflow=0.87 cfs 0.108 af  
Primary=0.29 cfs 0.037 af Secondary=0.57 cfs 0.072 af

### Link 4L: EX DI-1

Inflow=0.44 cfs 0.053 af  
Primary=0.44 cfs 0.053 af

### Link 5L: POA #2

Inflow=13.94 cfs 0.868 af  
Primary=13.94 cfs 0.868 af

### Link 8L: ENERGY BALANCE MAX Q REDUCTION

x 0.34 Inflow=0.43 cfs 0.026 af  
Primary=0.14 cfs 0.009 af Secondary=0.28 cfs 0.017 af

**Total Runoff Area = 17.339 ac Runoff Volume = 1.604 af Average Runoff Depth = 1.11"**

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**Summary for Subcatchment 1S: DA #1 - ON SITE**

Runoff = 0.33 cfs @ 12.87 hrs, Volume= 0.068 af, Depth= 0.40"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

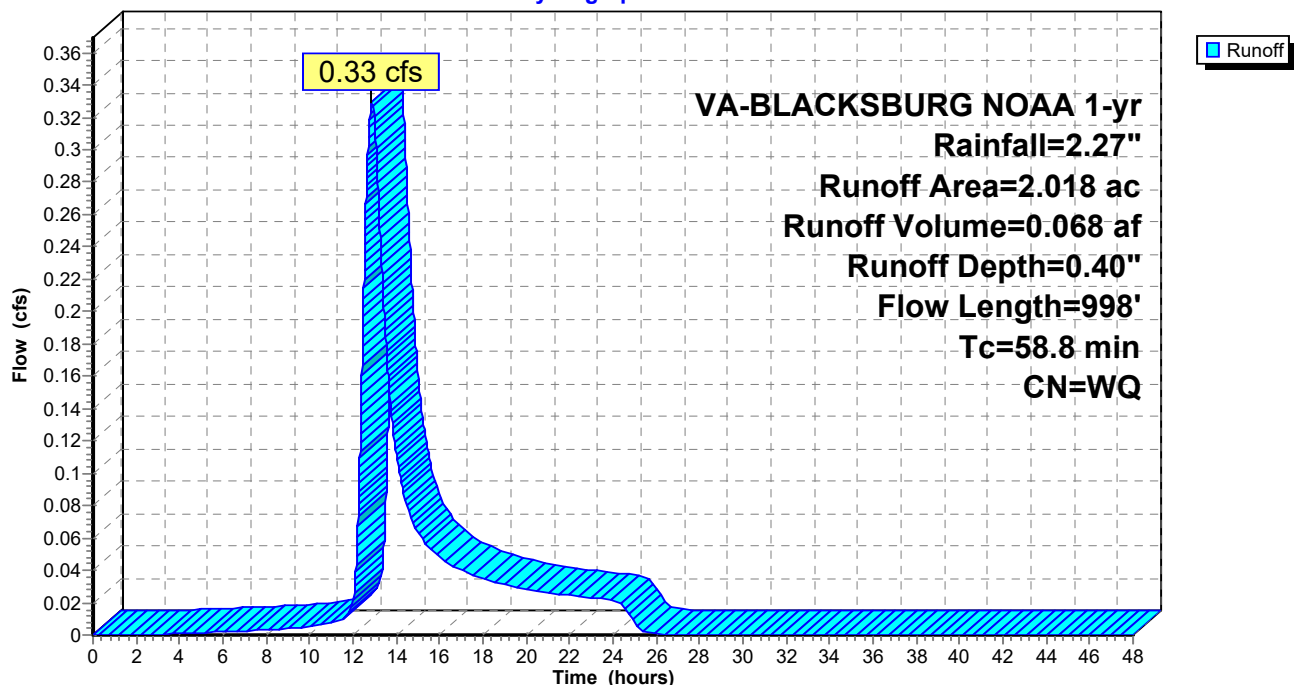
Area (ac)	CN	Description
0.081	61	>75% Grass cover, Good, HSG B
1.103	74	>75% Grass cover, Good, HSG C
0.541	55	Woods, Good, HSG B
0.207	70	Woods, Good, HSG C
0.036	98	Paved parking, HSG B
0.050	98	Paved parking, HSG C
2.018		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
49.6	150	0.0267	0.05		<b>Sheet Flow, Tc1</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
7.4	440	0.0398	1.00		<b>Shallow Concentrated Flow, Tc2</b> Woodland Kv= 5.0 fps
1.8	408	0.0564	3.82		<b>Shallow Concentrated Flow, Tc3</b> Unpaved Kv= 16.1 fps
58.8	998	Total			

**Subcatchment 1S: DA #1 - ON SITE**

Hydrograph



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**Summary for Subcatchment 2S: DA #1 - OFFSITE**

Runoff = 3.36 cfs @ 12.74 hrs, Volume= 0.580 af, Depth= 1.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Area (ac)	CN	Description
0.370	61	>75% Grass cover, Good, HSG B
0.330	74	>75% Grass cover, Good, HSG C
0.382	55	Woods, Good, HSG B
0.078	70	Woods, Good, HSG C
0.164	70	1/2 acre lots, 25% imp, HSG B
0.371	80	1/2 acre lots, 25% imp, HSG C
0.282	75	1/4 acre lots, 38% imp, HSG B
0.496	83	1/4 acre lots, 38% imp, HSG C
0.044	85	1/8 acre lots, 65% imp, HSG B
0.685	92	Urban commercial, 85% imp, HSG B
2.402	94	Urban commercial, 85% imp, HSG C
0.047	98	Paved roads w/curbs & sewers, HSG B
0.209	98	Paved roads w/curbs & sewers, HSG C
0.068	98	Paved parking, HSG B
0.051	98	Paved parking, HSG C
5.979		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
49.6	150	0.0267	0.05		<b>Sheet Flow, Tc1</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
7.4	440	0.0398	1.00		<b>Shallow Concentrated Flow, Tc2</b> Woodland Kv= 5.0 fps
1.8	408	0.0560	3.81		<b>Shallow Concentrated Flow, Tc3</b> Unpaved Kv= 16.1 fps
58.8	998	Total			



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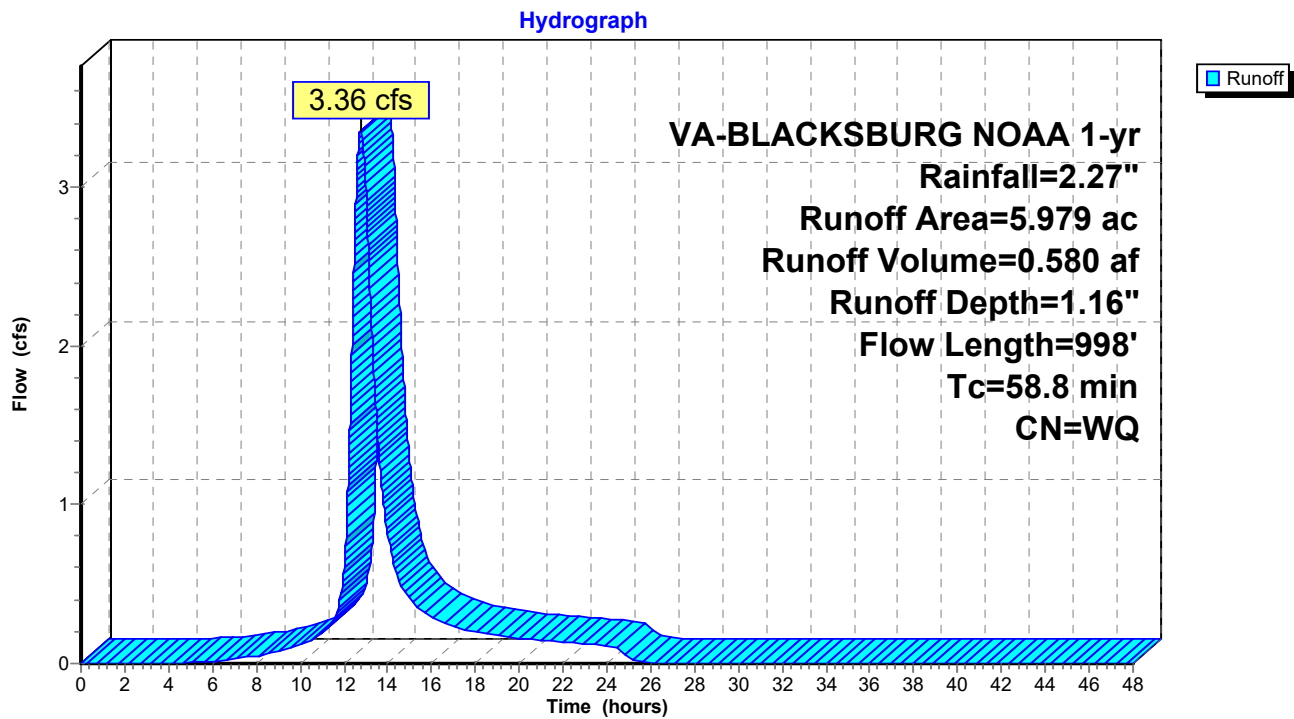
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### Subcatchment 2S: DA #1 - OFFSITE



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### Summary for Subcatchment 3S: DA #2 - ON SITE

Runoff = 0.87 cfs @ 12.30 hrs, Volume= 0.108 af, Depth= 0.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

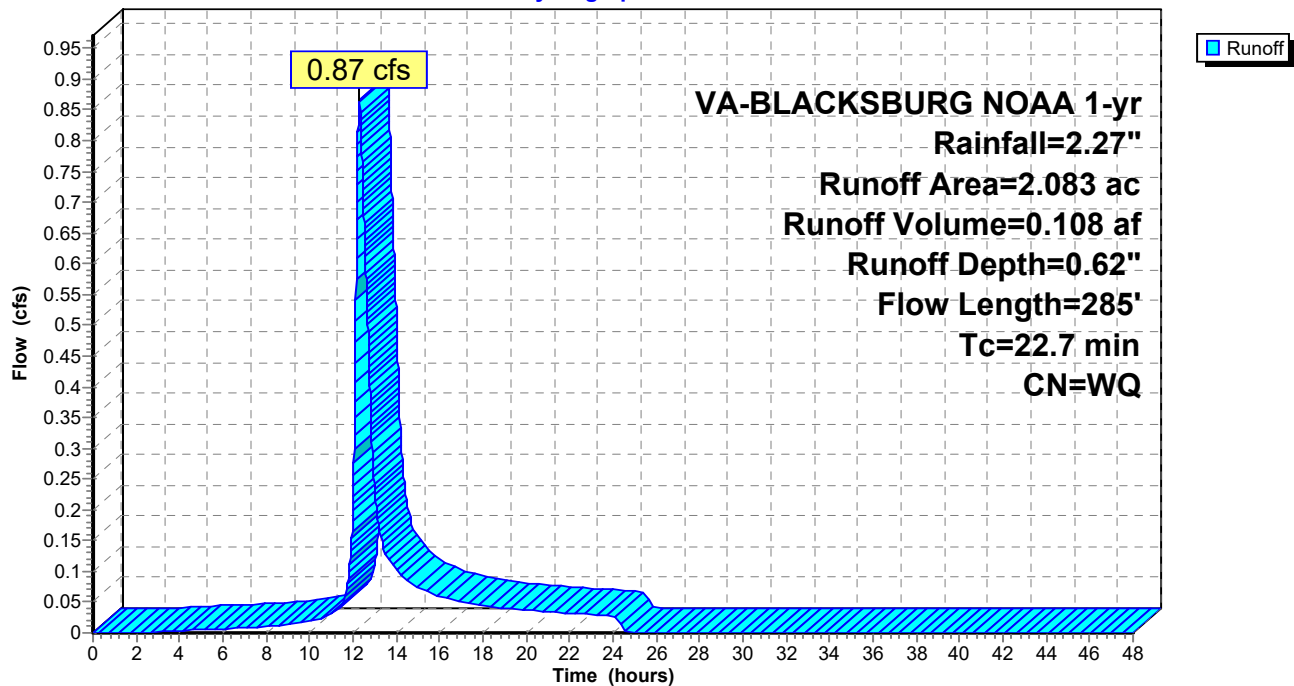
Area (ac)	CN	Description
0.944	74	>75% Grass cover, Good, HSG C
0.005	55	Woods, Good, HSG B
0.870	70	Woods, Good, HSG C
0.264	98	Paved parking, HSG C
2.083		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.8	60	0.0333	0.05		<b>Sheet Flow, Tc4</b> Woods: Dense underbrush n= 0.800 P2= 2.76"
0.9	225	0.0711	4.29		<b>Shallow Concentrated Flow, Tc5</b> Unpaved Kv= 16.1 fps
22.7	285	Total			

### Subcatchment 3S: DA #2 - ON SITE

Hydrograph



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**Summary for Subcatchment 5S: OFF SITE AREA DRAINING TO EX DI-1**

Runoff = 0.15 cfs @ 12.27 hrs, Volume= 0.017 af, Depth= 1.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

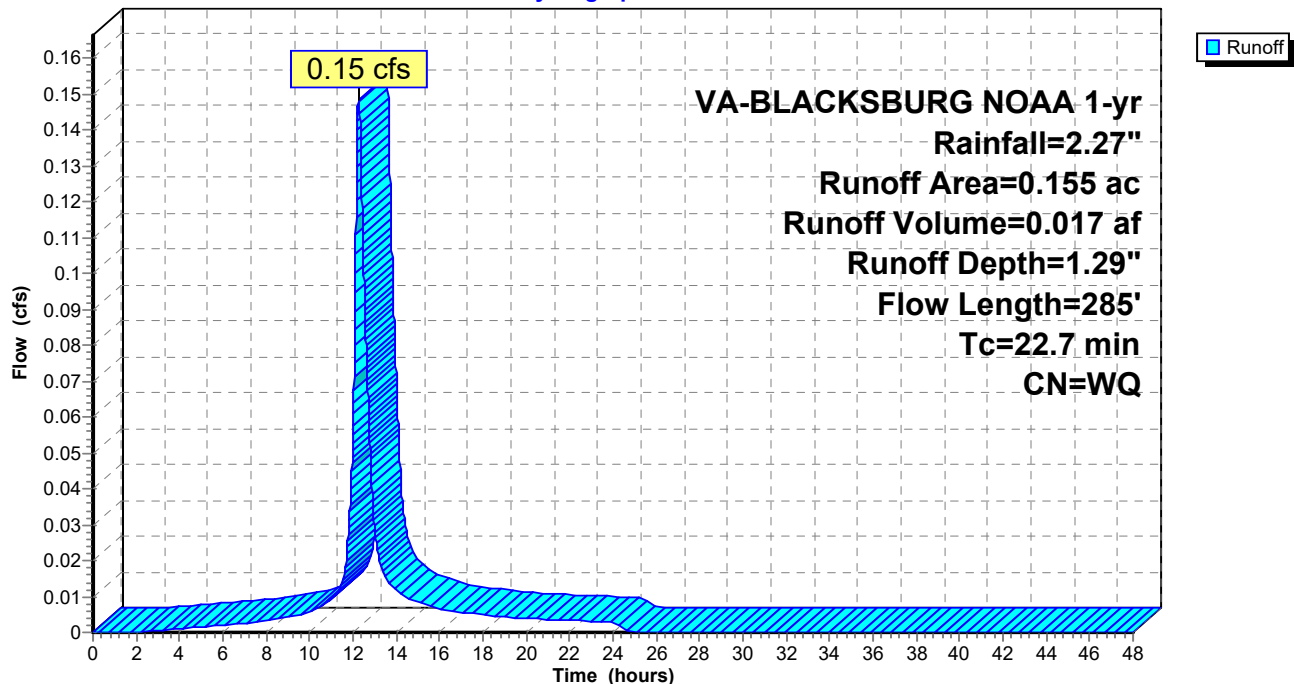
Area (ac)	CN	Description
0.073	74	>75% Grass cover, Good, HSG C
0.002	70	Woods, Good, HSG C
0.080	98	Paved parking, HSG C
0.155		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.8	60	0.0333	0.05		<b>Sheet Flow, Tc4</b>
					Woods: Dense underbrush n= 0.800 P2= 2.76"
0.9	225	0.0711	4.29		<b>Shallow Concentrated Flow, Tc5</b>
					Unpaved Kv= 16.1 fps
22.7	285	Total			

**Subcatchment 5S: OFF SITE AREA DRAINING TO EX DI-1**

Hydrograph



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### Summary for Subcatchment 6S: ONSITE AREA BYPASSING EX DI-1

Runoff = 0.43 cfs @ 12.04 hrs, Volume= 0.026 af, Depth= 0.87"

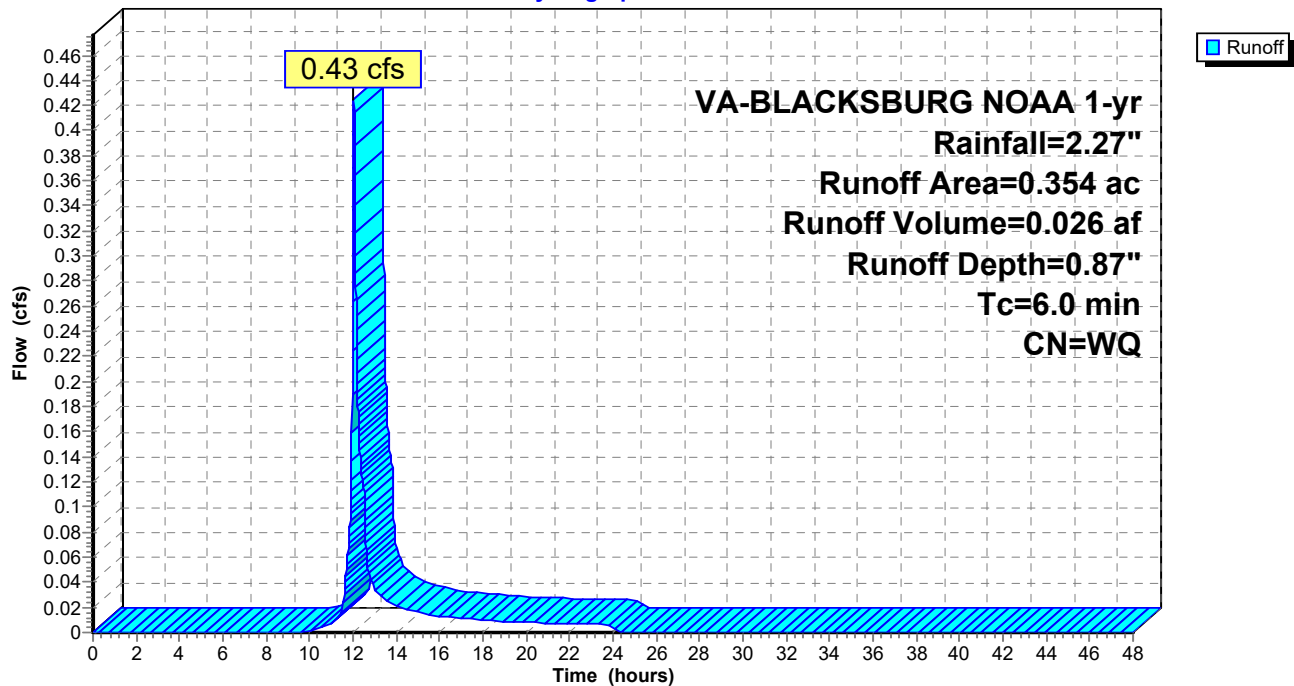
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Area (ac)	CN	Description
0.068	70	Woods, Good, HSG C
0.286	85	1/8 acre lots, 65% imp, HSG B
0.354		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

### Subcatchment 6S: ONSITE AREA BYPASSING EX DI-1

Hydrograph



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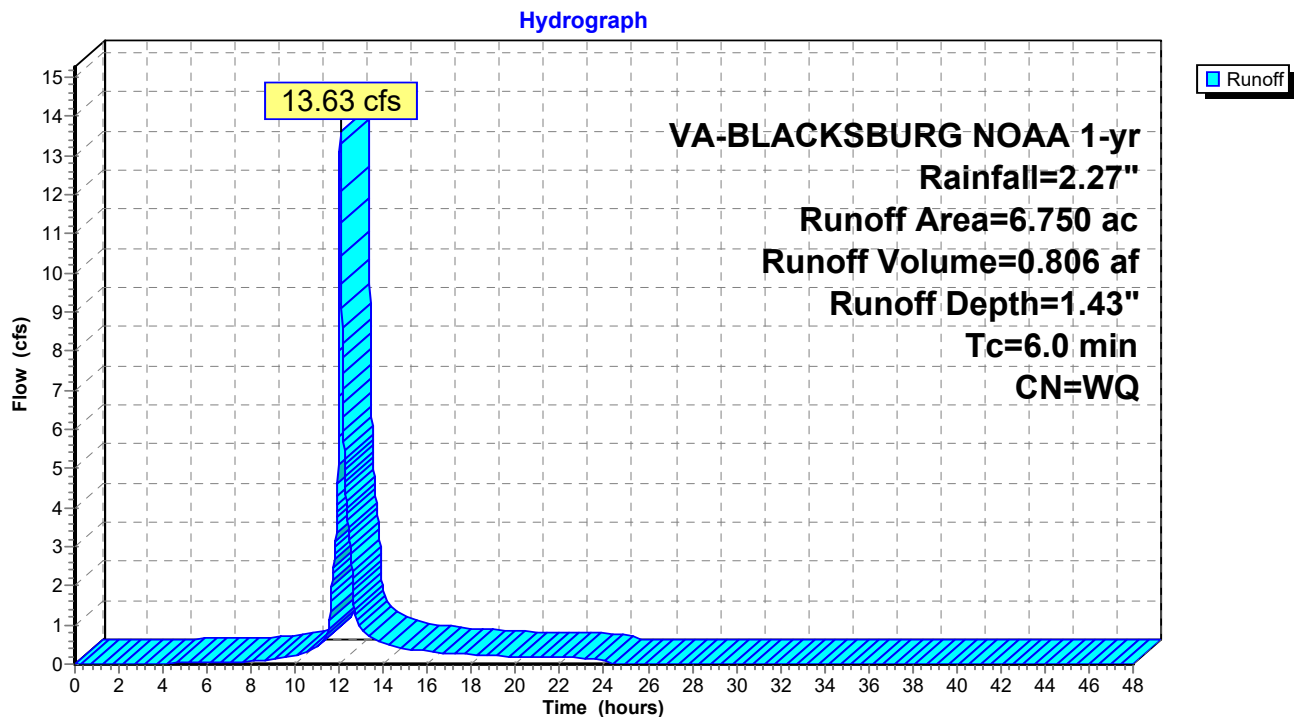
**Summary for Subcatchment 7S: OFFSITE AREA BYPASSING EX DI-1**

Runoff = 13.63 cfs @ 12.04 hrs, Volume= 0.806 af, Depth= 1.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs  
VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

Area (ac)	CN	Description
0.106	61	>75% Grass cover, Good, HSG B
0.044	74	>75% Grass cover, Good, HSG C
0.009	55	Woods, Good, HSG B
0.326	85	1/8 acre lots, 65% imp, HSG B
4.881	90	1/8 acre lots, 65% imp, HSG C
0.028	98	Paved roads w/curbs & sewers, HSG B
1.356	98	Paved parking, HSG C
6.750		Weighted Average

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry, DIRECT

**Subcatchment 7S: OFFSITE AREA BYPASSING EX DI-1**

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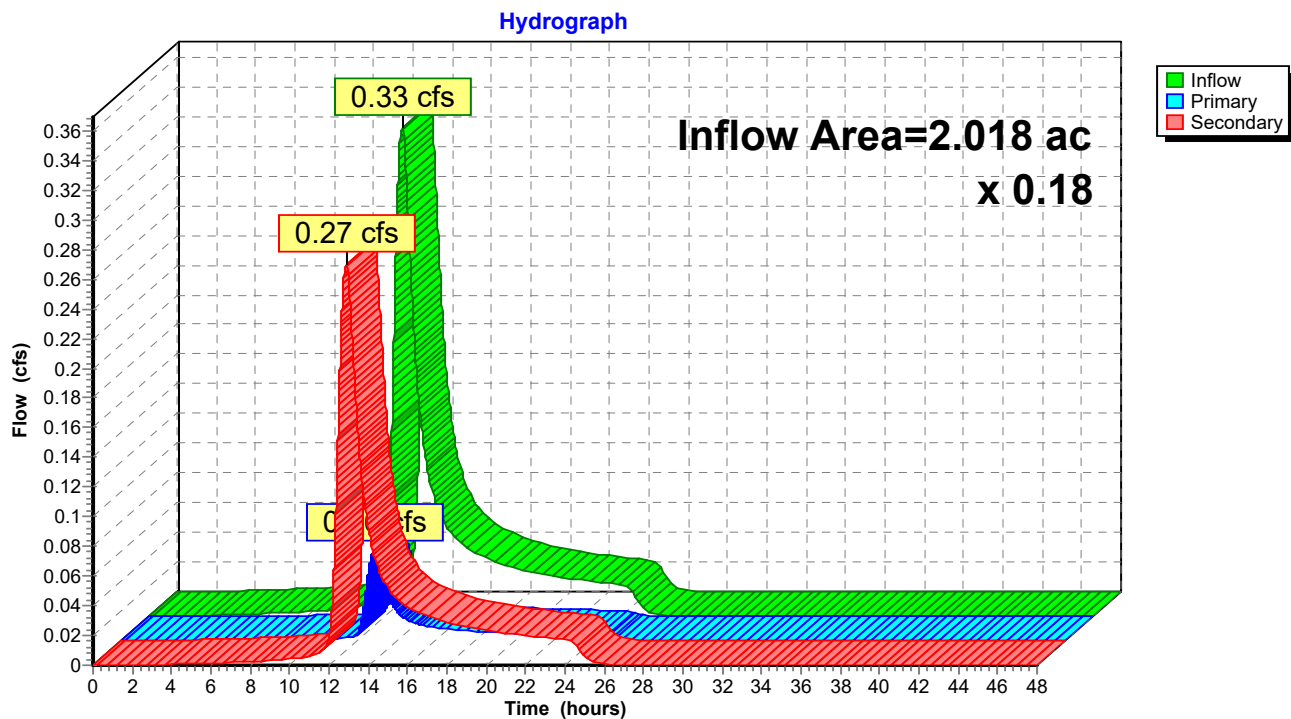
Page 10

### Summary for Link 1L: ENERGY BALANCE MAX Q REDUCTION

Inflow Area = 2.018 ac, Inflow Depth = 0.40" for 1-yr event  
Inflow = 0.33 cfs @ 12.87 hrs, Volume= 0.068 af  
Primary = 0.06 cfs @ 12.87 hrs, Volume= 0.012 af, Atten= 82%, Lag= 0.0 min  
Secondary = 0.27 cfs @ 12.87 hrs, Volume= 0.056 af

Primary outflow = Inflow x 0.18, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 1L: ENERGY BALANCE MAX Q REDUCTION



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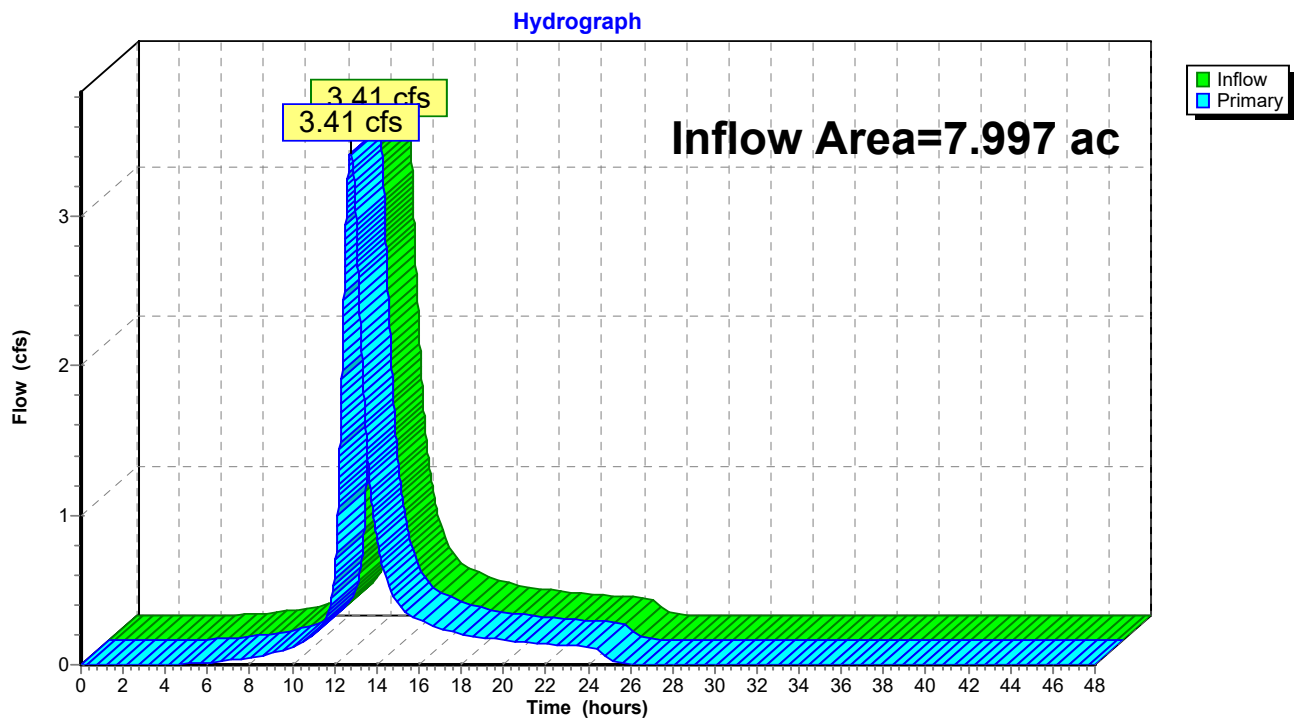
Page 11

### Summary for Link 2L: DA #1

Inflow Area = 7.997 ac, Inflow Depth = 0.89" for 1-yr event  
Inflow = 3.41 cfs @ 12.74 hrs, Volume= 0.592 af  
Primary = 3.41 cfs @ 12.74 hrs, Volume= 0.592 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 2L: DA #1



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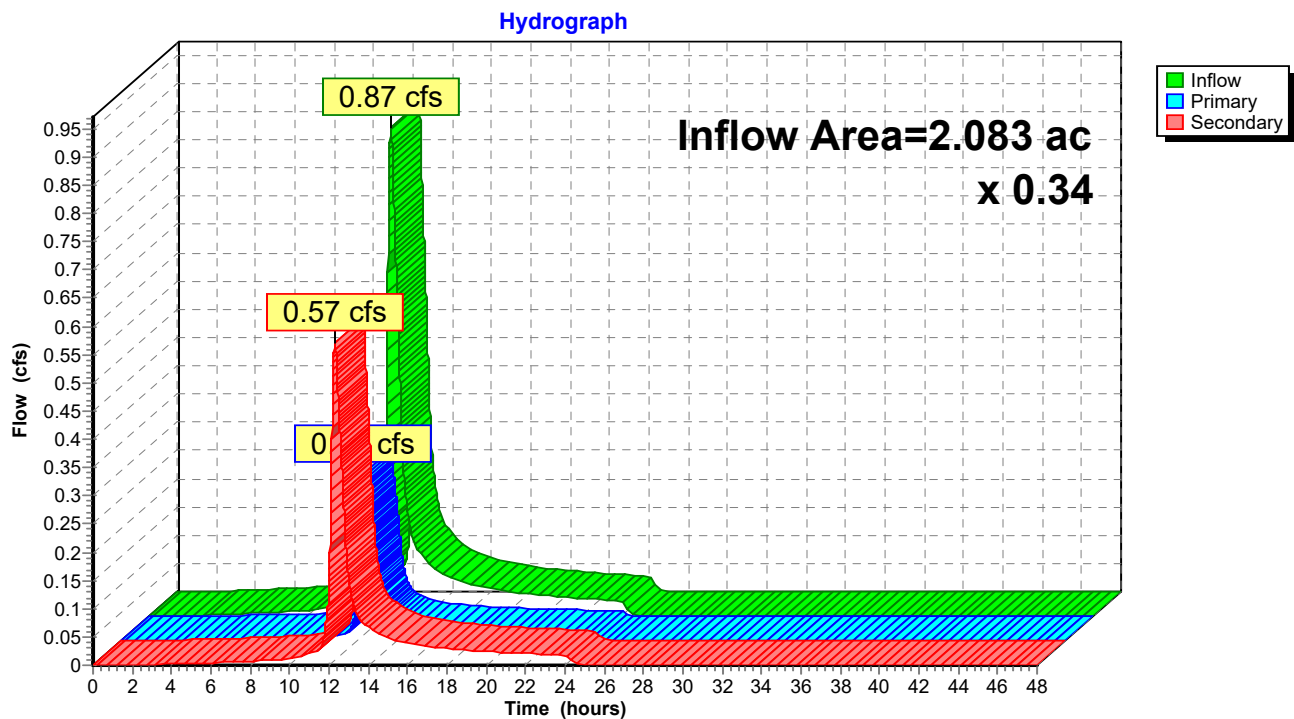
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### Summary for Link 3L: ENERGY BALANCE MAX Q REDUCTION

Inflow Area = 2.083 ac, Inflow Depth = 0.62" for 1-yr event  
Inflow = 0.87 cfs @ 12.30 hrs, Volume= 0.108 af  
Primary = 0.29 cfs @ 12.30 hrs, Volume= 0.037 af, Atten= 66%, Lag= 0.0 min  
Secondary = 0.57 cfs @ 12.30 hrs, Volume= 0.072 af

Primary outflow = Inflow x 0.34, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 3L: ENERGY BALANCE MAX Q REDUCTION





## CHANNEL PROTECTION

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VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

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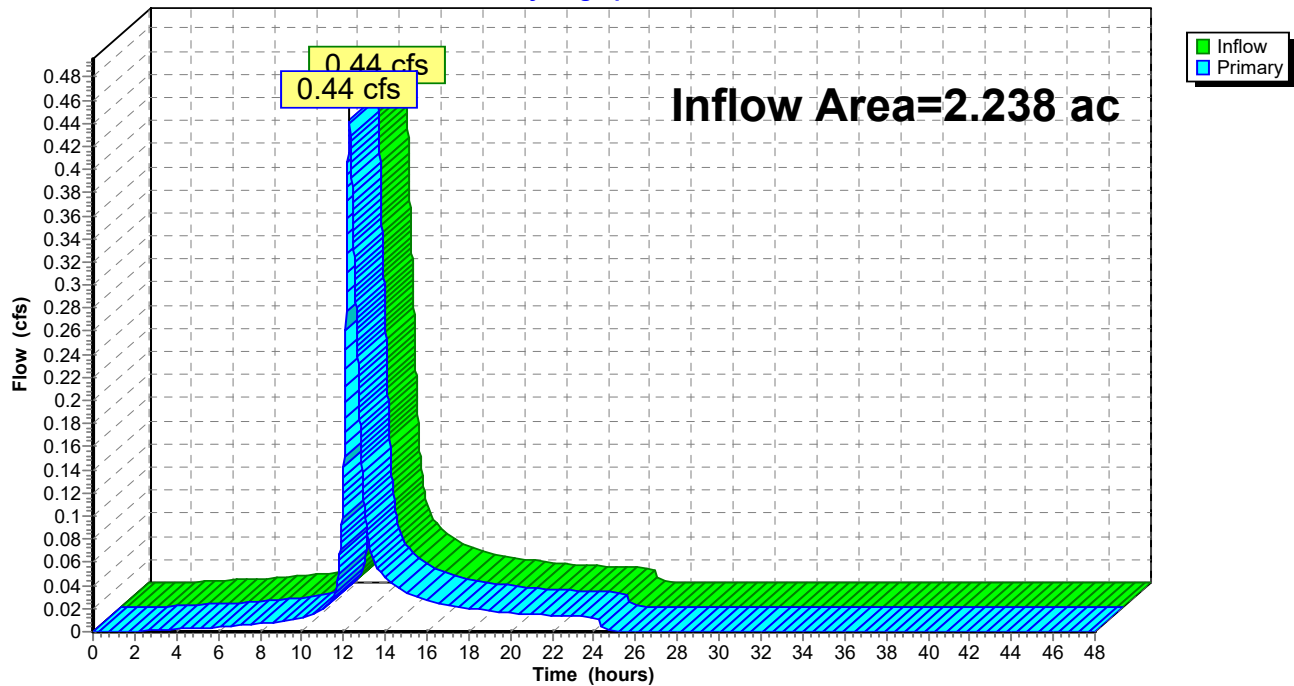
### Summary for Link 4L: EX DI-1

Inflow Area = 2.238 ac, Inflow Depth = 0.29" for 1-yr event  
Inflow = 0.44 cfs @ 12.29 hrs, Volume= 0.053 af  
Primary = 0.44 cfs @ 12.29 hrs, Volume= 0.053 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 4L: EX DI-1

Hydrograph



## CHANNEL PROTECTION

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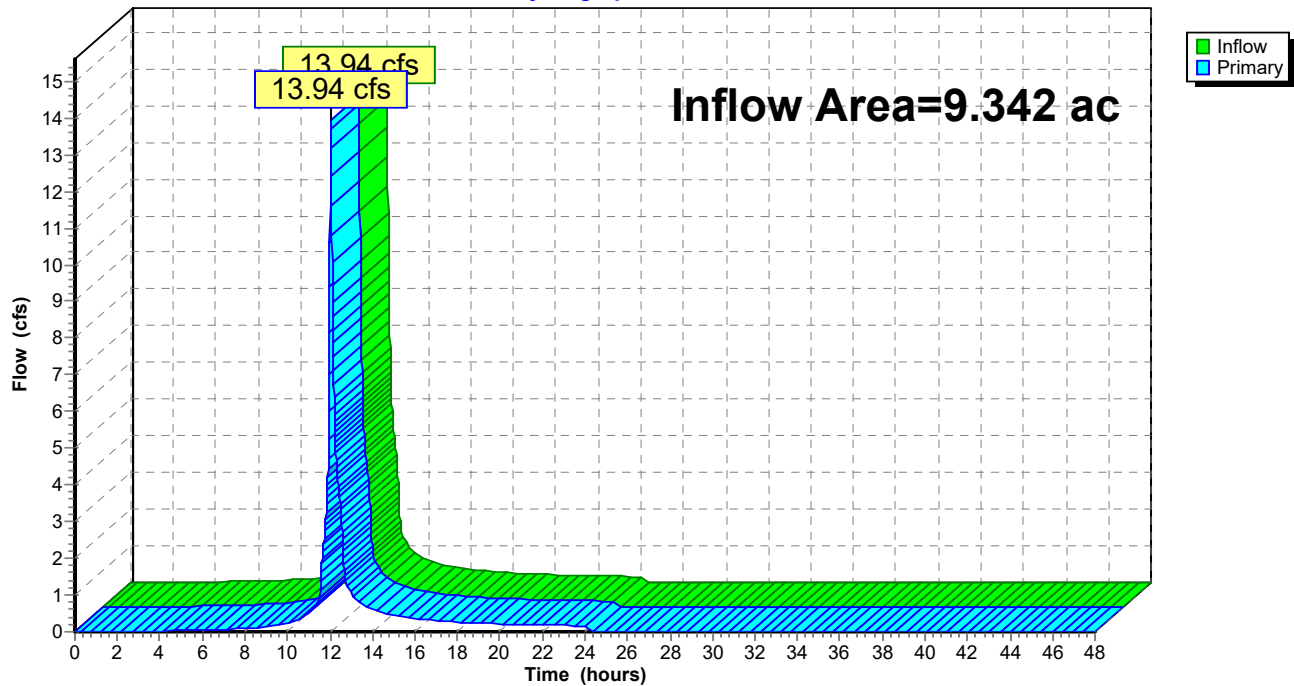
### Summary for Link 5L: POA #2

Inflow Area = 9.342 ac, Inflow Depth = 1.11" for 1-yr event  
Inflow = 13.94 cfs @ 12.04 hrs, Volume= 0.868 af  
Primary = 13.94 cfs @ 12.04 hrs, Volume= 0.868 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 5L: POA #2

Hydrograph



## CHANNEL PROTECTION

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VA-BLACKSBURG NOAA 1-yr Rainfall=2.27"

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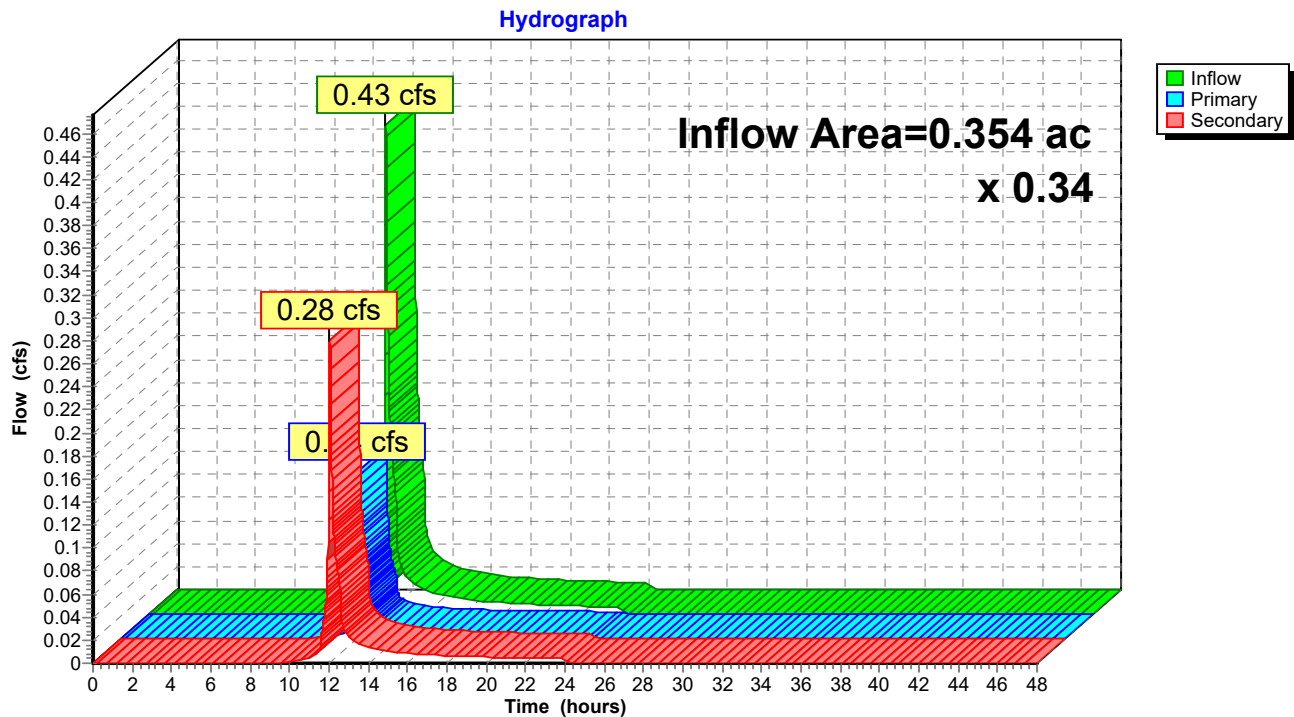
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### Summary for Link 8L: ENERGY BALANCE MAX Q REDUCTION

Inflow Area = 0.354 ac, Inflow Depth = 0.87" for 1-yr event  
Inflow = 0.43 cfs @ 12.04 hrs, Volume= 0.026 af  
Primary = 0.14 cfs @ 12.04 hrs, Volume= 0.009 af, Atten= 66%, Lag= 0.0 min  
Secondary = 0.28 cfs @ 12.04 hrs, Volume= 0.017 af

Primary outflow = Inflow x 0.34, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

### Link 8L: ENERGY BALANCE MAX Q REDUCTION



## **WATER QUALITY**

Project Name:

Timbre Apartments

Date:

8/1/2018

Linear Development Project?

No

CLEAR ALL

data input cells

constant values

calculation cells

final results

Site Information

Post-Development Project (Treatment Volume and Loads)

Enter Total Disturbed Area (acres) →

4.46

Maximum reduction required:

20%

The site's net increase in impervious cover (acres) is:

2.749

Post-Development TP Load Reduction for Site (lb/yr):

5.16

Check:

BMP Design Specifications List: 2013 Draft Stds & Specs

Linear project?

No

Land cover areas entered correctly?

✓

Total disturbed area entered?

✓

Pre-ReDevelopment Land Cover (acres)

	A Soils	B Soils	C Soils	D Soils	Totals
Forest/Open Space (acres) -- undisturbed forest/open space		0.62	1.36		1.98
Managed Turf (acres) -- disturbed, graded for yards or other turf to be mowed/managed		0.08	2.05		2.13
Impervious Cover (acres)		0.04	0.31		0.35
					4.46

Post-Development Land Cover (acres)

	A Soils	B Soils	C Soils	D Soils	Totals
Forest/Open Space (acres) -- undisturbed, protected forest/open space or reforested land		0.01	0.07		0.09
Managed Turf (acres) -- disturbed, graded for yards or other turf to be mowed/managed		0.25	1.03		1.28
Impervious Cover (acres)		0.47	2.63		3.10
Area Check	OK.	OK.	OK.	OK.	4.46

\* Forest/Open Space areas must be protected in accordance with the Virginia Runoff Reduction Method

Constants

Annual Rainfall (inches)	43
Target Rainfall Event (inches)	1.00
Total Phosphorus (TP) EMC (mg/L)	0.26
Total Nitrogen (TN) EMC (mg/L)	1.86
Target TP Load (lb/acre/yr)	0.41
Pj (unitless correction factor)	0.90

Runoff Coefficients (Rv)

	A Soils	B Soils	C Soils	D Soils
Forest/Open Space	0.02	0.03	0.04	0.05
Managed Turf	0.15	0.20	0.22	0.25
Impervious Cover	0.95	0.95	0.95	0.95

LAND COVER SUMMARY -- PRE-REDEVELOPMENT

Land Cover Summary-Pre		
Pre-ReDevelopment	Listed	Adjusted <sup>1</sup>
Forest/Open Space Cover (acres)	1.98	0.26
Weighted Rv(forest)	0.04	0.03
% Forest	44%	15%
Managed Turf Cover (acres)	2.13	1.11
Weighted Rv(turf)	0.22	0.22
% Managed Turf	48%	65%
Impervious Cover (acres)	0.35	0.35
Rv(impervious)	0.95	0.95
% Impervious	8%	20%
Total Site Area (acres)	4.46	1.71
Site Rv	0.20	0.34

Treatment Volume and Nutrient Load

Pre-ReDevelopment Treatment Volume (acre-ft)	0.0727	0.0485
Pre-ReDevelopment Treatment Volume (cubic feet)	3,168	2,115
Pre-ReDevelopment TP Load (lb/yr)	1.99	1.33
Pre-ReDevelopment TP Load per acre (lb/acre/yr)	0.45	0.78
Baseline TP Load (lb/yr) (0.41 lbs/acre/yr applied to pre-redevelopment area excluding pervious land proposed for new impervious cover)		0.70

<sup>1</sup> Adjusted Land Cover Summary:

Pre-ReDevelopment land cover minus pervious land cover (forest/open space or managed turf) acreage proposed for new impervious cover.

Adjusted total acreage is consistent with Post-ReDevelopment acreage (minus acreage of new impervious cover).

Column I shows load reduction requirement for new impervious cover (based on new development load limit, 0.41 lbs/acre/year).

LAND COVER SUMMARY -- POST DEVELOPMENT

Land Cover Summary-Post (Final)		
Post ReDev. & New Impervious		
Forest/Open Space Cover (acres)	0.09	
Weighted Rv(forest)	0.04	
% Forest	2%	
Managed Turf Cover (acres)	1.28	
Weighted Rv (turf)	0.22	
% Managed Turf	29%	
Impervious Cover (acres)	3.10	
Rv(impervious)	0.95	
% Impervious	69%	
Final Site Area (acres)	4.46	
Final Post Dev Site Rv	0.72	

Land Cover Summary-Post	
Post-ReDevelopment	
Forest/Open Space Cover (acres)	0.09
Weighted Rv(forest)	0.04
% Forest	5%
Managed Turf Cover (acres)	1.28
Weighted Rv (turf)	0.22
% Managed Turf	75%
ReDev. Impervious Cover (acres)	0.35
Rv(impervious)	0.95
% Impervious	20%
Total ReDev. Site Area (acres)	1.71
ReDev Site Rv	0.36

Land Cover Summary-Post	
Post-Development New Impervious	
New Impervious Cover (acres)	2.75
Rv(impervious)	0.95

Treatment Volume and Nutrient Load

Final Post-Development Treatment Volume (acre-ft)	0.2686	Post-ReDevelopment Treatment Volume (acre-ft)	0.0509	Post-Development Treatment Volume (acre-ft)	0.2176
Final Post-Development Treatment Volume (cubic feet)	11,699	Post-ReDevelopment Treatment Volume (cubic feet)	2,219	Post-Development Treatment Volume (cubic feet)	9,480
Final Post-Development TP Load (lb/yr)	7.35	Post-ReDevelopment Load (TP) (lb/yr)*	1.39	Post-Development TP Load (lb/yr)	5.96
Final Post-Development TP Load per acre (lb/acre/yr)	1.65	Post-ReDevelopment TP Load per acre (lb/acre/yr)	0.81		
		Max. Reduction Required (Below Pre-ReDevelopment Load)	20%		
		TP Load Reduction Required for Redeveloped Area (lb/yr)	0.33	TP Load Reduction Required for New Impervious Area (lb/yr)	4.83

Post-Development Requirement for Site Area

TP Load Reduction Required (lb/yr)	5.16
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Nitrogen Loads (Informational Purposes Only)

Pre-ReDevelopment TN Load (lb/yr)	14.24	Final Post-Development TN Load (Post-ReDevelopment & New Impervious) (lb/yr)	52.58
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## DEQ Virginia Runoff Reduction Method Re-Development Compliance Spreadsheet - Version 3.0

BMP Design Specifications List: 2013 Draft Stds &amp; Specs

## Site Summary

Project Title: Timbre Apartments

Date: 43313

Total Rainfall (in):	43
Total Disturbed Acreage:	4.46

## Site Land Cover Summary

## Pre-ReDevelopment Land Cover (acres)

	A soils	B Soils	C Soils	D Soils	Totals	% of Total
Forest/Open (acres)	0.00	0.62	1.36	0.00	1.98	44
Managed Turf (acres)	0.00	0.08	2.05	0.00	2.13	48
Impervious Cover (acres)	0.00	0.04	0.31	0.00	0.35	8
					4.46	100

## Post-ReDevelopment Land Cover (acres)

	A soils	B Soils	C Soils	D Soils	Totals	% of Total
Forest/Open (acres)	0.00	0.01	0.07	0.00	0.09	2
Managed Turf (acres)	0.00	0.25	1.03	0.00	1.28	29
Impervious Cover (acres)	0.00	0.47	2.63	0.00	3.10	69
					4.46	100

\* Forest/Open Space areas must be protected in accordance with the Virginia Runoff Reduction Method

## Site Tv and Land Cover Nutrient Loads

	Final Post-Development (Post-ReDevelopment & New Impervious)	Post- ReDevelopment	Post- Development (New Impervious)	Adjusted Pre- ReDevelopment
Site Rv	0.72	0.36	0.95	0.34
Treatment Volume (ft <sup>3</sup> )	11,699	2,219	9,480	2,115
TP Load (lb/yr)	7.35	1.39	5.96	1.33

Pre- ReDevelopment TP Load per acre (lb/acre/yr)	Final Post-Development TP Load per acre (lb/acre/yr)	Post-ReDevelopment TP Load per acre (lb/acre/yr)
0.78	1.65	0.81

Total TP Load Reduction Required (lb/yr)	5.16	0.33	4.83
--	------	------	------

	Final Post-Development Load (Post-ReDevelopment & New Impervious)	Pre- ReDevelopment
TN Load (lb/yr)	52.58	14.24

Site Compliance Summary

Maximum % Reduction Required Below Pre-ReDevelopment Load	20%
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Total Runoff Volume Reduction (ft <sup>3</sup> )	0
Total TP Load Reduction Achieved (lb/yr)	0.00
Total TN Load Reduction Achieved (lb/yr)	0.00
Remaining Post Development TP Load (lb/yr)	7.35
Remaining TP Load Reduction (lb/yr) Required	5.16